comune di
PRATO
Codice Fiscale: **84006890481**

Progetto: **Medialibrary, Bar, Coworking e Piazza del Totem**

POR FESR 2014-2020 - Progetto di Innovazione Urbana (P.I.U.)

Titolo: Relazione geotecnica

Fase: **Progetto esecutivo**

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Scala: **----**

Spazio riservato agli uffici:

data: **Novembre 2017**

PIU – PROGETTO INNOVAZIONE URBANA

OPERAZIONE COWORKING, MEDIALIBRARY

A6 – RELAZIONE GEOTECNICA

INTERVENTI DI RINFORZO STRUTTURALE E STRUTTURE NUOVE

(OTTOBRE 2017)

Introduzione

Sistemi di riferimento
Le coordinate, i carichi concentrati, i cedimenti, le reazioni vincolari e gli spostamenti dei NODI sono riferiti ad una terna destra cartesiana globale con l'asse Z verticale rivolto verso l'alto.
I carichi in coordinate locali e le sollecitazioni delle ASTE sono riferite ad una terna destra cartesiana locale così definita:
- origine nel nodo iniziale dell'asta;
- asse X coincidente con l'asse dell'asta e con verso dal nodo iniziale al nodo finale;
- immaginando la trave a sezione rettangolare l'asse Y è parallelo alla base e l'asse Z è parallelo all'altezza. La rotazione dell'asta comporta quindi una rotazione di tutta la terna locale.

Si può immaginare la terna locale di un'asta comunque disposta nello spazio come derivante da quella globale dopo una serie di trasformazioni:
- una rotazione intorno all'asse Z che porti l'asse X a coincidere con la proiezione dell'asse dell'asta sul piano orizzontale;
- una traslazione lungo il nuovo asse X così definito in modo da portare l'origine a coincidere con la proiezione del nodo iniziale dell'asta sul piano orizzontale;
- una traslazione lungo l'asse Z che porti l'origine a coincidere con il nodo iniziale dell'asta;
- una rotazione intorno all'asse Y così definito che porti l'asse X a coincidere con l'asse dell'asta;
- una rotazione intorno all'asse X così definito pari alla rotazione dell'asta.

In pratica le travi prive di rotazione avranno sempre l'asse Z rivolto verso l'alto e l'asse Y nel piano del solaio, mentre i pilastri privi di rotazione avranno l'asse Y parallelo all'asse Y globale e l'asse Z parallelo ma controverso all'asse X globale. Da notare quindi che per i pilastri la "base" è il lato parallelo a Y.

Le sollecitazioni ed i carichi in coordinate locali negli ELEMENTI BIDIMENSIONALI e nei MURI sono riferiti ad una terna destra cartesiana locale così definita:
- origine nel primo nodo dell'elemento;
- asse X coincidente con la congiungente il primo ed il secondo nodo dell'elemento;
- asse Y definito come prodotto vettoriale fra il versore dell'asse X e il versore della congiungente il primo e il quarto nodo. Asse Z a formare con gli altri due una terna destrorsa.

Praticamente un elemento verticale con l'asse X locale coincidente con l'asse X globale ha anche gli altri assi locali coincidenti con quelli globali.

Rotazioni e momenti
Seguendo il principio adottato per tutti i carichi che sono positivi se CONTROVERSI agli assi, anche i momenti concentrati e le rotazioni impresse in coordinate globali risultano positivi se CONTROVERSI al segno positivo delle rotazioni. Il segno positivo dei momenti e delle rotazioni è quello orario per l'osservatore posto nell'origine: X ruota su Y, Y ruota su Z, Z ruota su X. In pratica è sufficiente adottare la regola della mano destra: col pollice rivolto nella direzione dell'asse, la rotazione che porta a chiudere il palmo della mano corrisponde al segno positivo.

Normativa di riferimento
La normativa di riferimento è la seguente:
- Legge n. 64 del 2/2/1974 - Provvedimenti per le costruzioni con particolari prescrizioni per le zone sismiche.

- D.M. del 24/1/1986 - Norme tecniche relative alle costruzioni sismiche.

- Legge n. 1086 del 5/11/1971 - Norme per la disciplina delle opere di conglomerato cementizio armato, normale e precompresso ed a struttura metallica.

- D.M. del 14/2/1992 - Norme tecniche per l'esecuzione delle opere in c.a. normale e precompresso e per le strutture metalliche.

- D.M. del 9/1/1996 - Norme tecniche per l'esecuzione delle opere in c.a. normale e precompresso e per le strutture metalliche.

- D.M. del 16/1/1996 - Norme tecniche per le costruzioni in zone sismiche.

- Circolare n. 21745 del 30/7/1981 - Legge n. 219 del 14/5/1981 - Art. 10 - Istruzioni relative al

rafforzamento degli edifici in muratura danneggiati dal sisma.

- Regione Autonoma Friuli Venezia Giulia - Legge Regionale n. 30 del 20/6/1977 - Documentazione tecnica per la progettazione e direzione delle opere di riparazione degli edifici - Documento Tecnico n. 2 - Raccomandazioni per la riparazione strutturale degli edifici in muratura.

- D.M. del 20/11/1987 - Norme Tecniche per la progettazione, esecuzione e collaudo degli edifici in muratura e per il loro consolidamento.

- Norme Tecniche C.N.R. n. 10011-85 del 18/4/1985 - Costruzioni di acciaio - Istruzioni per il calcolo, l'esecuzione, il collaudo e la manutenzione.

- Norme Tecniche C.N.R. n. 10025-84 del 14/12/1984 - Istruzioni per il progetto, l'esecuzione ed il controllo delle strutture prefabbricate in conglomerato cementizio e per le strutture costruite con sistemi industrializzati di acciaio - Istruzioni per il calcolo, l'esecuzione, il collaudo e la manutenzione.

- Circolare n. 65 del 10/4/1997 - Istruzioni per l'applicazione delle "Norme tecniche per le costruzioni in zone sismiche" di cui al D.M. del 16/1/1996.

- Eurocodice 5 - Progettazione delle strutture di legno.

- DIN 1052 - Metodi di verifica per il legno.

- D.M. del 14/1/2008 - Norme tecniche per le costruzioni. Le verifiche degli elementi di fondazione sono eseguite utilizzando l'Approccio 2.

- Circolare n. 617 del 2/2/2009 - Istruzioni per l'applicazione delle "Nuove norme tecniche per le costruzioni" di cui al D.M. del 14/1/2008.

- Documento Tecnico CNR-DT 200 R1/2012 - Istruzioni per la Progettazione, l'Esecuzione ed il Controllo di Interventi di Consolidamento Statico mediante l'utilizzo di Compositi Fibrorinforzati.

- Eurocodice 3 - Progettazione delle strutture in acciaio.

Unità di misura
Le unità di misura adottate sono le seguenti:
- lunghezze : m
- forze : daN
- masse : kg
- temperature : gradi centigradi
- angoli : gradi sessadecimali o radianti

ELENCO VINCOLI NODI

Simbologia

Vn = Numero del vincolo nodo
Comm. = Commento
TV = Tipo vincolo se valutato da stratigrafia
SP = Plinto senza pali
CP = Palo o plinto con pali
Sx = Spostamento in dir. X (L=libero, B=bloccato, E=elastico)
Sy = Spostamento in dir. Y (L=libero, B=bloccato, E=elastico)
Sz = Spostamento in dir. Z (L=libero, B=bloccato, E=elastico)
Rx = Rotazione intorno all'asse X (L=libera, B=bloccata, E=elastica)
Ry = Rotazione intorno all'asse Y (L=libera, B=bloccata, E=elastica)
Rz = Rotazione intorno all'asse Z (L=libera, B=bloccata, E=elastica)
RL = Rotazione libera
Ly = Lunghezza (dir. Y locale)
Lz = Larghezza (dir. Z locale)
Kt = Coeff. di sottofondo su suolo elastico alla Winkler

Vn	Comm.	TV	Sx	Sy	Sz	Rx	Ry	Rz	RL	Ly <m>	Lz <m>	Kt <daN/cmc>
1	Libero		L	L	L	L	L	L				
2	Incastro		B	B	B	B	B	B				
3	El. sew 110001	CP	E	E	E	E	E	B				f(strat.)
3	El. sew 110001	SP	B	B	E	E	E	B				f(strat.)

ELENCO COSTANTI ELASTICHE NODALI

Simbologia

Nodo = Numero del nodo
Kx = Costante elastica in dir. X
Ky = Costante elastica in dir. Y
Kz = Costante elastica in dir. Z
KRx = Costante elastica intorno all'asse X
KRy = Costante elastica intorno all'asse Y

Nodo	Kx <daN/cm>	Ky <daN/cm>	Kz <daN/cm>	KRx <daNm/rad>	KRy <daNm/rad>
11	--	--	22562.50	752083.00	481333.00

ELENCO NODI

Simbologia

Nodo = Numero del nodo
X = Coordinata X del nodo
Y = Coordinata Y del nodo
Z = Coordinata Z del nodo
Imp. = Numero dell'impalcato
Vn = Numero del vincolo nodo

Nodo	X <m>	Y <m>	Z <m>	Imp.	Vn	Nodo	X <m>	Y <m>	Z <m>	Imp.	Vn	Nodo	X <m>	Y <m>	Z <m>	Imp.	Vn
-2590	40.02	-24.62	5.00	2	1	-2589	40.02	-24.62	4.50	0	1	-2588	40.02	-24.62	4.00	0	1
-2587	40.02	-24.62	3.50	0	1	-2586	40.02	-24.62	3.00	0	1	-2585	40.02	-24.62	2.50	0	1
-2584	40.02	-24.62	2.00	0	1	-2583	40.02	-24.62	1.50	0	1	-2582	40.02	-24.62	1.00	0	1
-2581	40.02	-24.62	0.50	0	1	-2580	40.02	-24.62	0.00	0	1	-2579	40.02	-24.62	-0.45	0	1
-2578	40.02	-24.62	-0.97	0	1	-2577	40.02	-24.62	-1.35	0	1	-2576	40.02	-24.62	-1.80	0	1
-2575	40.02	-24.62	-2.25	0	1	-2574	40.02	-24.62	-2.70	0	1	-2573	47.38	-17.83	13.38	0	1
-2572	44.75	-17.83	13.38	0	1	-2571	39.85	-17.83	13.38	0	1	-2570	34.95	-17.83	13.38	0	1
-2569	29.91	-17.83	13.38	0	1	-2568	24.98	-17.83	13.38	0	1	-2567	20.76	-17.83	13.38	0	1
-2566	47.38	-14.99	12.48	0	1	-2565	44.75	-14.99	12.48	0	1	-2564	39.85	-14.99	12.48	0	1
-2563	34.95	-14.99	12.48	0	1	-2562	29.91	-14.99	12.48	0	1	-2561	24.98	-14.99	12.48	0	1
-2560	20.76	-14.99	12.48	0	1	-2559	47.38	-19.13	12.41	0	1	-2558	44.75	-19.13	12.41	0	1
-2557	39.85	-19.13	12.41	0	1	-2556	34.95	-19.13	12.41	0	1	-2555	29.91	-19.13	12.41	0	1
-2554	24.98	-19.13	12.41	0	1	-2553	20.76	-19.13	12.41	0	1	-2552	47.38	-20.43	11.44	0	1
-2551	44.75	-20.43	11.44	0	1	-2550	39.85	-20.43	11.44	0	1	-2549	34.95	-20.43	11.44	0	1
-2548	29.91	-20.43	11.44	0	1	-2547	24.98	-20.43	11.44	0	1	-2546	20.76	-20.43	11.44	0	1
-2545	47.38	-13.47	10.62	0	1	-2544	44.75	-13.47	10.62	0	1	-2543	39.85	-13.47	10.62	0	1
-2542	34.95	-13.47	10.62	0	1	-2541	29.91	-13.47	10.62	0	1	-2540	24.98	-13.47	10.62	0	1
-2539	20.76	-13.47	10.62	0	1	-2538	47.38	-21.73	10.47	0	1	-2537	44.75	-21.73	10.47	0	1
-2536	39.85	-21.73	10.47	0	1	-2535	34.95	-21.73	10.47	0	1	-2534	29.91	-21.73	10.47	0	1
-2533	24.98	-21.73	10.47	0	1	-2532	20.76	-21.73	10.47	0	1	-2531	47.38	-23.05	9.48	0	1
-2530	44.75	-23.05	9.48	0	1	-2529	39.85	-23.05	9.48	0	1	-2528	34.95	-23.05	9.48	0	1
-2527	29.91	-23.05	9.48	0	1	-2526	24.98	-23.05	9.48	0	1	-2525	20.76	-23.05	9.48	0	1
-2524	47.38	-24.37	8.50	0	1	-2523	44.75	-24.37	8.50	0	1	-2522	39.85	-24.37	8.50	0	1
-2521	34.95	-24.37	8.50	0	1	-2520	29.91	-24.37	8.50	0	1	-2519	24.98	-24.37	8.50	0	1
-2518	20.76	-24.37	8.50	0	1	-2517	36.94	-22.09	8.40	0	1	-2516	36.66	-22.09	8.40	0	1
-2515	36.23	-22.09	8.40	0	1	-2514	35.81	-22.09	8.40	0	1	-2513	35.38	-22.09	8.40	0	1
-2512	34.95	-22.51	8.40	0	1	-2511	34.95	-22.93	8.40	0	1	-2510	34.95	-23.36	8.40	0	1
-2509	34.95	-23.78	8.40	0	1	-2508	34.95	-24.20	8.40	0	1	-2507	37.09	-24.62	8.40	0	1
-2506	36.66	-24.62	8.40	0	1	-2505	36.23	-24.62	8.40	0	1	-2504	35.81	-24.62	8.40	0	1
-2503	35.38	-24.62	8.40	0	1	-2502	34.95	-24.62	8.40	0	1	-2501	36.94	-22.09	8.00	0	1
-2500	36.66	-22.09	8.00	0	1	-2499	36.23	-22.09	8.00	0	1	-2498	35.81	-22.09	8.00	0	1
-2497	35.38	-22.09	8.00	0	1	-2496	34.95	-22.09	8.00	0	1	-2495	34.95	-22.51	8.00	0	1
-2494	34.95	-22.93	8.00	0	1	-2493	34.95	-23.36	8.00	0	1	-2492	34.95	-23.78	8.00	0	1
-2491	34.95	-24.20	8.00	0	1	-2490	37.09	-24.62	8.00	0	1	-2489	36.66	-24.62	8.00	0	1
-2488	36.23	-24.62	8.00	0	1	-2487	35.81	-24.62	8.00	0	1	-2486	35.38	-24.62	8.00	0	1
-2485	34.95	-24.62	8.00	0	1	-2484	36.94	-22.09	7.50	0	1	-2483	36.66	-22.09	7.50	0	1
-2482	36.23	-22.09	7.50	0	1	-2481	35.81	-22.09	7.50	0	1	-2480	35.38	-22.09	7.50	0	1
-2479	34.95	-22.09	7.50	0	1	-2478	34.95	-22.51	7.50	0	1	-2477	34.95	-22.93	7.50	0	1

-2476	34.95	-23.36	7.50	0	1	-2475	34.95	-23.78	7.50	0	1	-2474	34.95	-24.20	7.50	0	1
-2473	37.09	-24.62	7.50	0	1	-2472	36.66	-24.62	7.50	0	1	-2471	36.23	-24.62	7.50	0	1
-2470	35.81	-24.62	7.50	0	1	-2469	35.38	-24.62	7.50	0	1	-2468	34.95	-24.62	7.50	0	1
-2467	36.94	-22.09	7.00	0	1	-2466	36.66	-22.09	7.00	0	1	-2465	36.23	-22.09	7.00	0	1
-2464	35.81	-22.09	7.00	0	1	-2463	35.38	-22.09	7.00	0	1	-2462	34.95	-22.09	7.00	0	1
-2461	34.95	-22.51	7.00	0	1	-2460	34.95	-22.93	7.00	0	1	-2459	34.95	-23.36	7.00	0	1
-2458	34.95	-23.78	7.00	0	1	-2457	34.95	-24.20	7.00	0	1	-2456	37.09	-24.62	7.00	0	1
-2455	36.66	-24.62	7.00	0	1	-2454	36.23	-24.62	7.00	0	1	-2453	35.81	-24.62	7.00	0	1
-2452	35.38	-24.62	7.00	0	1	-2451	34.95	-24.62	7.00	0	1	-2450	36.94	-22.09	6.50	0	1
-2449	36.66	-22.09	6.50	0	1	-2448	36.23	-22.09	6.50	0	1	-2447	35.81	-22.09	6.50	0	1
-2446	35.38	-22.09	6.50	0	1	-2445	34.95	-22.09	6.50	0	1	-2444	34.95	-22.51	6.50	0	1
-2443	34.95	-22.93	6.50	0	1	-2442	34.95	-23.36	6.50	0	1	-2441	34.95	-23.78	6.50	0	1
-2440	34.95	-24.20	6.50	0	1	-2439	37.09	-24.62	6.50	0	1	-2438	36.66	-24.62	6.50	0	1
-2437	36.23	-24.62	6.50	0	1	-2436	35.81	-24.62	6.50	0	1	-2435	35.38	-24.62	6.50	0	1
-2434	34.95	-24.62	6.50	0	1	-2433	36.94	-22.09	6.00	0	1	-2432	36.66	-22.09	6.00	0	1
-2431	36.23	-22.09	6.00	0	1	-2430	35.81	-22.09	6.00	0	1	-2429	35.38	-22.09	6.00	0	1
-2428	34.95	-22.09	6.00	0	1	-2427	34.95	-22.51	6.00	0	1	-2426	34.95	-22.93	6.00	0	1
-2425	34.95	-23.36	6.00	0	1	-2424	34.95	-23.78	6.00	0	1	-2423	34.95	-24.20	6.00	0	1
-2422	37.09	-24.62	6.00	0	1	-2421	36.66	-24.62	6.00	0	1	-2420	36.23	-24.62	6.00	0	1
-2419	35.81	-24.62	6.00	0	1	-2418	35.38	-24.62	6.00	0	1	-2417	34.95	-24.62	6.00	0	1
-2416	36.94	-22.09	5.50	0	1	-2415	36.66	-22.09	5.50	0	1	-2414	36.23	-22.09	5.50	0	1
-2413	35.81	-22.09	5.50	0	1	-2412	35.38	-22.09	5.50	0	1	-2411	34.95	-22.09	5.50	0	1
-2410	34.95	-22.51	5.50	0	1	-2409	34.95	-22.93	5.50	0	1	-2408	34.95	-23.36	5.50	0	1
-2407	34.95	-23.78	5.50	0	1	-2406	34.95	-24.20	5.50	0	1	-2405	37.09	-24.62	5.50	0	1
-2404	36.66	-24.62	5.50	0	1	-2403	36.23	-24.62	5.50	0	1	-2402	35.81	-24.62	5.50	0	1
-2401	35.38	-24.62	5.50	0	1	-2400	34.95	-24.62	5.50	0	1	-2399	27.76	-11.93	5.00	2	1
-2398	27.30	-11.93	5.00	2	1	-2397	26.83	-11.93	5.00	2	1	-2396	26.37	-11.93	5.00	2	1
-2395	25.91	-11.93	5.00	2	1	-2394	25.44	-11.93	5.00	2	1	-2393	44.26	-22.09	5.00	2	1
-2392	43.77	-22.09	5.00	2	1	-2391	43.28	-22.09	5.00	2	1	-2390	42.79	-22.09	5.00	2	1
-2389	42.30	-22.09	5.00	2	1	-2388	41.81	-22.09	5.00	2	1	-2387	41.32	-22.09	5.00	2	1
-2386	40.83	-22.09	5.00	2	1	-2385	40.34	-22.09	5.00	2	1	-2384	39.59	-22.09	5.00	2	1
-2383	39.34	-22.09	5.00	2	1	-2382	36.94	-22.09	5.00	2	1	-2381	36.66	-22.09	5.00	2	1
-2380	36.23	-22.09	5.00	2	1	-2379	35.81	-22.09	5.00	2	1	-2378	35.38	-22.09	5.00	2	1
-2377	14.25	-22.14	5.00	0	1	-2376	13.30	-22.14	5.00	0	1	-2375	12.35	-22.14	5.00	0	1
-2374	6.05	-22.14	5.00	0	1	-2373	6.05	-22.48	5.00	0	1	-2372	44.75	-22.51	5.00	2	1
-2371	34.95	-22.51	5.00	2	1	-2370	20.88	-22.82	5.00	2	1	-2369	14.25	-22.82	5.00	0	1
-2368	12.35	-22.82	5.00	0	1	-2367	6.05	-22.82	5.00	0	1	-2366	44.75	-22.93	5.00	2	1
-2365	34.95	-22.93	5.00	2	1	-2364	6.05	-23.15	5.00	0	1	-2363	44.75	-23.36	5.00	2	1
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-1990	41.32	-24.62	2.50	0	1	-1989	40.83	-24.62	2.50	0	1	-1988	40.34	-24.62	2.50	0	1
-1987	39.70	-24.62	2.50	0	1	-1986	37.09	-24.62	2.50	0	1	-1985	36.66	-24.62	2.50	0	1
-1984	36.23	-24.62	2.50	0	1	-1983	35.81	-24.62	2.50	0	1	-1982	35.38	-24.62	2.50	0	1
-1981	34.95	-24.62	2.50	0	1	-1980	6.05	-22.14	2.33	0	1	-1979	6.05	-22.48	2.33	0	1
-1978	6.05	-22.82	2.33	0	1	-1977	6.05	-23.15	2.33	0	1	-1976	6.05	-23.49	2.33	0	1
-1975	6.05	-23.83	2.33	0	1	-1974	6.05	-24.16	2.33	0	1	-1973	6.05	-24.50	2.33	0	1
-1972	6.05	-24.84	2.33	0	1	-1971	20.88	-22.14	2.32	0	1	-1970	20.88	-22.82	2.32	0	1
-1969	20.88	-23.49	2.32	0	1	-1968	20.88	-24.16	2.32	0	1	-1967	20.88	-24.84	2.32	0	1
-1966	27.76	-11.93	2.00	0	1	-1965	27.30	-11.93	2.00	0	1	-1964	26.83	-11.93	2.00	0	1
-1963	26.37	-11.93	2.00	0	1	-1962	25.91	-11.93	2.00	0	1	-1961	25.44	-11.93	2.00	0	1
-1960	24.98	-11.93	2.00	0	1	-1959	44.75	-22.09	2.00	0	1	-1958	44.26	-22.09	2.00	0	1
-1957	43.77	-22.09	2.00	0	1	-1956	43.28	-22.09	2.00	0	1	-1955	42.79	-22.09	2.00	0	1
-1954	42.30	-22.09	2.00	0	1	-1953	41.81	-22.09	2.00	0	1	-1952	41.32	-22.09	2.00	0	1
-1951	40.83	-22.09	2.00	0	1	-1950	40.34	-22.09	2.00	0	1	-1949	39.85	-22.09	2.00	0	1
-1948	39.59	-22.09	2.00	0	1	-1947	39.34	-22.09	2.00	0	1	-1946	36.94	-22.09	2.00	0	1
-1945	36.66	-22.09	2.00	0	1	-1944	36.23	-22.09	2.00	0	1	-1943	35.81	-22.09	2.00	0	1
-1942	35.38	-22.09	2.00	0	1	-1941	34.95	-22.09	2.00	0	1	-1940	14.25	-22.14	2.00	0	1
-1939	13.30	-22.14	2.00	0	1	-1938	12.35	-22.14	2.00	0	1	-1937	6.05	-22.14	2.00	0	1
-1936	6.05	-22.48	2.00	0	1	-1935	44.75	-22.51	2.00	0	1	-1934	34.95	-22.51	2.00	0	1
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-1930	44.75	-22.93	2.00	0	1	-1929	34.95	-22.93	2.00	0	1	-1928	6.05	-23.15	2.00	0	1
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-1918	12.35	-24.16	2.00	0	1	-1917	6.05	-24.16	2.00	0	1	-1916	44.75	-24.20	2.00	0	1
-1915	34.95	-24.20	2.00	0	1	-1914	6.05	-24.50	2.00	0	1	-1913	44.75	-24.62	2.00	0	1
-1912	44.26	-24.62	2.00	0	1	-1911	43.77	-24.62	2.00	0	1	-1910	43.28	-24.62	2.00	0	1
-1909	42.79	-24.62	2.00	0	1	-1908	42.30	-24.62	2.00	0	1	-1907	41.81	-24.62	2.00	0	1
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-1831	6.05	-22.48	1.33	0	1	-1830	6.05	-22.82	1.33	0	1	-1829	6.05	-23.15	1.33	0	1
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-1645	12.35	-22.14	0.00	0	2	-1644	6.05	-22.14	0.00	0	4	-1643	6.05	-22.48	0.00	0	4
-1642	46.25	-22.51	0.00	0	1	-1641	44.75	-22.51	0.00	0	1	-1640	34.95	-22.51	0.00	0	1
-1639	20.88	-22.82	0.00	0	4	-1638	14.25	-22.82	0.00	0	2	-1637	12.35	-22.82	0.00	0	2
-1636	6.05	-22.82	0.00	0	4	-1635	46.25	-22.93	0.00	0	1	-1634	44.75	-22.93	0.00	0	1
-1633	34.95	-22.93	0.00	0	1	-1632	6.05	-23.15	0.00	0	4	-1631	46.25	-23.36	0.00	0	1
-1630	44.75	-23.36	0.00	0	1	-1629	34.95	-23.36	0.00	0	1	-1628	20.88	-23.49	0.00	0	4
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-1624	46.25	-23.78	0.00	0	1	-1623	44.75	-23.78	0.00	0	1	-1622	34.95	-23.78	0.00	0	1
-1621	6.05	-23.83	0.00	0	4	-1620	20.88	-24.16	0.00	0	4	-1619	14.25	-24.16	0.00	0	2
-1618	12.35	-24.16	0.00	0	2	-1617	6.05	-24.16	0.00	0	4	-1616	46.25	-24.20	0.00	0	1
-1615	44.75	-24.20	0.00	0	1	-1614	34.95	-24.20	0.00	0	1	-1613	6.05	-24.50	0.00	0	4
-1612	46.25	-24.62	0.00	0	1	-1611	44.75	-24.62	0.00	0	1	-1610	44.26	-24.62	0.00	0	1
-1609	43.77	-24.62	0.00	0	1	-1608	43.28	-24.62	0.00	0	1	-1607	42.79	-24.62	0.00	0	1
-1606	42.30	-24.62	0.00	0	1	-1605	41.81	-24.62	0.00	0	1	-1604	41.32	-24.62	0.00	0	1
-1603	40.83	-24.62	0.00	0	1	-1602	40.34	-24.62	0.00	0	1	-1601	39.70	-24.62	0.00	0	1

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-1591	20.88	-24.84	0.00	0	4	-1590	14.25	-24.84	0.00	0	2	-1589	13.30	-24.84	0.00	0	2
-1588	12.35	-24.84	0.00	0	2	-1587	6.05	-24.84	0.00	0	4	-1586	46.25	-25.11	0.00	0	1
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-1273	44.75	-23.36	-1.35	0	1	-1272	34.95	-23.36	-1.35	0	1	-1271	46.25	-23.78	-1.35	0	1
-1270	44.75	-23.78	-1.35	0	1	-1269	34.95	-23.78	-1.35	0	1	-1268	46.25	-24.20	-1.35	0	1
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-1255	40.34	-24.62	-1.35	0	1	-1254	39.70	-24.62	-1.35	0	1	-1253	36.66	-24.62	-1.35	0	1
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-1249	34.95	-24.62	-1.35	0	1	-1248	34.52	-24.62	-1.35	0	1	-1247	34.08	-24.62	-1.35	0	1
-1246	33.65	-24.62	-1.35	0	1	-1245	46.25	-25.11	-1.35	0	1	-1244	33.65	-25.11	-1.35	0	1
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-705	43.72	-22.58	-3.15	1	4	-704	40.82	-22.58	-3.15	1	4	-703	43.26	-22.59	-3.15	1	4
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-507	46.40	-24.67	-3.15	1	4	-506	37.48	-24.69	-3.15	1	4	-505	33.39	-24.74	-3.15	1	4
-504	33.05	-24.81	-3.15	1	4	-503	46.55	-24.88	-3.15	1	4	-502	39.12	-24.90	-3.15	1	4
-501	38.81	-24.91	-3.15	1	4	-500	37.61	-24.92	-3.15	1	4	-499	39.42	-24.92	-3.15	1	4

-498	39.72	-24.93	-3.15	1	4	-497	38.50	-24.94	-3.15	1	4	-496	37.36	-24.94	-3.15	1	4
-495	37.85	-24.94	-3.15	1	4	-494	38.17	-24.95	-3.15	1	4	-493	40.04	-24.95	-3.15	1	4
-492	34.95	-24.97	-3.15	1	4	-491	40.40	-24.98	-3.15	1	4	-490	35.35	-24.99	-3.15	1	4
-489	34.57	-24.99	-3.15	1	4	-488	46.40	-25.00	-3.15	1	4	-487	37.08	-25.01	-3.15	1	4
-486	35.78	-25.01	-3.15	1	4	-485	40.81	-25.01	-3.15	1	4	-484	36.66	-25.02	-3.15	1	4
-483	36.22	-25.03	-3.15	1	4	-482	45.25	-25.09	-3.15	1	4	-481	45.75	-25.09	-3.15	1	4
-480	44.76	-25.11	-3.15	1	4	-479	41.80	-25.11	-3.15	1	4	-478	44.26	-25.11	-3.15	1	4
-477	43.77	-25.11	-3.15	1	4	-476	43.28	-25.11	-3.15	1	4	-475	42.79	-25.11	-3.15	1	4
-474	42.30	-25.11	-3.15	1	4	-473	46.25	-25.11	-3.15	1	4	-472	33.65	-25.11	-3.15	1	4
-471	34.18	-25.13	-3.15	1	4	-470	41.28	-25.13	-3.15	1	4	-469	37.49	-25.14	-3.15	1	4
-468	39.11	-25.21	-3.15	1	4	-467	39.42	-25.21	-3.15	1	4	-466	33.36	-25.21	-3.15	1	4
-465	38.82	-25.22	-3.15	1	4	-464	39.71	-25.22	-3.15	1	4	-463	37.80	-25.23	-3.15	1	4
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-459	38.52	-25.28	-3.15	1	4	-458	40.03	-25.28	-3.15	1	4	-457	38.15	-25.28	-3.15	1	4
-456	40.38	-25.29	-3.15	1	4	-455	33.05	-25.30	-3.15	1	4	-454	46.40	-25.32	-3.15	1	4
-453	40.75	-25.32	-3.15	1	4	-452	41.04	-25.35	-3.15	1	4	-451	35.29	-25.35	-3.15	1	4
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-447	36.20	-25.43	-3.15	1	4	-446	39.70	-25.44	-3.15	1	4	-445	38.84	-25.45	-3.15	1	4
-444	36.68	-25.45	-3.15	1	4	-443	34.41	-25.46	-3.15	1	4	-442	39.43	-25.47	-3.15	1	4
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-402	40.12	-26.04	-3.15	1	4	-401	41.66	-26.04	-3.15	1	4	-400	38.09	-26.04	-3.15	1	4
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-195	37.05	-29.16	-3.15	1	4	-194	39.46	-29.17	-3.15	1	4	-193	37.53	-29.17	-3.15	1	4
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-180	43.82	-29.58	-3.15	1	4	-179	43.33	-29.58	-3.15	1	4	-178	42.85	-29.58	-3.15	1	4
-177	34.62	-29.58	-3.15	1	4	-176	42.36	-29.59	-3.15	1	4	-175	35.11	-29.59	-3.15	1	4
-174	41.88	-29.59	-3.15	1	4	-173	41.40	-29.60	-3.15	1	4	-172	35.59	-29.60	-3.15	1	4
-171	40.91	-29.61	-3.15	1	4	-170	36.08	-29.61	-3.15	1	4	-169	40.43	-29.62	-3.15	1	4
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-159	33.05	-29.70	-3.15	1	4	-158	46.55	-29.71	-3.15	1	4	-157	46.25	-30.06	-3.15	1	4
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-129	33.05	-30.18	-3.15	1	4	-128	46.55	-30.20	-3.15	1	4	-127	46.25	-30.56	-3.15	1	4
-126	33.65	-30.56	-3.15	1	4	-125	45.76	-30.56	-3.15	1	4	-124	45.28	-30.56	-3.15	1	4
-123	34.14	-30.56	-3.15	1	4	-122	44.79	-30.56	-3.15	1	4	-121	44.31	-30.56	-3.15	1	4
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-108	36.56	-30.57	-3.15	1	4	-107	39.95	-30.57	-3.15	1	4	-106	37.04	-30.58	-3.15	1	4
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-102	38.50	-30.58	-3.15	1	4	-101	38.01	-30.58	-3.15	1	4	-100	33.36	-30.62	-3.15	1	4
-99	33.05	-30.67	-3.15	1	4	-98	46.55	-30.68	-3.15	1	4	-97	46.25	-31.05	-3.15	1	4
-96	45.77	-31.05	-3.15	1	4	-95	45.28	-31.05	-3.15	1	4	-94	44.80	-31.05	-3.15	1	4
-93	44.31	-31.05	-3.15	1	4	-92	43.83	-31.05	-3.15	1	4	-91	43.34	-31.05	-3.15	1	4
-90	42.86	-31.05	-3.15	1	4	-89	42.37	-31.05	-3.15	1	4	-88	41.89	-31.05	-3.15	1	4
-87	41.40	-31.05	-3.15	1	4	-86	40.92	-31.05	-3.15	1	4	-85	40.43	-31.05	-3.15	1	4
-84	39.95	-31.05	-3.15	1	4	-83	39.47	-31.05	-3.15	1	4	-82	38.98	-31.05	-3.15	1	4
-81	38.50	-31.05	-3.15	1	4	-80	38.01	-31.05	-3.15	1	4	-79	37.53	-31.05	-3.15	1	4
-78	37.04	-31.05	-3.15	1	4	-77	36.56	-31.05	-3.15	1	4	-76	36.07	-31.05	-3.15	1	4
-75	35.59	-31.05	-3.15	1	4	-74	35.10	-31.05	-3.15	1	4	-73	34.62	-31.05	-3.15	1	4
-72	34.13	-31.05	-3.15	1	4	-71	33.65	-31.05	-3.15	1	4	-70	33.40	-31.12	-3.15	1	4
-69	33.05	-31.16	-3.15	1	4	-68	46.55	-31.17	-3.15	1	4	-67	45.95	-31.21	-3.15	1	4
-66	45.45	-31.22	-3.15	1	4	-65	46.17	-31.24	-3.15	1	4	-64	45.69	-31.26	-3.15	1	4
-63	44.79	-31.29	-3.15	1	4	-62	46.35	-31.29	-3.15	1	4	-61	45.14	-31.29	-3.15	1	4

-60	44.40	-31.33	-3.15	1	4	-59	45.90	-31.34	-3.15	1	4	-58	43.93	-31.35	-3.15	1	4
-57	43.44	-31.35	-3.15	1	4	-56	42.95	-31.35	-3.15	1	4	-55	42.46	-31.35	-3.15	1	4
-54	41.97	-31.35	-3.15	1	4	-53	41.48	-31.35	-3.15	1	4	-52	40.98	-31.35	-3.15	1	4
-51	40.49	-31.35	-3.15	1	4	-50	40.00	-31.35	-3.15	1	4	-49	39.51	-31.35	-3.15	1	4
-48	39.02	-31.35	-3.15	1	4	-47	38.52	-31.35	-3.15	1	4	-46	38.03	-31.35	-3.15	1	4
-45	37.54	-31.35	-3.15	1	4	-44	37.05	-31.35	-3.15	1	4	-43	36.55	-31.35	-3.15	1	4
-42	36.06	-31.35	-3.15	1	4	-41	35.57	-31.35	-3.15	1	4	-40	35.08	-31.35	-3.15	1	4
-39	34.60	-31.35	-3.15	1	4	-38	34.14	-31.35	-3.15	1	4	-37	33.78	-31.35	-3.15	1	4
-36	45.39	-31.36	-3.15	1	4	-35	46.11	-31.42	-3.15	1	4	-34	45.62	-31.44	-3.15	1	4
-33	46.34	-31.45	-3.15	1	4	-32	44.81	-31.47	-3.15	1	4	-31	45.09	-31.48	-3.15	1	4
-30	45.86	-31.48	-3.15	1	4	-29	45.35	-31.50	-3.15	1	4	-28	46.55	-31.65	-3.15	1	4
-27	46.05	-31.65	-3.15	1	4	-26	45.55	-31.65	-3.15	1	4	-25	45.05	-31.65	-3.15	1	4
-24	44.55	-31.65	-3.15	1	4	-23	44.05	-31.65	-3.15	1	4	-22	43.55	-31.65	-3.15	1	4
-21	43.05	-31.65	-3.15	1	4	-20	42.55	-31.65	-3.15	1	4	-19	42.05	-31.65	-3.15	1	4
-18	41.55	-31.65	-3.15	1	4	-17	41.05	-31.65	-3.15	1	4	-16	40.55	-31.65	-3.15	1	4
-15	40.05	-31.65	-3.15	1	4	-14	39.55	-31.65	-3.15	1	4	-13	39.05	-31.65	-3.15	1	4
-12	38.55	-31.65	-3.15	1	4	-11	38.05	-31.65	-3.15	1	4	-10	37.55	-31.65	-3.15	1	4
-9	37.05	-31.65	-3.15	1	4	-8	36.55	-31.65	-3.15	1	4	-7	36.05	-31.65	-3.15	1	4
-6	35.55	-31.65	-3.15	1	4	-5	35.05	-31.65	-3.15	1	4	-4	34.55	-31.65	-3.15	1	4
-3	34.05	-31.65	-3.15	1	4	-2	33.55	-31.65	-3.15	1	4	-1	33.05	-31.65	-3.15	1	4
1	24.98	-22.09	0.00	0	2	2	29.91	-22.09	0.00	0	2	6	24.98	-17.01	0.00	0	2
7	29.91	-17.01	0.00	0	2	8	34.95	-17.01	0.00	0	2	9	39.85	-17.01	0.00	0	2
10	44.75	-17.01	0.00	0	2	11	20.88	-11.93	0.00	0	3	12	24.98	-11.93	0.00	0	4
13	29.91	-11.93	0.00	0	2	14	34.95	-11.93	0.00	0	2	15	39.85	-11.93	0.00	0	2
16	44.75	-11.93	0.00	0	2	201	24.98	-22.09	5.00	2	1	202	29.91	-22.09	5.00	2	1
203	34.95	-22.09	5.00	2	1	204	39.85	-22.09	5.00	2	1	205	44.75	-22.09	5.00	2	1
206	24.98	-17.01	5.00	2	1	207	29.91	-17.01	5.00	2	1	208	34.95	-17.01	5.00	2	1
209	39.85	-17.01	5.00	2	1	210	44.75	-17.01	5.00	2	1	211	20.88	-11.93	5.00	2	1
212	24.98	-11.93	5.00	2	1	213	29.91	-11.93	5.00	2	1	214	34.95	-11.93	5.00	2	1
215	39.85	-11.93	5.00	2	1	216	44.75	-11.93	5.00	2	1	217	39.70	-24.62	5.00	2	1
218	20.88	-22.14	5.00	2	1	301	24.98	-22.09	10.20	0	1	302	29.91	-22.09	10.20	0	1
303	34.95	-22.09	8.40	0	1	304	39.85	-22.09	10.20	0	1	305	44.75	-22.09	10.20	0	1
312	24.98	-11.93	8.75	0	1	313	29.91	-11.93	8.75	0	1	314	34.95	-11.93	8.75	0	1
315	39.85	-11.93	8.75	0	1	316	44.75	-11.93	8.75	0	1	317	20.76	-11.93	8.75	0	1
318	47.38	-11.93	8.75	0	1	319	20.76	-22.09	10.20	0	1	320	34.95	-22.09	10.20	0	1
321	47.38	-22.09	10.20	0	1	322	20.76	-16.53	14.35	0	1	323	24.98	-16.53	14.35	0	1
324	29.91	-16.53	14.35	0	1	325	34.95	-16.53	14.35	0	1	326	39.85	-16.53	14.35	0	1
327	44.75	-16.53	14.35	0	1	328	47.38	-16.53	14.35	0	1						

ELENCO MATERIALI

Simbologia

Mat. = Numero del materiale
Comm. = Commento
P = Peso specifico
E = Modulo elastico
G = Modulo elastico tangenziale
ν = Coeff. di Poisson
α = Coeff. di dilatazione termica

Mat.	Comm.	P <daN/mc>	E <daN/cmq>	G <daN/cmq>	ν	α
1	Calcestruzzo	2500	300000.00	130000.00	0.1	1.000000E-05
2	Acciaio	7850	2100000.00	800000.00	0.3	1.000000E-05
6	MURATURA	1500	8000.00	1300.00	0.2	0.02

ELENCO SEZIONI ASTE

Simbologia

Sez. = Numero della sezione
Comm. = Commento
Tipo = Tipologia
2C = Doppia C lato labbri
2Cdx = Doppia C lato costola
2I = Doppia I

2L = Doppia L lato labbri
2Ldx = Doppia L lato costole
C = Sezione a C
Cdx = C destra
Cir. = Circolare
Cir.c = Circolare cava
I = Sezione a I
L = Sezione a L
Ldx = L destra
Om. = Omega
Pg = Pi greco
Pr = Poligono regolare
Prc = Poligono regolare cavo
Pc = Per coordinate
Ia = Inerzie assegnate
R = Rettangolare
Rc = Rettangolare cava
T = Sezione a T
U = Sezione a U
Ur = U rovescia
V = Sezione a V
Vr = V rovescia
Z = Sezione a Z
Zdx = Z destra
Ts = T stondata
Ls = L stondata
Cs = C stondata
Is = I stondata
Dis. = Disegnata

Mem. = Membratura
G = Generica
T = Trave
P = Pilastro

Ver. = Verifica prevista
N = Nessuna
C = Cemento armato
A = Acciaio
L = Legno

B = Base
b = Base inferiore
H = Altezza
h = Altezza parte inf.
s = Spessore ala
a = Spessore anima
r = Raggio raccordo anima-ala
r1 = Raggio in testa ala
D = Distanza
Ma = Numero del materiale
C = Numero del criterio di progetto
Crit. C.I. = Criterio di progetto collegamento iniziale
Crit. C.F. = Criterio di progetto collegamento finale

Sez.	Comm.	Tipo	Mem.	Ver.	B <cm>	b <cm>	H <cm>	h <cm>	s <cm>	a <cm>	r <cm>	r1 <cm>	D <cm>	Ma	C	Crit. C.I.	Crit. C.F.
3		R	T	C	30.00		35.00							1	6		
4	HEA200	Is	T	A	20.00		19.00		1.00	0.60	1.80	0.00		2	1	2	2
5	T12X25	R	T	C	12.00		25.00							1	5		
7	T30X40	R	T	C	30.00		40.00							1	5		
8	HEB300	Is	P	A	30.00		30.00		1.90	1.10	2.70	0.00		2	1	1	1
9	HEA260	Is	T	A	26.00		25.00		1.25	0.75	2.40	0.00		2	1	2	2
11	HEA360	Is	G	A	30.00		35.00		1.75	1.00	2.70	0.00		2	1	2	2
12	HEA160	Is	T	A	16.00		15.20		0.90	0.60	1.50	0.00		2	1	2	2
14	2HEA160	2I	T	A	16.00		15.20		0.90	0.60	1.50	0.00	0.00	2	1	2	2
16	P40X40	R	P	C	40.00		40.00							1	5		

18	HEA240	Is	T	A	24.00		23.00		1.20	0.75	2.10	0.00	2	2		2
2																
19	treave fond 20	T	T	C	40.00	130.00	70.00	30.00					1	6		
20		R	T	C	30.00		30.00						1	1		
21		R	P	C	80.00		40.00						1	5		
22	HEA400	Is	T	A	30.00		39.00		1.90	1.10	2.70	0.00	2	2		2
2																

ELENCO VINCOLI ASTE

Simbologia

Va = Numero del vincolo asta
Comm. = Commento
Tipo = Tipologia
SVI = Definizione di vincolamenti interni
ELA = Vincolo su suolo elastico alla Winkler
BIE-RTC = Biella resistente a trazione e a compressione
BIE-RC = Biella resistente solo a compressione
BIE-RT = Biella resistente solo a trazione
Ni = Sforzo normale nodo iniziale (0=sbloccato, 1=bloccato)
Tyi = Taglio in dir. Y locale nodo iniziale (0=sbloccato, 1=bloccato)
Tzi = Taglio in dir. Z locale nodo iniziale (0=sbloccato, 1=bloccato)
Mxi = Momento intorno all'asse X locale nodo iniziale (0=sbloccato, 1=bloccato)
Myi = Momento intorno all'asse Y locale nodo iniziale (0=sbloccato, 1=bloccato)
Mzi = Momento intorno all'asse Z locale nodo iniziale (0=sbloccato, 1=bloccato)
Nf = Sforzo normale nodo finale (0=sbloccato, 1=bloccato)
Tyf = Taglio in dir. Y locale nodo finale (0=sbloccato, 1=bloccato)
Tzf = Taglio in dir. Z locale nodo finale (0=sbloccato, 1=bloccato)
Mxf = Momento intorno all'asse X locale nodo finale (0=sbloccato, 1=bloccato)
Myf = Momento intorno all'asse Y locale nodo finale (0=sbloccato, 1=bloccato)
Mzf = Momento intorno all'asse Z locale nodo finale (0=sbloccato, 1=bloccato)
Kt = Coeff. di sottofondo su suolo elastico alla Winkler

Va	Comm.	Tipo	Ni	Tyi	Tzi	Mxi	Myi	Mzi	Nf	Tyf	Tzf	Mxf	Myf	Mzf	Kt <daN/cmc>
1	Inc+Inc	SVI	1	1	1	1	1	1	1	1	1	1	1	1	
2	Inc+Cer	SVI	1	1	1	1	1	1	1	1	1	0	0	0	
3	Cer+Inc	SVI	1	1	1	0	0	0	1	1	1	1	1	1	
5	Inc+CerY	SVI	1	1	1	1	1	1	1	1	1	1	0	1	
6	CerY+Inc	SVI	1	1	1	1	0	1	1	1	1	1	1	1	
7	CerY+CerY	SVI	1	1	1	1	0	1	1	1	1	1	0	1	
31	winkler aste	ELA													f(strat.)

ELENCO ASTE

Simbologia

Asta = Numero dell'asta
N1 = Nodo iniziale
N2 = Nodo finale
Sez. = Numero della sezione
Va = Numero del vincolo asta
Par. = Numero dei parametri aggiuntivi
Rot. = Rotazione
FF = Filo fisso
Dy1 = Scost. filo fisso Y1
Dy2 = Scost. filo fisso Y2
Dz1 = Scost. filo fisso Z1
Dz2 = Scost. filo fisso Z2
TC1 = Tipo collegamento iniziale
TC2 = Tipo collegamento finale
Kt = Coeff. di sottofondo su suolo elastico alla Winkler

Asta	N1	N2	Sez.	Va	Par.	Rot. <grad>	FF	Dy1 <cm>	Dy2 <cm>	Dz1 <cm>	Dz2 <cm>	TC1	TC2	Kt <daN/cmc>
0	-2327	-2348	1			0.00	11	0.00	0.00	0.00	0.00	ND	ND	

0	-2348	-2351	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2351	-2355	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2355	-2358	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2358	-2364	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2364	-2367	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2367	-2373	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2373	-2374	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2327	-2328	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2374	-2375	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2352	-2328	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2359	-2352	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2368	-2359	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2353	-2330	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2375	-2368	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2360	-2353	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2369	-2360	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2377	-2369	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2331	-2330	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2377	218	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2179	-2180	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2180	-2181	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2331	-2354	1	0.00	22	0.00	0.00	0.00	0.00	ND	ND
0	-2181	-2182	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2354	-2361	1	0.00	22	0.00	0.00	0.00	0.00	ND	ND
0	-2182	-2183	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2361	-2370	1	0.00	22	0.00	0.00	0.00	0.00	ND	ND
0	-2370	218	1	0.00	22	0.00	0.00	0.00	0.00	ND	ND
0	-1536	-1537	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1563	-1536	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2331	-2332	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1537	-1538	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1565	-1563	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1538	-1539	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1567	-1565	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1539	-1540	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1569	-1567	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1540	-1541	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1571	-1569	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1541	-1542	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1573	-1571	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1542	-1543	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	218	203	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
0	-1575	-1573	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1543	-1544	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1577	-1575	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1544	-1545	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1579	-1577	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1545	-1546	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1581	-1579	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1546	-1547	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1583	-1581	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1547	-1548	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1585	-1583	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1548	-1549	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1592	-1585	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1549	-1550	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1593	-1592	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1550	-1551	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1594	-1593	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1551	-1552	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1595	-1594	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1595	-1614	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1596	-1595	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1614	-1622	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1597	-1596	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1553	-1554	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1622	-1629	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1598	-1597	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1599	-1598	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1633	-1640	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1601	-2580	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2332	-2333	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1552	-1553	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND

0	-1600	-1599	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1653	-1654	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2333	-2334	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1554	-1555	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1629	-1633	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1555	-1556	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1640	-1649	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1649	-1650	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1651	-1652	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1652	-1653	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1654	-1655	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1655	-1656	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1601	-1661	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1660	-1661	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2356	-2349	1	0.00	22	0.00	0.00	0.00	0.00	ND	ND
0	-2365	-2362	1	0.00	22	0.00	0.00	0.00	0.00	ND	ND
0	-1556	-1557	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1657	-1658	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2349	-2332	1	0.00	22	0.00	0.00	0.00	0.00	ND	ND
0	-2362	-2356	1	0.00	22	0.00	0.00	0.00	0.00	ND	ND
0	-2335	-2336	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1557	-1558	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1650	-1651	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2371	-2365	1	0.00	22	0.00	0.00	0.00	0.00	ND	ND
0	-2336	-2337	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	203	-2371	1	0.00	22	0.00	0.00	0.00	0.00	ND	ND
0	203	-2378	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2502	-2503	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1558	-1559	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1560	-1561	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2580	-1602	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1602	-1603	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2378	-2379	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2379	-2380	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1566	-1564	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1656	-1657	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2334	-2335	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1603	-1604	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1604	-1605	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1659	-1660	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2381	-2382	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1605	-1606	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1606	-1607	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1607	-1608	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1662	-1663	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1663	-1664	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2380	-2381	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2509	-2508	1	0.00	22	0.00	0.00	0.00	0.00	ND	ND
0	-2503	-2504	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2510	-2509	1	0.00	22	0.00	0.00	0.00	0.00	ND	ND
0	-2504	-2505	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2505	-2506	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1561	-1562	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1658	-1659	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1661	-1662	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1664	-1665	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	303	-2512	1	0.00	22	0.00	0.00	0.00	0.00	ND	ND
0	-1559	-1560	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	217	-2590	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1564	-1562	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	217	204	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1568	-1566	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1572	-1570	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1574	-1572	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1608	-1609	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1665	-1666	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1666	-1667	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2508	-2502	1	0.00	22	0.00	0.00	0.00	0.00	ND	ND
0	-2511	-2510	1	0.00	22	0.00	0.00	0.00	0.00	ND	ND
0	-2512	-2511	1	0.00	22	0.00	0.00	0.00	0.00	ND	ND
0	-1610	-1611	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2590	-2338	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2339	-2340	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND

0	-1570	-1568		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2384	204		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1576	-1574		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1578	-1576		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1609	-1610		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1580	-1578		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1582	-1580		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1611	-1615		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1584	-1582		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1615	-1623		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1611	-1612		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1667	-1668		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1623	-1630		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1668	-1669		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1616	-1612		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1669	-1670		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2383	-2384		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1630	-1634		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1634	-1641		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1641	-1671		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	204	-2385		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2506	-2507		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2338	-2339		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1612	-1586		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1624	-1616		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1670	-1671		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1631	-1624		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1671	-1672		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1672	-1673		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-1673	-1674		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2340	-2341		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2386	-2387		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1635	-1631		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1674	-1642		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2342	-2343		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2343	-2344		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2385	-2386		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1586	-1584		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-1642	-1635		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2341	-2342		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2344	-2345		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2345	-2346		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2387	-2388		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2346	-2347		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2388	-2389		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2347	-2350		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2389	-2390		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2350	-2357		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2390	-2391		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2357	-2363		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2391	-2392		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2363	-2366		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2392	-2393		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2366	-2372		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
0	-2393	205		1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
0	-2372	205		1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
1	1	201	16	1	270.00	77	0.00	0.00	0.00	0.00	ND	ND
2	2	202	16	1	270.00	88	0.00	0.00	0.00	0.00	ND	ND
3	203	-2411	8	1	270.00	88	0.00	0.00	0.00	0.00	ND	ND
3	-2411	-2428	8	1	270.00	88	0.00	0.00	0.00	0.00	ND	ND
3	-2428	-2445	8	1	270.00	88	0.00	0.00	0.00	0.00	ND	ND
3	-2445	-2462	8	1	270.00	88	0.00	0.00	0.00	0.00	ND	ND
3	-2462	-2479	8	1	270.00	88	0.00	0.00	0.00	0.00	ND	ND
3	-2479	-2496	8	1	270.00	88	0.00	0.00	0.00	0.00	ND	ND
3	-2496	303	8	1	270.00	88	0.00	0.00	0.00	0.00	ND	ND
3	303	320	8	1	270.00	88	0.00	0.00	0.00	0.00	ND	ND
4	204	304	8	1	270.00	88	0.00	0.00	0.00	0.00	PF	ND
5	205	305	8	1	270.00	88	0.00	0.00	0.00	0.00	PF	ND
6	6	206	16	1	90.00	55	-15.00	-15.00	0.00	0.00	ND	ND
7	7	207	16	1	90.00	55	0.00	0.00	0.00	0.00	ND	ND
8	8	208	16	1	90.00	55	0.00	0.00	0.00	0.00	ND	ND
9	9	209	16	1	90.00	55	0.00	0.00	0.00	0.00	ND	ND
10	10	210	16	1	90.00	55	0.00	0.00	0.00	0.00	ND	ND

11	11	211	21	1	90.00	11	0.00	0.00	0.00	0.00	ND	ND
12	12	-1817	16	1	90.00	33	0.00	0.00	0.00	0.00	ND	ND
12	-1817	-1960	16	1	90.00	33	0.00	0.00	0.00	0.00	ND	ND
12	-1960	-2103	16	1	90.00	33	0.00	0.00	0.00	0.00	ND	ND
12	-2103	-2251	16	1	90.00	33	0.00	0.00	0.00	0.00	ND	ND
12	-2251	212	16	1	90.00	33	0.00	0.00	0.00	0.00	ND	ND
13	13	213	16	1	90.00	22	0.00	0.00	0.00	0.00	ND	ND
14	214	314	8	1	90.00	22	0.00	0.00	0.00	0.00	PF	ND
15	15	215	16	1	90.00	22	0.00	0.00	0.00	0.00	ND	ND
16	16	216	16	1	90.00	22	0.00	0.00	0.00	0.00	ND	ND
17	215	315	8	1	90.00	22	0.00	0.00	0.00	0.00	PF	ND
18	202	302	8	1	270.00	88	0.00	0.00	0.00	0.00	PF	ND
19	201	301	8	1	270.00	77	0.00	0.00	0.00	0.00	PF	ND
20	212	312	8	1	90.00	33	0.00	0.00	0.00	0.00	PF4	CA
21	216	316	8	1	90.00	22	0.00	0.00	0.00	0.00	PF	ND
22	213	313	8	1	90.00	22	0.00	0.00	0.00	0.00	PF	ND
23	14	214	16	1	90.00	22	0.00	0.00	0.00	0.00	ND	ND
201	-2337	217	20	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
204	-2382	-2383	20	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
212	211	212	3	7	0.00	11	0.00	0.00	0.00	0.00	ND	ND
212	-2394	212	3	5	0.00	33	0.00	0.00	0.00	0.00	ND	ND
212	-2395	-2394	3	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
212	-2396	-2395	3	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
212	-2397	-2396	3	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
212	-2398	-2397	3	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
212	-2399	-2398	3	1	0.00	33	0.00	0.00	0.00	0.00	ND	ND
212	213	214	3	7	0.00	11	0.00	0.00	0.00	0.00	ND	ND
212	214	215	3	7	0.00	11	0.00	0.00	0.00	0.00	ND	ND
212	215	216	3	7	0.00	11	0.00	0.00	0.00	0.00	ND	ND
215	218	211	22	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND
216	206	201	18	7	0.00	11	0.00	0.00	0.00	0.00	PF	PF
216	212	206	18	7	0.00	11	0.00	0.00	0.00	0.00	PF	PF
217	207	202	18	7	0.00	22	0.00	0.00	0.00	0.00	ND	ND
217	213	207	18	7	0.00	22	0.00	0.00	0.00	0.00	PF	ND
218	208	203	18	7	0.00	22	0.00	0.00	0.00	0.00	ND	ND
218	214	208	18	7	0.00	22	0.00	0.00	0.00	0.00	ND	ND
219	209	204	18	7	0.00	22	0.00	0.00	0.00	0.00	ND	ND
219	215	209	18	7	0.00	22	0.00	0.00	0.00	0.00	ND	ND
220	210	205	18	7	0.00	22	0.00	0.00	0.00	0.00	ND	ND
220	216	210	18	7	0.00	22	0.00	0.00	0.00	0.00	ND	ND
222	201	202	20	7	0.00	11	0.00	0.00	0.00	0.00	ND	ND
222	202	203	20	7	0.00	11	0.00	0.00	0.00	0.00	ND	ND
300	213	-2399	3	6	0.00	33	0.00	0.00	0.00	0.00	ND	ND
302	-2518	-2519	14	3	37.00	88	0.00	0.00	0.00	0.00	ND	ND
302	-2519	-2520	14	2	37.00	88	0.00	0.00	0.00	0.00	ND	ND
302	-2520	-2521	12	3	37.00	88	0.00	0.00	0.00	0.00	ND	ND
302	-2521	-2522	12	2	37.00	88	0.00	0.00	0.00	0.00	ND	ND
302	-2522	-2523	12	3	37.00	88	0.00	0.00	0.00	0.00	ND	ND
302	-2523	-2524	12	2	37.00	88	0.00	0.00	0.00	0.00	ND	ND
303	-2525	-2526	14	3	37.00	88	0.00	0.00	0.00	0.00	ND	ND
303	-2526	-2527	14	2	37.00	88	0.00	0.00	0.00	0.00	ND	ND
303	-2527	-2528	12	3	37.00	88	0.00	0.00	0.00	0.00	ND	ND
303	-2528	-2529	12	2	37.00	88	0.00	0.00	0.00	0.00	ND	ND
303	-2529	-2530	12	3	37.00	88	0.00	0.00	0.00	0.00	ND	ND
303	-2530	-2531	12	2	37.00	88	0.00	0.00	0.00	0.00	ND	ND
304	301	302	9	7	0.00	11	0.00	0.00	0.00	0.00	ND	ND
304	302	320	9	7	0.00	11	0.00	0.00	0.00	0.00	ND	ND
304	320	304	9	7	0.00	11	0.00	0.00	0.00	0.00	ND	ND
304	304	305	9	7	0.00	11	0.00	0.00	0.00	0.00	ND	ND
305	-2532	-2533	14	3	37.00	88	0.00	0.00	0.00	0.00	ND	ND
305	-2533	-2534	14	2	37.00	88	0.00	0.00	0.00	0.00	ND	ND
305	-2534	-2535	12	3	37.00	88	0.00	0.00	0.00	0.00	ND	ND
305	-2535	-2536	12	2	37.00	88	0.00	0.00	0.00	0.00	ND	ND
305	-2536	-2537	12	3	37.00	88	0.00	0.00	0.00	0.00	ND	ND
305	-2537	-2538	12	2	37.00	88	0.00	0.00	0.00	0.00	ND	ND
306	-2546	-2547	14	3	37.00	88	0.00	0.00	0.00	0.00	ND	ND
306	-2547	-2548	14	2	37.00	88	0.00	0.00	0.00	0.00	ND	ND
306	-2548	-2549	12	3	37.00	88	0.00	0.00	0.00	0.00	ND	ND
306	-2549	-2550	12	2	37.00	88	0.00	0.00	0.00	0.00	ND	ND
306	-2550	-2551	12	3	37.00	88	0.00	0.00	0.00	0.00	ND	ND
306	-2551	-2552	12	2	37.00	88	0.00	0.00	0.00	0.00	ND	ND
307	-2553	-2554	14	3	37.00	88	0.00	0.00	0.00	0.00	ND	ND
307	-2554	-2555	14	2	37.00	88	0.00	0.00	0.00	0.00	ND	ND

307	-2555	-2556	12	3	37.00	88	0.00	0.00	0.00	0.00	ND	ND
307	-2556	-2557	12	2	37.00	88	0.00	0.00	0.00	0.00	ND	ND
307	-2557	-2558	12	3	37.00	88	0.00	0.00	0.00	0.00	ND	ND
307	-2558	-2559	12	2	37.00	88	0.00	0.00	0.00	0.00	ND	ND
308	-2567	-2568	14	3	37.00	88	0.00	0.00	0.00	0.00	ND	ND
308	-2568	-2569	14	2	37.00	88	0.00	0.00	0.00	0.00	ND	ND
308	-2569	-2570	12	3	37.00	88	0.00	0.00	0.00	0.00	ND	ND
308	-2570	-2571	12	2	37.00	88	0.00	0.00	0.00	0.00	ND	ND
308	-2571	-2572	12	3	37.00	88	0.00	0.00	0.00	0.00	ND	ND
308	-2572	-2573	12	2	37.00	88	0.00	0.00	0.00	0.00	ND	ND
309	322	323	14	3	0.00	88	0.00	0.00	0.00	0.00	ND	ND
309	323	324	14	2	0.00	88	0.00	0.00	0.00	0.00	ND	ND
309	324	325	14	3	0.00	88	0.00	0.00	0.00	0.00	ND	ND
309	325	326	14	2	0.00	88	0.00	0.00	0.00	0.00	ND	ND
309	326	327	14	3	0.00	88	0.00	0.00	0.00	0.00	ND	ND
309	327	328	14	2	0.00	88	0.00	0.00	0.00	0.00	ND	ND
310	-2560	-2561	14	3	309.00	88	0.00	0.00	0.00	0.00	CF	CF
310	-2561	-2562	14	2	309.00	88	0.00	0.00	0.00	0.00	CF	CF
310	-2562	-2563	12	3	309.00	88	0.00	0.00	0.00	0.00	FESI	FESI
310	-2563	-2564	12	2	309.00	88	0.00	0.00	0.00	0.00	CA	CA
310	-2564	-2565	12	3	309.00	88	0.00	0.00	0.00	0.00	ND	ND
310	-2565	-2566	12	2	309.00	88	0.00	0.00	0.00	0.00	ND	ND
311	-2539	-2540	14	3	309.00	88	0.00	0.00	0.00	0.00	CF	CF
311	-2540	-2541	14	2	309.00	88	0.00	0.00	0.00	0.00	CF	CF
311	-2541	-2542	12	3	309.00	88	0.00	0.00	0.00	0.00	FESI	FESI
311	-2542	-2543	12	2	309.00	88	0.00	0.00	0.00	0.00	CA	CA
311	-2543	-2544	12	3	309.00	88	0.00	0.00	0.00	0.00	ND	ND
311	-2544	-2545	12	2	309.00	88	0.00	0.00	0.00	0.00	ND	ND
312	317	312	14	3	309.00	88	0.00	0.00	0.00	0.00	FESI	FESI
312	312	313	14	2	309.00	88	0.00	0.00	0.00	0.00	CF	CF
312	313	314	12	3	309.00	88	0.00	0.00	0.00	0.00	CF	CF
312	314	315	12	2	309.00	88	0.00	0.00	0.00	0.00	ND	ND
312	315	316	12	3	309.00	88	0.00	0.00	0.00	0.00	ND	ND
312	316	318	12	2	309.00	88	0.00	0.00	0.00	0.00	ND	ND
314	-2525	-2518	12	1	0.00	77	0.00	0.00	0.00	0.00	ND	ND
314	319	-2525	12	1	0.00	77	0.00	0.00	0.00	0.00	ND	ND
314	-2532	319	12	1	0.00	77	0.00	0.00	0.00	0.00	ND	ND
314	-2546	-2532	12	1	0.00	77	0.00	0.00	0.00	0.00	ND	ND
314	-2553	-2546	12	1	0.00	77	0.00	0.00	0.00	0.00	ND	ND
314	-2567	-2553	12	1	0.00	77	0.00	0.00	0.00	0.00	ND	ND
314	322	-2567	12	1	0.00	77	0.00	0.00	0.00	0.00	ND	ND
316	-2526	-2519	11	1	0.00	77	0.00	0.00	0.00	0.00	ND	ND
316	301	-2526	11	1	0.00	77	0.00	0.00	0.00	0.00	ND	ND
316	-2533	301	11	1	0.00	77	0.00	0.00	0.00	0.00	ND	ND
316	-2547	-2533	11	1	0.00	77	0.00	0.00	0.00	0.00	ND	ND
316	-2554	-2547	11	1	0.00	77	0.00	0.00	0.00	0.00	ND	ND
316	-2568	-2554	11	1	0.00	77	0.00	0.00	0.00	0.00	ND	ND
316	323	-2568	11	1	0.00	77	0.00	0.00	0.00	0.00	ND	ND
317	-2527	-2520	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
317	302	-2527	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
317	-2534	302	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
317	-2548	-2534	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
317	-2555	-2548	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
317	-2569	-2555	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
317	324	-2569	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
318	-2528	-2521	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
318	320	-2528	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
318	-2535	320	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
318	-2549	-2535	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
318	-2556	-2549	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
318	-2570	-2556	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
318	325	-2570	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
319	-2529	-2522	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
319	304	-2529	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
319	-2536	304	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
319	-2550	-2536	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
319	-2557	-2550	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
319	-2571	-2557	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
319	326	-2571	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
320	-2530	-2523	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
320	305	-2530	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
320	-2537	305	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND
320	-2551	-2537	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND

320	-2558	-2551	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND		
320	-2572	-2558	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND		
320	327	-2572	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND		
321	-2531	-2524	12	1	0.00	99	0.00	0.00	0.00	0.00	ND	ND		
321	321	-2531	12	1	0.00	99	0.00	0.00	0.00	0.00	ND	ND		
321	-2538	321	12	1	0.00	99	0.00	0.00	0.00	0.00	ND	ND		
321	-2552	-2538	12	1	0.00	99	0.00	0.00	0.00	0.00	ND	ND		
321	-2559	-2552	12	1	0.00	99	0.00	0.00	0.00	0.00	ND	ND		
321	-2573	-2559	12	1	0.00	99	0.00	0.00	0.00	0.00	ND	ND		
321	328	-2573	12	1	0.00	99	0.00	0.00	0.00	0.00	ND	ND		
336	317	-2539	12	1	0.00	77	0.00	0.00	8.00	8.00	ND	ND		
336	-2539	-2560	12	1	0.00	77	0.00	0.00	8.00	8.00	ND	ND		
336	-2560	322	12	1	0.00	77	0.00	0.00	8.00	8.00	ND	ND		
338	312	-2540	11	1	0.00	77	0.00	0.00	0.00	0.00	ND	ND		
338	-2540	-2561	11	1	0.00	77	0.00	0.00	0.00	0.00	ND	ND		
338	-2561	323	11	1	0.00	77	0.00	0.00	0.00	0.00	ND	ND		
339	313	-2541	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND		
339	-2541	-2562	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND		
339	-2562	324	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND		
340	314	-2542	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND		
340	-2542	-2563	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND		
340	-2563	325	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND		
341	315	-2543	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND		
341	-2543	-2564	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND		
341	-2564	326	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND		
342	316	-2544	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND		
342	-2544	-2565	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND		
342	-2565	327	11	1	0.00	88	0.00	0.00	0.00	0.00	ND	ND		
343	318	-2545	12	1	0.00	99	0.00	0.00	0.00	0.00	ND	ND		
343	-2545	-2566	12	1	0.00	99	0.00	0.00	0.00	0.00	ND	ND		
343	-2566	328	12	1	0.00	99	0.00	0.00	0.00	0.00	ND	ND		
501	-1601	-1600	7	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND		
512	-1675	12	19	31	0.00	22	-15.00	-15.00	0.00	0.00	ND	ND		0.76
512	-1676	-1675	19	31	0.00	22	-15.00	-15.00	0.00	0.00	ND	ND		0.76
512	-1677	-1676	19	31	0.00	22	-15.00	-15.00	0.00	0.00	ND	ND		0.76
512	-1678	-1677	19	31	0.00	22	-15.00	-15.00	0.00	0.00	ND	ND		0.76
512	-1679	-1678	19	31	0.00	22	-15.00	-15.00	0.00	0.00	ND	ND		0.76
512	-1680	-1679	19	31	0.00	22	-15.00	-15.00	0.00	0.00	ND	ND		0.76
513	-1587	-1613	19	31	0.00	22	20.00	20.00	0.00	0.00	ND	ND		0.76
513	-1613	-1617	19	31	0.00	22	20.00	20.00	0.00	0.00	ND	ND		0.76
513	-1617	-1621	19	31	0.00	22	20.00	20.00	0.00	0.00	ND	ND		0.76
513	-1621	-1625	19	31	0.00	22	20.00	20.00	0.00	0.00	ND	ND		0.76
513	-1625	-1632	19	31	0.00	22	20.00	20.00	0.00	0.00	ND	ND		0.76
513	-1632	-1636	19	31	0.00	22	20.00	20.00	0.00	0.00	ND	ND		0.76
513	-1636	-1643	19	31	0.00	22	20.00	20.00	0.00	0.00	ND	ND		0.76
513	-1643	-1644	19	31	0.00	22	20.00	20.00	0.00	0.00	ND	ND		0.76
515	-1591	-1620	19	31	0.00	22	20.00	20.00	0.00	0.00	ND	ND		0.76
515	-1620	-1628	19	31	0.00	22	20.00	20.00	0.00	0.00	ND	ND		0.76
515	-1628	-1639	19	31	0.00	22	20.00	20.00	0.00	0.00	ND	ND		0.76
515	-1639	-1648	19	31	0.00	22	20.00	20.00	0.00	0.00	ND	ND		0.76
1500	-519	-518	5	1	0.00	11	0.00	0.00	0.00	0.00	ND	ND		
2000	218	201	4	7	0.00	11	0.00	0.00	0.00	0.00	ND	ND		

ELENCO TIPI ELEMENTI BIDIMENSIONALI

Simbologia

Tb = Numero del tipo muro/elemento bidimensionale
Comm. = Commento
Tipo = Tipologia
- F = Membranale e Flessionale
- M = Membranale
- W-RC = Winkler resistente solo a compressione
- W-RTC = Winkler resistente a trazione e a compressione

Uso = Utilizzo
- G = Generico
- P = Parete
- S = Soletta/Platea
- N = Nucleo
- M = Muratura ordinaria
- L = Pilastro

MA = Muratura armata
X = Pannello X-LAM
Mat. = Numero del materiale
Crit. = Numero del criterio di progetto
Spess. = Spessore
Kt = Coeff. di sottofondo su suolo elastico alla Winkler

Tb	Comm.	Tipo	Uso	Mat.	Crit.	Spess. <cm>	Kt <daN/cmc>
2	SETTO 40	F	P	1	5	40.00	
4	SETTO 30	F	P	1	5	30.00	
5	fondazione scantinato 25	W-RTC	S	1	1	25.00	f(strat.)
6	SETTO 20	F	P	1	5	20.00	

ELENCO ELEMENTI BIDIMENSIONALI

Simbologia

Bid. = Numero del muro/elemento bidimensionale
Tb = Numero del tipo muro/elemento bidimensionale
FF = Filo fisso
Dy1 = Scost. filo fisso Y1
Dy2 = Scost. filo fisso Y2
Kt = Coeff. di sottofondo su suolo elastico alla Winkler
NN = Nodi

Bid.	Tb	FF	Dy1 <cm>	Dy2 <cm>	Kt <daN/cmc>	NN	Bid.	Tb	FF	Dy1 <cm>	Dy2 <cm>	Kt <daN/cmc>	NN
217	4	33	0.00	0.00		-2479 -2478 -2495 -2496 -2425 -2424 -2441 -2442	217	4	33	0.00	0.00		-2476 -2475 -2492 -2493 -2458 -2457 -2474 -2475
217	4	33	0.00	0.00		-1778 -1772 -1850 -1852 -1709 -1707 -1772 -1778	217	4	33	0.00	0.00		-1622 -1614 -1707 -1709 -2289 -2272 -2332 -2349
217	4	33	0.00	0.00		-2206 -2188 -2272 -2289 -2141 -2124 -2188 -2206	217	4	33	0.00	0.00		-2058 -2040 -2124 -2141 -1998 -1981 -2040 -2058
217	4	33	0.00	0.00		-1915 -1897 -1981 -1998 -1850 -1833 -1897 -1915	217	4	33	0.00	0.00		-1772 -1754 -1833 -1850 -1707 -1690 -1754 -1772
217	4	33	0.00	0.00		-726 -708 -935 -938 -2299 -2297 -2371 203	217	4	33	0.00	0.00		-2232 -2225 -2297 -2299 -2151 -2149 -2225 -2232
217	4	33	0.00	0.00		-2084 -2077 -2149 -2151 -1929 -1926 -2002 -2004	217	4	33	0.00	0.00		-2008 -2006 -2077 -2084 -1941 -1934 -2006 -2008
217	4	33	0.00	0.00		-1860 -1858 -1934 -1941 -1798 -1791 -1858 -1860	217	4	33	0.00	0.00		-2293 -2291 -2356 -2362 -1717 -1715 -1791 -1798
217	4	33	0.00	0.00		-1649 -1640 -1715 -1717 -2297 -2295 -2365 -2371	217	4	33	0.00	0.00		-2225 -2220 -2295 -2297 -1164 -1161 -1275 -1278
217	4	33	0.00	0.00		-1167 -1164 -1278 -1281 -1037 -1020 -1135 -1152	217	4	33	0.00	0.00		-1614 -1595 -1690 -1707 -1043 -1040 -1155 -1158
217	4	33	0.00	0.00		-1046 -1043 -1158 -1161 -1049 -1046 -1161 -1164	217	4	33	0.00	0.00		-1052 -1049 -1164 -1167

2064 -2058 -2141 -2143
 217 4 33   0.00   0.00   -923 -906 -1020 -1037   217 4 33   0.00   0.00   -
2441 -2440 -2457 -2458
 217 4 33   0.00   0.00   -2491 -2485 -2502 -2508   217 4 33   0.00   0.00   -
2494 -2493 -2510 -2511
 217 4 33   0.00   0.00   -1494 -1477 -1595 -1614   217 4 33   0.00   0.00   -
1497 -1494 -1614 -1622
 217 4 33   0.00   0.00   -1500 -1497 -1622 -1629   217 4 33   0.00   0.00   -
1503 -1500 -1629 -1633
 217 4 33   0.00   0.00   -1506 -1503 -1633 -1640   217 4 33   0.00   0.00   -
1509 -1506 -1640 -1649
 217 4 33   0.00   0.00   -1380 -1364 -1477 -1494   217 4 33   0.00   0.00   -
1383 -1380 -1494 -1497
 217 4 33   0.00   0.00   -1386 -1383 -1497 -1500   217 4 33   0.00   0.00   -
1389 -1386 -1500 -1503
 217 4 33   0.00   0.00   -1392 -1389 -1503 -1506   217 4 33   0.00   0.00   -
1395 -1392 -1506 -1509
 217 4 33   0.00   0.00   -1266 -1249 -1364 -1380   217 4 33   0.00   0.00   -
1269 -1266 -1380 -1383
 217 4 33   0.00   0.00   -2423 -2417 -2434 -2440   217 4 33   0.00   0.00   -
1272 -1269 -1383 -1386
 217 4 33   0.00   0.00   -1275 -1272 -1386 -1389   217 4 33   0.00   0.00   -
1278 -1275 -1389 -1392
 217 4 33   0.00   0.00   -1281 -1278 -1392 -1395   217 4 33   0.00   0.00   -
2407 -2406 -2423 -2424
 217 4 33   0.00   0.00   -1152 -1135 -1249 -1266   217 4 33   0.00   0.00   -
1155 -1152 -1266 -1269
 217 4 33   0.00   0.00   -1158 -1155 -1269 -1272   217 4 33   0.00   0.00   -
1161 -1158 -1272 -1275
 217 4 33   0.00   0.00   -1926 -1921 -2000 -2002   217 4 33   0.00   0.00   -
1854 -1852 -1921 -1926
 217 4 33   0.00   0.00   -1783 -1778 -1852 -1854   217 4 33   0.00   0.00   -
1040 -1037 -1152 -1155
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 502  5 33   0.00   0.00      0.53  -567 -610 -595 -541      502  5 33   0.00   0.00      0.53  -507
-531 -567 -541
 502  5 33   0.00   0.00      0.53  -488 -473 -531 -507      502  5 33   0.00   0.00      0.53  -503
-488 -507 -541
 502  5 33   0.00   0.00      0.53  -454 -450 -409 -423      502  5 33   0.00   0.00      0.53  -488
-503 -450 -454
 502  5 33   0.00   0.00      0.53  -473 -488 -454 -423      502  5 33   0.00   0.00      0.53  -388
-377 -347 -357
 502  5 33   0.00   0.00      0.53  -388 -423 -409 -377      502  5 33   0.00   0.00      0.53  -317
-337 -357 -347
 502  5 33   0.00   0.00      0.53  -317 -282 -307 -337      502  5 33   0.00   0.00      0.53  -277
-248 -218 -247
 502  5 33   0.00   0.00      0.53  -277 -307 -282 -248      502  5 33   0.00   0.00      0.53  -247
-218 -188 -217
 502  5 33   0.00   0.00      0.53  -217 -188 -158 -187      502  5 33   0.00   0.00      0.53  -187
-158 -128 -157
 502  5 33   0.00   0.00      0.53  -157 -128 -98 -127       502  5 33   0.00   0.00      0.53  -127
-98 -68 -97
 502  5 33   0.00   0.00      0.53  -65 -97 -68 -62           502  5 33   0.00   0.00      0.53  -28
-33 -62 -68
 502  5 33   0.00   0.00      0.53  -35 -65 -62 -33           502  5 33   0.00   0.00      0.53  -27
-35 -33 -28
 502  5 33   0.00   0.00      0.53  -67 -59 -64 -96           502  5 33   0.00   0.00      0.53  -65
-35 -59 -67
 502  5 33   0.00   0.00      0.53  -96 -97 -65 -67           502  5 33   0.00   0.00      0.53  -30
-59 -35 -27
 502  5 33   0.00   0.00      0.53  -34 -64 -59 -30           502  5 33   0.00   0.00      0.53  -26
-34 -30 -27
 502  5 33   0.00   0.00      0.53  -828 -829 -786 -788      502  5 33   0.00   0.00      0.53  -808
-777 -786 -829
 502  5 33   0.00   0.00      0.53  -808 -806 -773 -777      502  5 33   0.00   0.00      0.53  -829
-830 -806 -808
 502  5 33   0.00   0.00      0.53  -830 -831 -801 -806      502  5 33   0.00   0.00      0.53  -801
-769 -773 -806
 502  5 33   0.00   0.00      0.53  -788 -786 -729 -728      502  5 33   0.00   0.00      0.53  -773
-769 -732 -731
 502  5 33   0.00   0.00      0.53  -777 -730 -729 -786      502  5 33   0.00   0.00      0.53  -777
-773 -731 -730
 502  5 33   0.00   0.00      0.53  -840 -841 -805 -799      502  5 33   0.00   0.00      0.53  -839
-840 -818 -812
 502  5 33   0.00   0.00      0.53  -792 -780 -812 -818      502  5 33   0.00   0.00      0.53  -799
-792 -818 -840
 502  5 33   0.00   0.00      0.53  -807 -812 -780 -775      502  5 33   0.00   0.00      0.53  -838
-839 -812 -807
 502  5 33   0.00   0.00      0.53  -768 -774 -744 -743      502  5 33   0.00   0.00      0.53  -768
-799 -805 -774
 502  5 33   0.00   0.00      0.53  -742 -741 -775 -780      502  5 33   0.00   0.00      0.53  -762
-768 -743 -742
 502  5 33   0.00   0.00      0.53  -792 -799 -768 -762      502  5 33   0.00   0.00      0.53  -780
-792 -762 -742
 502  5 33   0.00   0.00      0.53  -835 -836 -798 -785      502  5 33   0.00   0.00      0.53  -837
```

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-838 -807 -803
 502  5 33   0.00   0.00      0.53  -836 -837 -803 -798         502  5 33   0.00   0.00      0.53  -770
-775 -741 -740
 502  5 33   0.00   0.00      0.53  -770 -803 -807 -775         502  5 33   0.00   0.00      0.53  -766
-770 -740 -739
 502  5 33   0.00   0.00      0.53  -766 -798 -803 -770         502  5 33   0.00   0.00      0.53  -757
-738 -737 -785
 502  5 33   0.00   0.00      0.53  -766 -739 -738 -757         502  5 33   0.00   0.00      0.53  -798
-766 -757 -785
 502  5 33   0.00   0.00      0.53  -824 -797 -801 -831         502  5 33   0.00   0.00      0.53  -824
-822 -794 -797
 502  5 33   0.00   0.00      0.53  -831 -832 -822 -824         502  5 33   0.00   0.00      0.53  -832
-833 -819 -822
 502  5 33   0.00   0.00      0.53  -822 -819 -790 -794         502  5 33   0.00   0.00      0.53  -834
-835 -813 -814
 502  5 33   0.00   0.00      0.53  -814 -813 -781 -783         502  5 33   0.00   0.00      0.53  -785
-781 -813 -835
 502  5 33   0.00   0.00      0.53  -819 -814 -783 -790         502  5 33   0.00   0.00      0.53  -833
-834 -814 -819
 502  5 33   0.00   0.00      0.53  -781 -785 -737 -736         502  5 33   0.00   0.00      0.53  -761
-765 -797 -794
 502  5 33   0.00   0.00      0.53  -765 -761 -734 -733         502  5 33   0.00   0.00      0.53  -783
-781 -736 -735
 502  5 33   0.00   0.00      0.53  -758 -790 -783 -735         502  5 33   0.00   0.00      0.53  -761
-794 -790 -758
 502  5 33   0.00   0.00      0.53  -761 -758 -735 -734         502  5 33   0.00   0.00      0.53  -769
-765 -733 -732
 502  5 33   0.00   0.00      0.53  -769 -801 -797 -765         502  5 33   0.00   0.00      0.53  -842
-843 -816 -811
 502  5 33   0.00   0.00      0.53  -816 -787 -778 -811         502  5 33   0.00   0.00      0.53  -844
-845 -823 -820
 502  5 33   0.00   0.00      0.53  -795 -793 -820 -823         502  5 33   0.00   0.00      0.53  -802
-795 -823 -845
 502  5 33   0.00   0.00      0.53  -816 -820 -793 -787         502  5 33   0.00   0.00      0.53  -843
-844 -820 -816
 502  5 33   0.00   0.00      0.53  -845 -846 -810 -802         502  5 33   0.00   0.00      0.53  -805
-811 -778 -774
 502  5 33   0.00   0.00      0.53  -841 -842 -811 -805         502  5 33   0.00   0.00      0.53  -759
-764 -747 -746
 502  5 33   0.00   0.00      0.53  -759 -793 -795 -764         502  5 33   0.00   0.00      0.53  -756
-759 -746 -745
 502  5 33   0.00   0.00      0.53  -787 -793 -759 -756         502  5 33   0.00   0.00      0.53  -778
-787 -756 -745
 502  5 33   0.00   0.00      0.53  -778 -745 -744 -774         502  5 33   0.00   0.00      0.53  -771
-764 -795 -802
 502  5 33   0.00   0.00      0.53  -771 -748 -747 -764         502  5 33   0.00   0.00      0.53  -779
-771 -802 -810
 502  5 33   0.00   0.00      0.53  -779 -749 -748 -771         502  5 33   0.00   0.00      0.53  -720
-669 -672 -711
 502  5 33   0.00   0.00      0.53  -847 -848 -821 -817         502  5 33   0.00   0.00      0.53  -796
-789 -817 -821
 502  5 33   0.00   0.00      0.53  -804 -796 -821 -848         502  5 33   0.00   0.00      0.53  -810
-817 -789 -779
 502  5 33   0.00   0.00      0.53  -846 -847 -817 -810         502  5 33   0.00   0.00      0.53  -760
-767 -750 -749
 502  5 33   0.00   0.00      0.53  -789 -796 -767 -760         502  5 33   0.00   0.00      0.53  -779
-789 -760 -749
 502  5 33   0.00   0.00      0.53  -776 -767 -796 -804         502  5 33   0.00   0.00      0.53  -776
-751 -750 -767
 502  5 33   0.00   0.00      0.53  -849 -850 -809 -800         502  5 33   0.00   0.00      0.53  -753
-782 -809 -850
 502  5 33   0.00   0.00      0.53  -772 -800 -809 -782         502  5 33   0.00   0.00      0.53  -752
-772 -782 -753
 502  5 33   0.00   0.00      0.53  -848 -849 -815 -804         502  5 33   0.00   0.00      0.53  -791
-776 -804 -815
 502  5 33   0.00   0.00      0.53  -800 -791 -815 -849         502  5 33   0.00   0.00      0.53  -763
-772 -752 -751
 502  5 33   0.00   0.00      0.53  -791 -800 -772 -763         502  5 33   0.00   0.00      0.53  -776
-791 -763 -751
 502  5 33   0.00   0.00      0.53  -752 -753 -720 -711         502  5 33   0.00   0.00      0.53  -678
-676 -637 -634
 502  5 33   0.00   0.00      0.53  -676 -670 -639 -637         502  5 33   0.00   0.00      0.53  -784
-788 -728 -727
```

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 502  5 33   0.00   0.00      0.53  -827 -828 -788 -784         502  5 33   0.00   0.00      0.53  -825
-826 -754 -755
 502  5 33   0.00   0.00      0.53  -721 -719 -676 -678         502  5 33   0.00   0.00      0.53  -755
-754 -719 -721
 502  5 33   0.00   0.00      0.53  -708 -670 -676 -719         502  5 33   0.00   0.00      0.53  -726
-708 -719 -754
 502  5 33   0.00   0.00      0.53  -754 -784 -727 -726         502  5 33   0.00   0.00      0.53  -826
-827 -784 -754
 502  5 33   0.00   0.00      0.53  -42 -43 -8 -7               502  5 33   0.00   0.00      0.53  -76
-77 -43 -42
 502  5 33   0.00   0.00      0.53  -41 -42 -7 -6               502  5 33   0.00   0.00      0.53  -75
-76 -42 -41
 502  5 33   0.00   0.00      0.53  -40 -41 -6 -5               502  5 33   0.00   0.00      0.53  -74
-75 -41 -40
 502  5 33   0.00   0.00      0.53  -39 -40 -5 -4               502  5 33   0.00   0.00      0.53  -73
-74 -40 -39
 502  5 33   0.00   0.00      0.53  -637 -639 -607 -603         502  5 33   0.00   0.00      0.53  -603
-598 -634 -637
 502  5 33   0.00   0.00      0.53  -231 -262 -275 -246         502  5 33   0.00   0.00      0.53  -231
-219 -253 -262
 502  5 33   0.00   0.00      0.53  -199 -231 -246 -216         502  5 33   0.00   0.00      0.53  -199
-189 -219 -231
 502  5 33   0.00   0.00      0.53  -165 -199 -216 -186         502  5 33   0.00   0.00      0.53  -165
-159 -189 -199
 502  5 33   0.00   0.00      0.53  -130 -100 -99 -129          502  5 33   0.00   0.00      0.53  -130
-156 -126 -100
 502  5 33   0.00   0.00      0.53  -165 -130 -129 -159         502  5 33   0.00   0.00      0.53  -165
-186 -156 -130
 502  5 33   0.00   0.00      0.53  -70 -69 -99 -100            502  5 33   0.00   0.00      0.53  -70
-2 -1 -69
 502  5 33   0.00   0.00      0.53  -38 -39 -4 -3               502  5 33   0.00   0.00      0.53  -72
-73 -39 -38
 502  5 33   0.00   0.00      0.53  -37 -38 -3 -2               502  5 33   0.00   0.00      0.53  -71
-72 -38 -37
 502  5 33   0.00   0.00      0.53  -70 -71 -37 -2              502  5 33   0.00   0.00      0.53  -71
-70 -100 -126
 502  5 33   0.00   0.00      0.53  -382 -418 -422 -387         502  5 33   0.00   0.00      0.53  -382
-379 -413 -418
 502  5 33   0.00   0.00      0.53  -352 -382 -387 -356         502  5 33   0.00   0.00      0.53  -352
-349 -379 -382
 502  5 33   0.00   0.00      0.53  -323 -352 -356 -330         502  5 33   0.00   0.00      0.53  -323
-319 -349 -352
 502  5 33   0.00   0.00      0.53  -293 -323 -330 -304         502  5 33   0.00   0.00      0.53  -293
-287 -319 -323
 502  5 33   0.00   0.00      0.53  -262 -293 -304 -275         502  5 33   0.00   0.00      0.53  -262
-253 -287 -293
 502  5 33   0.00   0.00      0.53  -548 -549 -505 -504         502  5 33   0.00   0.00      0.53  -455
-466 -418 -413
 502  5 33   0.00   0.00      0.53  -455 -504 -505 -466         502  5 33   0.00   0.00      0.53  -557
-564 -513 -512
 502  5 33   0.00   0.00      0.53  -557 -603 -607 -564         502  5 33   0.00   0.00      0.53  -472
-422 -418 -466
 502  5 33   0.00   0.00      0.53  -510 -472 -466 -505         502  5 33   0.00   0.00      0.53  -549
-538 -510 -505
 502  5 33   0.00   0.00      0.53  -549 -550 -539 -538         502  5 33   0.00   0.00      0.53  -538
-539 -511 -510
 502  5 33   0.00   0.00      0.53  -551 -598 -603 -557         502  5 33   0.00   0.00      0.53  -512
-540 -551 -557
 502  5 33   0.00   0.00      0.53  -539 -540 -512 -511         502  5 33   0.00   0.00      0.53  -550
-551 -540 -539
 502  5 33   0.00   0.00      0.53  -451 -449 -412 -417         502  5 33   0.00   0.00      0.53  -451
-490 -486 -449
 502  5 33   0.00   0.00      0.53  -440 -414 -424 -443         502  5 33   0.00   0.00      0.53  -471
-460 -443 -424
 502  5 33   0.00   0.00      0.53  -462 -440 -443 -460         502  5 33   0.00   0.00      0.53  -489
-462 -460 -471
 502  5 33   0.00   0.00      0.53  -439 -461 -451 -417         502  5 33   0.00   0.00      0.53  -462
-461 -439 -440
 502  5 33   0.00   0.00      0.53  -414 -440 -439 -417         502  5 33   0.00   0.00      0.53  -492
-461 -462 -489
 502  5 33   0.00   0.00      0.53  -492 -490 -451 -461         502  5 33   0.00   0.00      0.53  -414
-383 -386 -424
 502  5 33   0.00   0.00      0.53  -414 -417 -381 -383         502  5 33   0.00   0.00      0.53  -380
```

-412 -407 -378
 502 5 33   0.00   0.00   0.53 -380 -381 -417 -412   502 5 33   0.00   0.00   0.53 -345
-346 -375 -374
 502 5 33   0.00   0.00   0.53 -345 -316 -318 -346   502 5 33   0.00   0.00   0.53 -318
-316 -285 -288
 502 5 33   0.00   0.00   0.53 -346 -348 -376 -375   502 5 33   0.00   0.00   0.53 -346
-318 -320 -348
 502 5 33   0.00   0.00   0.53 -320 -318 -288 -290   502 5 33   0.00   0.00   0.53 -315
-280 -285 -316
 502 5 33   0.00   0.00   0.53 -315 -314 -278 -280   502 5 33   0.00   0.00   0.53 -344
-345 -374 -373
 502 5 33   0.00   0.00   0.53 -344 -315 -316 -345   502 5 33   0.00   0.00   0.53 -343
-344 -373 -372
 502 5 33   0.00   0.00   0.53 -343 -314 -315 -344   502 5 33   0.00   0.00   0.53 -457
-459 -420 -419
 502 5 33   0.00   0.00   0.53 -497 -494 -509 -533   502 5 33   0.00   0.00   0.53 -497
-459 -457 -494
 502 5 33   0.00   0.00   0.53 -419 -420 -399 -400   502 5 33   0.00   0.00   0.53 -399
-372 -373 -400
 502 5 33   0.00   0.00   0.53 -404 -375 -376 -405   502 5 33   0.00   0.00   0.53 -404
-403 -374 -375
 502 5 33   0.00   0.00   0.53 -374 -403 -400 -373   502 5 33   0.00   0.00   0.53 -448
-404 -405 -444
 502 5 33   0.00   0.00   0.53 -448 -436 -403 -404

ELENCO TIPI PLINTI/PALI

Simbologia

Tl   = Numero del tipo plinto/palo
Tipo = Tipologia
        Gra = Gradoni
        Pir = Piramidale
        P = Palo
        T3 = Triangolare 3 pali
        T3B = Triangolare 3 pali + bicchiere
        R = Rettangolare
        RB = Rettangolare + bicchiere
        R1 = Rettangolare 1 palo
        R1B = Rettangolare 1 palo + bicchiere
        R2x = Rettangolare 2 pali dir. X
        R2xB = Rettangolare 2 pali dir. X + bicchiere
        R2y = Rettangolare 2 pali dir. Y
        R2B = Rettangolare 2 pali dir. Y + bicchiere
        R4 = Rettangolare 4 pali
        R4B = Rettangolare 4 pali + bicchiere
        P5 = Pentagonale 5 pali
        P5B = Pentagonale 5 pali + bicchiere
        E6 = Esagonale 6 pali
        E6B = Esagonale 6 pali + bicchiere
Tp   = Tipo palo
        ND = Non definito
        BP = Battuto prefabbricato
        BGO = Battuto gettato in opera
        T = Trivellato
        TEC = Trivellato con elica continua
        MP = Micropalo
Comm. = Commento
A1   = Prima dimensione plinto/palo in dir. X
A2   = Seconda dimensione plinto/palo in dir. X
A3   = Terza dimensione plinto/palo in dir. X
B1   = Prima dimensione plinto/palo in dir. Y
B2   = Seconda dimensione plinto/palo in dir. Y
B3   = Terza dimensione plinto/palo in dir. Y
H1   = Altezza parte inferiore plinto/palo
H2   = Altezza parte superiore plinto/palo
c1   = Allargamento magrone in dir. X
c2   = Allargamento magrone in dir. Y
h   = Altezza magrone
Crit. = Numero del criterio di progetto

Tl	Tipo Tp	Comm.	A1 <m>	A2 <m>	A3 <m>	B1 <m>	B2 <m>	B3 <m>	H1 <m>	H2 <m>	c1 <m>	c2 <m>	h <m>	Crit.
1	Gra	-- plinto nuovo pilastro	0.60	0.40	0.60	0.60	0.80	0.60	0.30	0.70	0.20	0.20	0.20	1

ELENCO PLINTI/PALI

Simbologia

PL = Plinto/Palo
Tl = Numero del tipo plinto/palo
Nodo = Nodo plinto/palo
Kt = Coeff. di sottofondo su suolo elastico alla Winkler

PL	Tl	Nodo	Kt <daN/cmc>
11	1	11	0.71

ELENCO TIPI SOLAI

Simbologia

Ts = Numero del tipo solaio
Comm. = Commento
Rc = Ripartizione carichi
UN = Unidirezionale
PP = A piastra perimetrale
PB = A piastra bisettrice
Qps = Carico permanente strutturale
Qpn = Carico permanente non strutturale
QA = Primo carico accidentale
QA2 = Secondo carico accidentale
QA3 = Terzo carico accidentale
Rip. ter. = Ripartizione su aste terminali
Rip. int. = Ripartizione su aste interne
Lfl = Larghezza fascia laterale
Zcv = Quota di riferimento del piano di campagna
s = Coeff. di riduzione

Ts	Comm.	Rc	Qps <daN/mq>	Qpn <daN/mq>	QA <daN/mq>	QA2 <daN/mq>	QA3 <daN/mq>	Rip. ter.	Rip. int.	Lfl <m>	Zcv <m>	s
1	COPERTURA A VOLTE	UN	250.00	70.00	80.00	50.00	0.00	50.00	50.00	0.00	0.00	1.00
2	SOLAIO NUOVO	UN	350.00	100.00	300.00	0.00	0.00	50.00	50.00	0.00	0.00	1.00
3	COPERTURA NUOVA	UN	25.00	150.00	80.00	50.00	60.00	50.00	50.00	0.00	18.00	1.00
4	TIPO 1 PREDALLE 30	UN	360.00	80.00	300.00	80.00	0.00	50.00	50.00	0.00	0.00	1.00
5	TIPO 2 SPIROL 36	UN	400.00	80.00	400.00	0.00	0.00	50.00	50.00	0.00	0.00	1.00
6	VANO SCALA	UN	500.00	100.00	400.00	0.00	0.00	50.00	50.00	0.00	0.00	1.00
8	COPERTURA NUOVA LATO ML	UN	25.00	150.00	20.00	50.00	80.00	50.00	50.00	0.00	18.00	1.00
10	PASSERELLA SPIROL 35	UN	400.00	80.00	400.00	80.00	0.00	50.00	50.00	0.00	0.00	1.00

ELENCO SOLAI

Simbologia

Sol. = Numero del solaio
Ts = Numero del tipo solaio
Ord. = Orditura
Nodi = Nodi del solaio

Sol.	Ts	Ord. <grad>	Nodi
200	1	0.00	203 -2378 -2379 -2380 -2381 -2382 -2383 -2384 204 209 215 214 208
201	1	0.00	204 -2385 -2386 -2387 -2388 -2389 -2390 -2391 -2392 -2393 205 210 216 215 209
202	2	0.00	218 201 206 212 211
203	5	0.00	-2331 -2332 -2349 -2356 -2362 -2365 -2371 203 218 -2370 -2361 -2354
204	2	0.00	202 203 208 214 213 207
205	6	90.00	-2332 -2333 -2334 -2335 -2336 -2337 217 204 -2384 -2383 -2382 -2381 -2380 -2379 -2378 203 -2371 -2365 -2362 -2356 -2349
206	6	90.00	217 -2590 -2338 -2339 -2340 -2341 -2342 -2343 -2344 -2345 -2346 -2347 -2350 -2357 -2363 -2366 -2372 205 -2393 -2392 -2391 -2390 -2389 -2388 -2387 -2386 -2385 204
207	2	0.00	201 202 207 213 -2399 -2398 -2397 -2396 -2395 -2394 212 206
208	10	0.00	-2377 -2369 -2360 -2353 -2330 -2331 -2354 -2361 -2370 218
209	10	0.00	-2327 -2348 -2351 -2355 -2358 -2364 -2367 -2373 -2374 -2375 -2368 -2359 -2352 -2328
300	3	90.00	-2553 -2567 -2568 -2554
301	8	90.00	-2544 -2543 -2542 -2541 -2540 -2561 -2562 -2563 -2564 -2565
302	8	90.00	312 317 -2539 -2540
303	3	90.00	-2567 322 323 -2568
304	3	90.00	-2537 305 -2530 -2529 304 -2536
305	3	90.00	-2546 -2553 -2554 -2547
306	3	90.00	-2532 -2546 -2547 -2533
307	3	90.00	-2525 -2526 -2519 -2518
308	3	90.00	-2568 323 324 325 326 327 -2572 -2571 -2570 -2569
309	3	90.00	-2554 -2568 -2569 -2570 -2571 -2572 -2558 -2557 -2556 -2555
310	3	90.00	-2547 -2554 -2555 -2556 -2557 -2558 -2551 -2550 -2549 -2548
311	3	90.00	-2533 -2547 -2548 -2549 -2550 -2551 -2537 -2536 -2535 -2534
312	3	90.00	-2525 319 -2532 -2533 301 -2526
313	3	90.00	-2529 -2530 -2523 -2522
314	8	90.00	-2544 -2545 -2566 -2565
315	8	90.00	316 315 314 313 312 -2540 -2541 -2542 -2543 -2544
316	8	90.00	-2540 -2539 -2560 -2561
317	8	90.00	-2565 -2564 -2563 -2562 -2561 323 324 325 326 327
318	3	90.00	-2521 -2528 -2529 -2522
319	3	90.00	-2520 -2527 -2528 -2521
320	3	90.00	-2519 -2526 -2527 -2520
321	3	90.00	-2535 -2536 304 -2529 -2528 320
322	3	90.00	-2528 -2527 302 -2534 -2535 320
323	3	90.00	-2527 -2526 301 -2533 -2534 302
324	3	90.00	-2523 -2530 -2531 -2524
325	3	90.00	-2530 305 -2537 -2538 321 -2531
326	3	90.00	-2537 -2551 -2552 -2538
327	3	90.00	-2551 -2558 -2559 -2552
328	3	90.00	-2558 -2572 -2573 -2559
329	3	90.00	-2572 327 328 -2573
330	8	90.00	316 318 -2545 -2544
331	8	90.00	-2560 -2561 323 322
332	8	90.00	-2565 -2566 328 327
500	4	90.00	-1536 -1537 -1538 -1539 -1540 -1541 -1542 -1543 -1544 -1545 -1546 -1547 -1548 -1549 -1550 -1551 -1552 -1553 -1554 -1555 -1556 -1557 -1558 -1559 -1560 -1561 -1562 -1564 -1566 -1568 -1570 -1572 -1574 -1576 -1578 -1580 -1582 -1584 -1586 -1612 -1611 -1610 -1609 -1608 -1607 -1606 -1605 -1604 -1603 -1602 -2580 -1601 -1600 -1599 -1598 -1597 -1596 -1595 -1594 -1593 -1592 -1585 -1583 -1581 -1579 -1577 -1575 -1573 -1571 -1569 -1567 -1565 -1563
501	4	0.00	-1671 -1672 -1673 -1674 -1642 -1635 -1631 -1624 -1616 -1612 -1611 -1615 -1623 -1630 -1634 -1641
502	6	90.00	-1649 -1650 -1651 -1652 -1653 -1654 -1655 -1656 -1657 -1658 -1659 -1660 -1661 -1601 -1600 -1599 -1598 -1597 -1596 -1595 -1614 -1622 -1629 -1633 -1640
503	6	90.00	-1601 -2580 -1602 -1603 -1604 -1605 -1606 -1607 -1608 -1609 -1610 -1611 -1615 -1623 -1630 -1634 -1641 -1671 -1670 -1669 -1668 -1667 -1666 -1665 -1664 -1663 -1662 -1661

ELENCO TIPI RETICOLARI

Simbologia

Tr   = Numero del tipo reticolare
Tipo = Tipologia
Comm. = Commento
Crit. = Numero del criterio di progetto

Tr	Tipo	Comm.	Crit.
1	Bullonata controvento		6

ELENCO TIPI TAMPONATURE

Simbologia

Tt   = Numero del tipo tamponatura
Comm. = Commento
Qpn   = Carico permanente non strutturale
Rcg   = Ripartizione carichi gravitazionali
  AP = Sull'asta di piede
  AL = Sulle aste laterali
  APT = Sulle aste di piede e di testa
Rcv   = Ripartizione carichi vento
  AP = Sull'asta di piede
  AL = Sulle aste laterali
  APT = Sulle aste di piede e di testa
  PP = A piastra perimetrale
  PB = A piastra bisettrice
Zcv   = Quota di riferimento del piano di campagna
P   = Puntoni equivalenti
  S = Genera i puntoni equivalenti
  N = Non genera i puntoni equivalenti
Tipo = Tipologia
  C = Area di carico
  V = Area di carico e verifica
Crit. = Criterio di progetto

Tt	Comm.	Qpn <daN/mq>	Rcg	Rcv	Zcv <m>	P	Tipo	Crit.
1	TAMPONATURA CW	150.00	AP	AL	0.00	N	C	--

ELENCO TAMPONATURE

Simbologia

Tam. = Numero della tamponatura
Tt   = Numero del tipo tamponatura
Nodi = Nodi della tamponatura

Tam.	Tt	Nodi
109	1	205 305 -2537 -2551 -2558 -2572 327 -2565 -2544 316 216 210
208	1	212 312 -2540 -2561 323 -2568 -2554 -2547 -2533 301 201 206
105	1	312 313 213 -2399 -2398 -2397 -2396 -2395 -2394 212
103	1	203 -2378 -2379 -2380 -2381 -2382 -2383 -2384 204 304 320 303 -2496 -2479 -2462 -2445 -2428 -2411
106	1	213 214 314 313
107	1	214 215 315 314
108	1	215 216 316 315
101	1	201 202 302 301
102	1	202 203 -2411 -2428 -2445 -2462 -2479 -2496 303 320 302
104	1	204 -2385 -2386 -2387 -2388 -2389 -2390 -2391 -2392 -2393 205 305 304

CONDIZIONI DI CARICO ELEMENTARI:

Simbologia

CCE = Numero della condizione di carico elementare
Comm. = Commento
Tipo CCE = Tipo di CCE per calcolo agli stati limite
Sic. = Contributo alla sicurezza
F = a favore
S = a sfavore
A = ambigua
Var. = Tipo di variabilità
B = di base
I = indipendente
A = ambigua
Dir. = Direzione del vento
Tipo = Tipologia di pressione vento
M = Massimizzata
E = Esterna
I = Interna
Mx = Moltiplicatore della massa in dir. X
My = Moltiplicatore della massa in dir. Y
Mz = Moltiplicatore della massa in dir. Z
Jpx = Moltiplicatore del momento d'inerzia intorno all'asse X
Jpy = Moltiplicatore del momento d'inerzia intorno all'asse Y
Jpz = Moltiplicatore del momento d'inerzia intorno all'asse Z

Condizioni di carico elementari

CCE	Comm.	Tipo CCE	Sic.	Var.	Dir.	Tipo	Mx	My	Mz	Jpx	Jpy	Jpz
<grad>												
1	PERMANENTI ST	1 D.M. 08 Permanenti strutturali	S	--	--	--	1.00	1.00	0.00	0.00	0.00	1.00
2	PERMANENTI NST	2 D.M. 08 Permanenti non strutturali	S	--	--	--	1.00	1.00	0.00	0.00	0.00	1.00
3	ACCIDENTALI	5 D.M. 08 Variabili Categoria C Ambienti suscettibili di affollamento	S	A	--	--	1.00	1.00	0.00	0.00	0.00	1.00
4	NEVE	11 D.M. 08 Variabili Neve (a quota <= 1000 m s.l.m.)	S	A	--	--	1.00	1.00	0.00	0.00	0.00	1.00
5	VENTO	10 D.M. 08 Variabili Vento	S	A	--	--	1.00	1.00	0.00	0.00	0.00	1.00

ELENCO CARICHI ASTE

CONDIZIONE DI CARICO 1: PERMANENTI ST

ELENCO PESO PROPRIO ASTE

Simbologia

Sez. = Numero della sezione
Comm. = Commento
A = Area
Mat. = Materiale
P = Peso specifico
PL = Peso specifico a metro lineare

Sez.	Comm.	A <cmq>	Mat.	P <daN/mc>	PL <daN/m>	Sez.	Comm.	A <cmq>	Mat.	P <daN/mc>	PL <daN/m>
3		1050.000000	Calcestruzzo	2500.00	262.50	4	HEA200	52.983000	Acciaio	7850.00	41.59
5	T12X25	300.000000	Calcestruzzo	2500.00	75.00	7	T30X40	1200.000000	Calcestruzzo	2500.00	300.00

```
   8 HEB300          149.082000 Acciaio       7850.00  117.03      9 HEA260           86.822500 Acciaio
7850.00   68.16
  11 HEA360          142.762000 Acciaio       7850.00  112.07     12 HEA160           38.772600 Acciaio
7850.00   30.44
  14 2HEA160          77.545200 Acciaio       7850.00   60.87     16 P40X40         1600.000000
Calcestruzzo  2500.00  400.00
  18 HEA240          76.837900 Acciaio       7850.00   60.32     19 treave fond 20 6700.000000
Calcestruzzo  2500.00 1675.00
  20                900.000000 Calcestruzzo  2500.00  225.00     21                3200.000000
Calcestruzzo  2500.00  800.00
  22 HEA400          158.982000 Acciaio       7850.00  124.80
```

ELENCO CARICHI ASTE

CONDIZIONE DI CARICO 1: PERMANENTI ST

CARICHI DISTRIBUITI

Simbologia

Asta = Numero dell'asta
N1 = Nodo iniziale
N2 = Nodo finale
E = Elemento provenienza del carico
S = Solaio
T = Tamponatura
NE = Numero elemento di provenienza del carico
T = Tipo di carico
QA = Primo carico accidentale
QA2 = Secondo carico accidentale
QA3 = Terzo carico accidentale
QPS = Carico permanente strutturale
QPN = Carico permanente non strutturale
VE = Vento
M = Manuale
DC = Direzione del carico
XG,YG,ZG = secondo gli assi globali
XL,YL,ZL = secondo gli assi locali
Xi = Distanza iniziale
Qi = Carico iniziale
Xf = Distanza finale
Qf = Carico finale

Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>
0	-2327	-2348	S	209	QPS	ZG	0.00	1260.00	0.34	1260.00
0	-2348	-2351	S	209	QPS	ZG	0.00	1260.00	0.34	1260.00
0	-2351	-2355	S	209	QPS	ZG	0.00	1260.00	0.34	1260.00
0	-2355	-2358	S	209	QPS	ZG	0.00	1260.00	0.34	1260.00
0	-2358	-2364	S	209	QPS	ZG	0.00	1260.00	0.34	1260.00
0	-2364	-2367	S	209	QPS	ZG	0.00	1260.00	0.34	1260.00
0	-2367	-2373	S	209	QPS	ZG	0.00	1260.00	0.34	1260.00
0	-2373	-2374	S	209	QPS	ZG	0.00	1260.00	0.34	1260.00
0	-2352	-2328	S	209	QPS	ZG	0.00	1260.00	0.68	1260.00
0	-2359	-2352	S	209	QPS	ZG	0.00	1260.00	0.68	1260.00
0	-2368	-2359	S	209	QPS	ZG	0.00	1260.00	0.68	1260.00
0	-2353	-2330	S	208	QPS	ZG	0.00	1326.00	0.68	1326.00
0	-2375	-2368	S	209	QPS	ZG	0.00	1260.00	0.68	1260.00
0	-2360	-2353	S	208	QPS	ZG	0.00	1326.00	0.68	1326.00
0	-2369	-2360	S	208	QPS	ZG	0.00	1326.00	0.68	1326.00
0	-2377	-2369	S	208	QPS	ZG	0.00	1326.00	0.68	1326.00
0	-2331	-2354	S	203	QPS	ZG	0.00	0.00	0.22	2814.00
0	-2331	-2354	S	208	QPS	ZG	0.00	1326.00	0.68	1326.00
0	-2331	-2354	S	203	QPS	ZG	0.22	2814.00	0.68	2814.00
0	-2354	-2361	S	203	QPS	ZG	0.00	2814.00	0.68	2814.00
0	-2354	-2361	S	208	QPS	ZG	0.00	1326.00	0.68	1326.00
0	-2361	-2370	S	203	QPS	ZG	0.00	2814.00	0.68	2814.00
0	-2361	-2370	S	208	QPS	ZG	0.00	1326.00	0.68	1326.00
0	-2370	218	S	203	QPS	ZG	0.00	2814.00		

```
0.68 2814.00
   0 -2370   218 S 208 QPS ZG 0.00 1326.00  0.68 1326.00      0 -1536 -1537 S 500 QPS ZG 0.00 1157.40
0.48 1157.40
   0 -2331 -2332 S 203 QPS ZG 0.00    0.00 14.07   43.99      0 -1537 -1538 S 500 QPS ZG 0.00 1157.40
0.48 1157.40
   0 -1538 -1539 S 500 QPS ZG 0.00 1157.40  0.48 1157.40      0 -1539 -1540 S 500 QPS ZG 0.00 1157.40
0.48 1157.40
   0 -1540 -1541 S 500 QPS ZG 0.00 1157.40  0.48 1157.40      0 -1541 -1542 S 500 QPS ZG 0.00 1157.40
0.48 1157.40
   0 -1542 -1543 S 500 QPS ZG 0.00 1157.40  0.48 1157.40      0   218   203 S 203 QPS ZG 0.00   10.00
14.07    0.00
   0 -1543 -1544 S 500 QPS ZG 0.00 1157.40  0.48 1157.40      0 -1544 -1545 S 500 QPS ZG 0.00 1157.40
0.48 1157.40
   0 -1545 -1546 S 500 QPS ZG 0.00 1157.40  0.48 1157.40      0 -1546 -1547 S 500 QPS ZG 0.00 1157.40
0.48 1157.40
   0 -1547 -1548 S 500 QPS ZG 0.00 1157.40  0.48 1157.40      0 -1548 -1549 S 500 QPS ZG 0.00 1157.40
0.48 1157.40
   0 -1549 -1550 S 500 QPS ZG 0.00 1157.40  0.48 1157.40      0 -1593 -1592 S 500 QPS ZG 0.00 1157.40
0.43 1157.40
   0 -1550 -1551 S 500 QPS ZG 0.00 1157.40  0.48 1157.40      0 -1594 -1593 S 500 QPS ZG 0.00 1157.40
0.43 1157.40
   0 -1551 -1552 S 500 QPS ZG 0.00 1157.40  0.48 1157.40      0 -1595 -1594 S 500 QPS ZG 0.00 1157.40
0.43 1157.40
   0 -1596 -1595 S 500 QPS ZG 0.00 1157.40  0.43 1157.40      0 -1596 -1595 S 502 QPS ZG 0.00  632.50
0.43  632.50
   0 -1597 -1596 S 500 QPS ZG 0.00 1157.40  0.43 1157.40      0 -1597 -1596 S 502 QPS ZG 0.00  632.50
0.43  632.50
   0 -1553 -1554 S 500 QPS ZG 0.00 1157.40  0.48 1157.40      0 -1598 -1597 S 500 QPS ZG 0.00 1157.40
0.43 1157.40
   0 -1598 -1597 S 502 QPS ZG 0.00  632.50  0.43  632.50      0 -1599 -1598 S 500 QPS ZG 0.00 1157.40
0.43 1157.40
   0 -1599 -1598 S 502 QPS ZG 0.00  632.50  0.43  632.50      0 -1601 -2580 S 500 QPS ZG 0.00 1157.40
0.32 1157.40
   0 -1601 -2580 S 503 QPS ZG 0.15  632.50  0.32  632.50      0 -1601 -2580 S 503 QPS ZG 0.00    0.00
0.15  632.50
   0 -2332 -2333 S 205 QPS ZG 0.00  632.50  0.43  632.50      0 -1552 -1553 S 500 QPS ZG 0.00 1157.40
0.48 1157.40
   0 -1600 -1599 S 500 QPS ZG 0.00 1157.40  0.43 1157.40      0 -1600 -1599 S 502 QPS ZG 0.00  632.50
0.43  632.50
   0 -1653 -1654 S 502 QPS ZG 0.00  632.50  0.28  632.50      0 -2333 -2334 S 205 QPS ZG 0.00  632.50
0.43  632.50
   0 -1554 -1555 S 500 QPS ZG 0.00 1157.40  0.48 1157.40      0 -1555 -1556 S 500 QPS ZG 0.00 1157.40
0.48 1157.40
   0 -1649 -1650 S 502 QPS ZG 0.00  632.50  0.43  632.50      0 -1651 -1652 S 502 QPS ZG 0.00  632.50
0.43  632.50
   0 -1652 -1653 S 502 QPS ZG 0.00  632.50  0.43  632.50      0 -1654 -1655 S 502 QPS ZG 0.00  632.50
0.60  632.50
   0 -1655 -1656 S 502 QPS ZG 0.00  632.50  0.45  632.50      0 -1601 -1661 S 502 QPS ZG 0.00   37.43
2.53    0.00
   0 -1601 -1661 S 503 QPS ZG 0.00    0.00  2.53   37.43      0 -1660 -1661 S 502 QPS ZG 0.00  632.50
0.10  632.50
   0 -1660 -1661 S 502 QPS ZG 0.10  632.50  0.26    0.00      0 -2356 -2349 S 203 QPS ZG 0.00 2814.00
0.42 2814.00
   0 -2365 -2362 S 203 QPS ZG 0.00 2814.00  0.42 2814.00      0 -1556 -1557 S 500 QPS ZG 0.00 1157.40
0.48 1157.40
   0 -1657 -1658 S 502 QPS ZG 0.00  632.50  0.45  632.50      0 -2349 -2332 S 203 QPS ZG 0.00 2814.00
0.42 2814.00
   0 -2362 -2356 S 203 QPS ZG 0.00 2814.00  0.42 2814.00      0 -2335 -2336 S 205 QPS ZG 0.00  632.50
0.43  632.50
   0 -1557 -1558 S 500 QPS ZG 0.00 1157.40  0.48 1157.40      0 -1650 -1651 S 502 QPS ZG 0.00  632.50
0.43  632.50
   0 -2371 -2365 S 203 QPS ZG 0.00 2814.00  0.42 2814.00      0 -2336 -2337 S 205 QPS ZG 0.00  632.50
0.43  632.50
   0   203 -2371 S 203 QPS ZG 0.00    0.00  0.05 2814.00      0   203 -2371 S 203 QPS ZG 0.05 2814.00
0.42 2814.00
   0   203 -2378 S 205 QPS ZG 0.00  632.50  0.43  632.50      0 -1558 -1559 S 500 QPS ZG 0.00 1157.40
0.48 1157.40
   0 -1560 -1561 S 500 QPS ZG 0.00 1157.40  0.48 1157.40      0 -2580 -1602 S 500 QPS ZG 0.00 1157.40
0.32 1157.40
   0 -2580 -1602 S 503 QPS ZG 0.00  632.50  0.32  632.50      0 -1602 -1603 S 500 QPS ZG 0.00 1157.40
0.49 1157.40
   0 -1602 -1603 S 503 QPS ZG 0.00  632.50  0.49  632.50      0 -2378 -2379 S 205 QPS ZG 0.00  632.50
0.43  632.50
```

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   0 -2379 -2380 S 205 QPS ZG 0.00  632.50  0.43  632.50      0 -1656 -1657 S 502 QPS ZG 0.00  632.50
0.45  632.50
   0 -2334 -2335 S 205 QPS ZG 0.00  632.50  0.43  632.50      0 -1603 -1604 S 500 QPS ZG 0.00 1157.40
0.49 1157.40
   0 -1603 -1604 S 503 QPS ZG 0.00  632.50  0.49  632.50      0 -1604 -1605 S 500 QPS ZG 0.00 1157.40
0.49 1157.40
   0 -1604 -1605 S 503 QPS ZG 0.00  632.50  0.49  632.50      0 -1659 -1660 S 502 QPS ZG 0.00  632.50
0.26  632.50
   0 -2381 -2382 S 205 QPS ZG 0.00  632.50  0.28  632.50      0 -1605 -1606 S 500 QPS ZG 0.00 1157.40
0.49 1157.40
   0 -1605 -1606 S 503 QPS ZG 0.00  632.50  0.49  632.50      0 -1606 -1607 S 500 QPS ZG 0.00 1157.40
0.49 1157.40
   0 -1606 -1607 S 503 QPS ZG 0.00  632.50  0.49  632.50      0 -1607 -1608 S 500 QPS ZG 0.00 1157.40
0.49 1157.40
   0 -1607 -1608 S 503 QPS ZG 0.00  632.50  0.49  632.50      0 -1662 -1663 S 503 QPS ZG 0.00  632.50
0.49  632.50
   0 -1663 -1664 S 503 QPS ZG 0.00  632.50  0.49  632.50      0 -2380 -2381 S 205 QPS ZG 0.00  632.50
0.43  632.50
   0 -1561 -1562 S 500 QPS ZG 0.00 1157.40  0.48 1157.40      0 -1658 -1659 S 502 QPS ZG 0.00  632.50
0.45  632.50
   0 -1661 -1662 S 503 QPS ZG 0.00  632.50  0.49  632.50      0 -1664 -1665 S 503 QPS ZG 0.00  632.50
0.49  632.50
   0 -1559 -1560 S 500 QPS ZG 0.00 1157.40  0.48 1157.40      0   217 -2590 S 206 QPS ZG 0.00    0.00
0.15  632.50
   0   217 -2590 S 206 QPS ZG 0.15  632.50  0.32  632.50      0   217   204 S 205 QPS ZG 0.00   37.43
2.53    0.00
   0   217   204 S 206 QPS ZG 0.00    0.00  2.53   37.43      0 -1608 -1609 S 500 QPS ZG 0.00 1157.40
0.49 1157.40
   0 -1608 -1609 S 503 QPS ZG 0.00  632.50  0.49  632.50      0 -1665 -1666 S 503 QPS ZG 0.00  632.50
0.49  632.50
   0 -1666 -1667 S 503 QPS ZG 0.00  632.50  0.49  632.50      0 -1610 -1611 S 500 QPS ZG 0.00 1157.40
0.49 1157.40
   0 -1610 -1611 S 503 QPS ZG 0.00  632.50  0.49  632.50      0 -2590 -2338 S 206 QPS ZG 0.00  632.50
0.32  632.50
   0 -2339 -2340 S 206 QPS ZG 0.00  632.50  0.49  632.50      0 -2384   204 S 205 QPS ZG 0.00  632.50
0.10  632.50
   0 -2384   204 S 205 QPS ZG 0.10  632.50  0.26    0.00      0 -1609 -1610 S 500 QPS ZG 0.00 1157.40
0.49 1157.40
   0 -1609 -1610 S 503 QPS ZG 0.00  632.50  0.49  632.50      0 -1611 -1615 S 501 QPS ZG 0.00  270.00
0.42  270.00
   0 -1615 -1623 S 501 QPS ZG 0.00  270.00  0.42  270.00      0 -1611 -1612 S 500 QPS ZG 0.00 1157.40
1.50 1157.40
   0 -1667 -1668 S 503 QPS ZG 0.00  632.50  0.49  632.50      0 -1623 -1630 S 501 QPS ZG 0.00  270.00
0.42  270.00
   0 -1668 -1669 S 503 QPS ZG 0.00  632.50  0.49  632.50      0 -1616 -1612 S 501 QPS ZG 0.00  270.00
0.42  270.00
   0 -1669 -1670 S 503 QPS ZG 0.00  632.50  0.49  632.50      0 -2383 -2384 S 205 QPS ZG 0.00  632.50
0.26  632.50
   0 -1630 -1634 S 501 QPS ZG 0.00  270.00  0.42  270.00      0 -1634 -1641 S 501 QPS ZG 0.00  270.00
0.42  270.00
   0 -1641 -1671 S 501 QPS ZG 0.00  270.00  0.42  270.00      0   204 -2385 S 206 QPS ZG 0.00  632.50
0.49  632.50
   0 -2338 -2339 S 206 QPS ZG 0.00  632.50  0.49  632.50      0 -1624 -1616 S 501 QPS ZG 0.00  270.00
0.42  270.00
   0 -1670 -1671 S 503 QPS ZG 0.00  632.50  0.49  632.50      0 -1631 -1624 S 501 QPS ZG 0.00  270.00
0.42  270.00
   0 -2340 -2341 S 206 QPS ZG 0.00  632.50  0.49  632.50      0 -2386 -2387 S 206 QPS ZG 0.00  632.50
0.49  632.50
   0 -1635 -1631 S 501 QPS ZG 0.00  270.00  0.42  270.00      0 -1674 -1642 S 501 QPS ZG 0.00  270.00
0.42  270.00
   0 -2342 -2343 S 206 QPS ZG 0.00  632.50  0.49  632.50      0 -2343 -2344 S 206 QPS ZG 0.00  632.50
0.49  632.50
   0 -2385 -2386 S 206 QPS ZG 0.00  632.50  0.49  632.50      0 -1642 -1635 S 501 QPS ZG 0.00  270.00
0.42  270.00
   0 -2341 -2342 S 206 QPS ZG 0.00  632.50  0.49  632.50      0 -2344 -2345 S 206 QPS ZG 0.00  632.50
0.49  632.50
   0 -2345 -2346 S 206 QPS ZG 0.00  632.50  0.49  632.50      0 -2387 -2388 S 206 QPS ZG 0.00  632.50
0.49  632.50
   0 -2346 -2347 S 206 QPS ZG 0.00  632.50  0.49  632.50      0 -2388 -2389 S 206 QPS ZG 0.00  632.50
0.49  632.50
   0 -2389 -2390 S 206 QPS ZG 0.00  632.50  0.49  632.50      0 -2390 -2391 S 206 QPS ZG 0.00  632.50
0.49  632.50
   0 -2391 -2392 S 206 QPS ZG 0.00  632.50  0.49  632.50      0 -2392 -2393 S 206 QPS ZG 0.00  632.50
```

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0.49  632.50
   0 -2393   205 S 206 QPS ZG 0.00  632.50  0.49  632.50    201 -2337   217 S 205 QPS ZG 0.00  632.50
2.61  632.50
 204 -2382 -2383 S 205 QPS ZG 0.00  632.50  2.40  632.50    215   218   211 S 202 QPS ZG 0.00    0.00
0.05  717.50
 215   218   211 S 202 QPS ZG 0.05  717.50 10.21  717.50    216   206   201 S 202 QPS ZG 0.00  717.50
5.08  717.50
 216   206   201 S 207 QPS ZG 0.00  862.75  5.08  862.75    216   212   206 S 202 QPS ZG 0.00  717.50
5.08  717.50
 216   212   206 S 207 QPS ZG 0.00  862.75  5.08  862.75    217   207   202 S 204 QPS ZG 0.00  882.00
5.08  882.00
 217   207   202 S 207 QPS ZG 0.00  862.75  5.08  862.75    217   213   207 S 204 QPS ZG 0.00  882.00
5.08  882.00
 217   213   207 S 207 QPS ZG 0.00  862.75  5.08  862.75    218   208   203 S 200 QPS ZG 0.00  612.50
5.08  612.50
 218   208   203 S 204 QPS ZG 0.00  882.00  5.08  882.00    218   214   208 S 200 QPS ZG 0.00  612.50
5.08  612.50
 218   214   208 S 204 QPS ZG 0.00  882.00  5.08  882.00    219   209   204 S 200 QPS ZG 0.00  612.50
5.08  612.50
 219   209   204 S 201 QPS ZG 0.00  612.50  5.08  612.50    219   215   209 S 200 QPS ZG 0.00  612.50
5.08  612.50
 219   215   209 S 201 QPS ZG 0.00  612.50  5.08  612.50    220   210   205 S 201 QPS ZG 0.00  612.50
5.08  612.50
 220   210   205 T 109 QPN ZG 0.00 1348.76  5.08  780.00    220   216   210 S 201 QPS ZG 0.00  612.50
5.08  612.50
 220   216   210 T 109 QPN ZG 4.60 1402.50  5.08 1348.76    220   216   210 T 109 QPN ZG 0.00  562.50
4.60 1402.50
 302 -2518 -2519 S 307 QPS ZG 0.00   20.63  4.22   20.63    302 -2519 -2520 S 320 QPS ZG 0.00   20.63
4.93   20.63
 302 -2520 -2521 S 319 QPS ZG 0.00   20.63  5.04   20.63    302 -2521 -2522 S 318 QPS ZG 0.00   20.63
4.90   20.63
 302 -2522 -2523 S 313 QPS ZG 0.00   20.63  4.90   20.63    302 -2523 -2524 S 324 QPS ZG 0.00   20.63
2.63   20.63
 303 -2525 -2526 S 307 QPS ZG 0.00   20.63  4.22   20.63    303 -2525 -2526 S 312 QPS ZG 0.00   20.60
4.22   20.60
 303 -2526 -2527 S 320 QPS ZG 0.00   20.63  4.93   20.63    303 -2526 -2527 S 323 QPS ZG 0.00   20.60
4.93   20.60
 303 -2527 -2528 S 319 QPS ZG 0.00   20.63  5.04   20.63    303 -2527 -2528 S 322 QPS ZG 0.00   20.60
5.04   20.60
 303 -2528 -2529 S 318 QPS ZG 0.00   20.63  4.90   20.63    303 -2528 -2529 S 321 QPS ZG 0.00   20.60
4.90   20.60
 303 -2529 -2530 S 304 QPS ZG 0.00   20.60  4.90   20.60    303 -2529 -2530 S 313 QPS ZG 0.00   20.63
4.90   20.63
 303 -2530 -2531 S 324 QPS ZG 0.00   20.63  2.63   20.63    303 -2530 -2531 S 325 QPS ZG 0.00   20.60
2.63   20.60
 305 -2532 -2533 S 306 QPS ZG 0.00   20.28  4.22   20.28    305 -2532 -2533 S 312 QPS ZG 0.00   20.60
4.22   20.60
 305 -2533 -2534 S 311 QPS ZG 0.00   20.28  4.93   20.28    305 -2533 -2534 S 323 QPS ZG 0.00   20.60
4.93   20.60
 305 -2534 -2535 S 311 QPS ZG 0.00   20.28  5.04   20.28    305 -2534 -2535 S 322 QPS ZG 0.00   20.60
5.04   20.60
 305 -2535 -2536 S 311 QPS ZG 0.00   20.28  4.90   20.28    305 -2535 -2536 S 321 QPS ZG 0.00   20.60
4.90   20.60
 305 -2536 -2537 S 304 QPS ZG 0.00   20.60  4.90   20.60    305 -2536 -2537 S 311 QPS ZG 0.00   20.28
4.90   20.28
 305 -2537 -2538 S 325 QPS ZG 0.00   20.60  2.63   20.60    305 -2537 -2538 S 326 QPS ZG 0.00   20.28
2.63   20.28
 306 -2546 -2547 S 305 QPS ZG 0.00   20.28  4.22   20.28    306 -2546 -2547 S 306 QPS ZG 0.00   20.28
4.22   20.28
 306 -2547 -2548 S 310 QPS ZG 0.00   20.28  4.93   20.28    306 -2547 -2548 S 311 QPS ZG 0.00   20.28
4.93   20.28
 306 -2548 -2549 S 310 QPS ZG 0.00   20.28  5.04   20.28    306 -2548 -2549 S 311 QPS ZG 0.00   20.28
5.04   20.28
 306 -2549 -2550 S 310 QPS ZG 0.00   20.28  4.90   20.28    306 -2549 -2550 S 311 QPS ZG 0.00   20.28
4.90   20.28
 306 -2550 -2551 S 310 QPS ZG 0.00   20.28  4.90   20.28    306 -2550 -2551 S 311 QPS ZG 0.00   20.28
4.90   20.28
 306 -2551 -2552 S 326 QPS ZG 0.00   20.28  2.63   20.28    306 -2551 -2552 S 327 QPS ZG 0.00   20.28
2.63   20.28
 307 -2553 -2554 S 300 QPS ZG 0.00   20.28  4.22   20.28    307 -2553 -2554 S 305 QPS ZG 0.00   20.28
4.22   20.28
 307 -2554 -2555 S 309 QPS ZG 0.00   20.28  4.93   20.28    307 -2554 -2555 S 310 QPS ZG 0.00   20.28
4.93   20.28
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307 -2555 -2556 S 309 QPS ZG 0.00 20.28 5.04 20.28 307 -2555 -2556 S 310 QPS ZG 0.00 20.28
5.04 20.28
307 -2556 -2557 S 309 QPS ZG 0.00 20.28 4.90 20.28 307 -2556 -2557 S 310 QPS ZG 0.00 20.28
4.90 20.28
307 -2557 -2558 S 309 QPS ZG 0.00 20.28 4.90 20.28 307 -2557 -2558 S 310 QPS ZG 0.00 20.28
4.90 20.28
307 -2558 -2559 S 327 QPS ZG 0.00 20.28 2.63 20.28 307 -2558 -2559 S 328 QPS ZG 0.00 20.28
2.63 20.28
308 -2567 -2568 S 300 QPS ZG 0.00 20.28 4.22 20.28 308 -2567 -2568 S 303 QPS ZG 0.00 20.28
4.22 20.28
308 -2568 -2569 S 308 QPS ZG 0.00 20.28 4.93 20.28 308 -2568 -2569 S 309 QPS ZG 0.00 20.28
4.93 20.28
308 -2569 -2570 S 308 QPS ZG 0.00 20.28 5.04 20.28 308 -2569 -2570 S 309 QPS ZG 0.00 20.28
5.04 20.28
308 -2570 -2571 S 308 QPS ZG 0.00 20.28 4.90 20.28 308 -2570 -2571 S 309 QPS ZG 0.00 20.28
4.90 20.28
308 -2571 -2572 S 308 QPS ZG 0.00 20.28 4.90 20.28 308 -2571 -2572 S 309 QPS ZG 0.00 20.28
4.90 20.28
308 -2572 -2573 S 328 QPS ZG 0.00 20.28 2.63 20.28 308 -2572 -2573 S 329 QPS ZG 0.00 20.28
2.63 20.28
309 322 323 S 303 QPS ZG 0.00 20.28 4.22 20.28 309 322 323 S 331 QPS ZG 0.00 30.29
4.22 30.29
309 323 324 S 308 QPS ZG 0.00 20.28 4.93 20.28 309 323 324 S 317 QPS ZG 0.00 30.29
4.93 30.29
309 324 325 S 308 QPS ZG 0.00 20.28 5.04 20.28 309 324 325 S 317 QPS ZG 0.00 30.29
5.04 30.29
309 325 326 S 308 QPS ZG 0.00 20.28 4.90 20.28 309 325 326 S 317 QPS ZG 0.00 30.29
4.90 30.29
309 326 327 S 308 QPS ZG 0.00 20.28 4.90 20.28 309 326 327 S 317 QPS ZG 0.00 30.29
4.90 30.29
309 327 328 S 329 QPS ZG 0.00 20.28 2.63 20.28 309 327 328 S 332 QPS ZG 0.00 30.29
2.63 30.29
310 -2560 -2561 S 316 QPS ZG 0.00 30.04 4.22 30.04 310 -2560 -2561 S 331 QPS ZG 0.00 30.29
4.22 30.29
310 -2561 -2562 S 301 QPS ZG 0.00 30.04 4.93 30.04 310 -2561 -2562 S 317 QPS ZG 0.00 30.29
4.93 30.29
310 -2562 -2563 S 301 QPS ZG 0.00 30.04 5.04 30.04 310 -2562 -2563 S 317 QPS ZG 0.00 30.29
5.04 30.29
310 -2563 -2564 S 301 QPS ZG 0.00 30.04 4.90 30.04 310 -2563 -2564 S 317 QPS ZG 0.00 30.29
4.90 30.29
310 -2564 -2565 S 301 QPS ZG 0.00 30.04 4.90 30.04 310 -2564 -2565 S 317 QPS ZG 0.00 30.29
4.90 30.29
310 -2565 -2566 S 314 QPS ZG 0.00 30.04 2.63 30.04 310 -2565 -2566 S 332 QPS ZG 0.00 30.29
2.63 30.29
311 -2539 -2540 S 302 QPS ZG 0.00 30.25 4.22 30.25 311 -2539 -2540 S 316 QPS ZG 0.00 30.04
4.22 30.04
311 -2540 -2541 S 301 QPS ZG 0.00 30.04 4.93 30.04 311 -2540 -2541 S 315 QPS ZG 0.00 30.25
4.93 30.25
311 -2541 -2542 S 301 QPS ZG 0.00 30.04 5.04 30.04 311 -2541 -2542 S 315 QPS ZG 0.00 30.25
5.04 30.25
311 -2542 -2543 S 301 QPS ZG 0.00 30.04 4.90 30.04 311 -2542 -2543 S 315 QPS ZG 0.00 30.25
4.90 30.25
311 -2543 -2544 S 301 QPS ZG 0.00 30.04 4.90 30.04 311 -2543 -2544 S 315 QPS ZG 0.00 30.25
4.90 30.25
311 -2544 -2545 S 314 QPS ZG 0.00 30.04 2.63 30.04 311 -2544 -2545 S 330 QPS ZG 0.00 30.25
2.63 30.25
312 317 312 S 302 QPS ZG 0.00 30.25 4.22 30.25 312 312 313 S 315 QPS ZG 0.00 30.25
4.93 30.25
312 313 314 S 315 QPS ZG 0.00 30.25 5.04 30.25 312 314 315 S 315 QPS ZG 0.00 30.25
4.90 30.25
312 315 316 S 315 QPS ZG 0.00 30.25 4.90 30.25 312 316 318 S 330 QPS ZG 0.00 30.25
2.63 30.25
501 -1601 -1600 S 500 QPS ZG 0.00 1157.40 2.61 1157.40 501 -1601 -1600 S 502 QPS ZG 0.00 632.50
2.61 632.50
2000 218 201 S 202 QPS ZG 0.00 0.00 4.10 8.75

ELENCO CARICHI ASTE

CONDIZIONE DI CARICO 2: PERMANENTI NST

CARICHI DISTRIBUITI

Asta N1 N2 E NE T DC Xi Qi Xf Qf Asta N1 N2 E NE T DC Xi Qi

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Xf     Qf
                                  <m> <daN/m>  <m>  <daN/m>                                  <m> <daN/m>
<m>  <daN/m>
-------------------------------------------------------   ------------------------------------------
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   0 -2327 -2348 S 209 QPN ZG 0.00  252.00  0.34  252.00      0 -2348 -2351 S 209 QPN ZG 0.00  252.00
0.34  252.00
   0 -2351 -2355 S 209 QPN ZG 0.00  252.00  0.34  252.00      0 -2355 -2358 S 209 QPN ZG 0.00  252.00
0.34  252.00
   0 -2358 -2364 S 209 QPN ZG 0.00  252.00  0.34  252.00      0 -2364 -2367 S 209 QPN ZG 0.00  252.00
0.34  252.00
   0 -2367 -2373 S 209 QPN ZG 0.00  252.00  0.34  252.00      0 -2373 -2374 S 209 QPN ZG 0.00  252.00
0.34  252.00
   0 -2352 -2328 S 209 QPN ZG 0.00  252.00  0.68  252.00      0 -2359 -2352 S 209 QPN ZG 0.00  252.00
0.68  252.00
   0 -2368 -2359 S 209 QPN ZG 0.00  252.00  0.68  252.00      0 -2353 -2330 S 208 QPN ZG 0.00  265.20
0.68  265.20
   0 -2375 -2368 S 209 QPN ZG 0.00  252.00  0.68  252.00      0 -2360 -2353 S 208 QPN ZG 0.00  265.20
0.68  265.20
   0 -2369 -2360 S 208 QPN ZG 0.00  265.20  0.68  265.20      0 -2377 -2369 S 208 QPN ZG 0.00  265.20
0.68  265.20
   0 -2331 -2354 S 203 QPN ZG 0.00    0.00  0.22  562.80      0 -2331 -2354 S 208 QPN ZG 0.00  265.20
0.68  265.20
   0 -2331 -2354 S 203 QPN ZG 0.22  562.80  0.68  562.80      0 -2354 -2361 S 203 QPN ZG 0.00  562.80
0.68  562.80
   0 -2354 -2361 S 208 QPN ZG 0.00  265.20  0.68  265.20      0 -2361 -2370 S 203 QPN ZG 0.00  562.80
0.68  562.80
   0 -2361 -2370 S 208 QPN ZG 0.00  265.20  0.68  265.20      0 -2370   218 S 203 QPN ZG 0.00  562.80
0.68  562.80
   0 -2370   218 S 208 QPN ZG 0.00  265.20  0.68  265.20      0 -1536 -1537 S 500 QPN ZG 0.00  257.20
0.48  257.20
   0 -2331 -2332 S 203 QPN ZG 0.00    0.00 14.07    8.80      0 -1537 -1538 S 500 QPN ZG 0.00  257.20
0.48  257.20
   0 -1538 -1539 S 500 QPN ZG 0.00  257.20  0.48  257.20      0 -1539 -1540 S 500 QPN ZG 0.00  257.20
0.48  257.20
   0 -1540 -1541 S 500 QPN ZG 0.00  257.20  0.48  257.20      0 -1541 -1542 S 500 QPN ZG 0.00  257.20
0.48  257.20
   0 -1542 -1543 S 500 QPN ZG 0.00  257.20  0.48  257.20      0   218   203 S 203 QPN ZG 0.00    2.00
14.07    0.00
   0 -1543 -1544 S 500 QPN ZG 0.00  257.20  0.48  257.20      0 -1544 -1545 S 500 QPN ZG 0.00  257.20
0.48  257.20
   0 -1545 -1546 S 500 QPN ZG 0.00  257.20  0.48  257.20      0 -1546 -1547 S 500 QPN ZG 0.00  257.20
0.48  257.20
   0 -1547 -1548 S 500 QPN ZG 0.00  257.20  0.48  257.20      0 -1548 -1549 S 500 QPN ZG 0.00  257.20
0.48  257.20
   0 -1549 -1550 S 500 QPN ZG 0.00  257.20  0.48  257.20      0 -1593 -1592 S 500 QPN ZG 0.00  257.20
0.43  257.20
   0 -1550 -1551 S 500 QPN ZG 0.00  257.20  0.48  257.20      0 -1594 -1593 S 500 QPN ZG 0.00  257.20
0.43  257.20
   0 -1551 -1552 S 500 QPN ZG 0.00  257.20  0.48  257.20      0 -1595 -1594 S 500 QPN ZG 0.00  257.20
0.43  257.20
   0 -1596 -1595 S 500 QPN ZG 0.00  257.20  0.43  257.20      0 -1596 -1595 S 502 QPN ZG 0.00  126.50
0.43  126.50
   0 -1597 -1596 S 500 QPN ZG 0.00  257.20  0.43  257.20      0 -1597 -1596 S 502 QPN ZG 0.00  126.50
0.43  126.50
   0 -1553 -1554 S 500 QPN ZG 0.00  257.20  0.48  257.20      0 -1598 -1597 S 500 QPN ZG 0.00  257.20
0.43  257.20
   0 -1598 -1597 S 502 QPN ZG 0.00  126.50  0.43  126.50      0 -1599 -1598 S 500 QPN ZG 0.00  257.20
0.43  257.20
   0 -1599 -1598 S 502 QPN ZG 0.00  126.50  0.43  126.50      0 -1601 -2580 S 500 QPN ZG 0.00  257.20
0.32  257.20
   0 -1601 -2580 S 503 QPN ZG 0.15  126.50  0.32  126.50      0 -1601 -2580 S 503 QPN ZG 0.00    0.00
0.15  126.50
   0 -2332 -2333 S 205 QPN ZG 0.00  126.50  0.43  126.50      0 -1552 -1553 S 500 QPN ZG 0.00  257.20
0.48  257.20
   0 -1600 -1599 S 500 QPN ZG 0.00  257.20  0.43  257.20      0 -1600 -1599 S 502 QPN ZG 0.00  126.50
0.43  126.50
   0 -1653 -1654 S 502 QPN ZG 0.00  126.50  0.28  126.50      0 -2333 -2334 S 205 QPN ZG 0.00  126.50
0.43  126.50
   0 -1554 -1555 S 500 QPN ZG 0.00  257.20  0.48  257.20      0 -1555 -1556 S 500 QPN ZG 0.00  257.20
0.48  257.20
   0 -1649 -1650 S 502 QPN ZG 0.00  126.50  0.43  126.50      0 -1651 -1652 S 502 QPN ZG 0.00  126.50
0.43  126.50
```

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   0 -1652 -1653 S 502 QPN ZG 0.00  126.50  0.43  126.50      0 -1654 -1655 S 502 QPN ZG 0.00  126.50
0.60  126.50
   0 -1655 -1656 S 502 QPN ZG 0.00  126.50  0.45  126.50      0 -1601 -1661 S 502 QPN ZG 0.00    7.49
2.53    0.00
   0 -1601 -1661 S 503 QPN ZG 0.00    0.00  2.53    7.49      0 -1660 -1661 S 502 QPN ZG 0.00  126.50
0.10  126.50
   0 -1660 -1661 S 502 QPN ZG 0.10  126.50  0.26    0.00      0 -2356 -2349 S 203 QPN ZG 0.00  562.80
0.42  562.80
   0 -2365 -2362 S 203 QPN ZG 0.00  562.80  0.42  562.80      0 -1556 -1557 S 500 QPN ZG 0.00  257.20
0.48  257.20
   0 -1657 -1658 S 502 QPN ZG 0.00  126.50  0.45  126.50      0 -2349 -2332 S 203 QPN ZG 0.00  562.80
0.42  562.80
   0 -2362 -2356 S 203 QPN ZG 0.00  562.80  0.42  562.80      0 -2335 -2336 S 205 QPN ZG 0.00  126.50
0.43  126.50
   0 -1557 -1558 S 500 QPN ZG 0.00  257.20  0.48  257.20      0 -1650 -1651 S 502 QPN ZG 0.00  126.50
0.43  126.50
   0 -2371 -2365 S 203 QPN ZG 0.00  562.80  0.42  562.80      0 -2336 -2337 S 205 QPN ZG 0.00  126.50
0.43  126.50
   0   203 -2371 S 203 QPN ZG 0.00    0.00  0.05  562.80      0   203 -2371 S 203 QPN ZG 0.05  562.80
0.42  562.80
   0   203 -2378 S 205 QPN ZG 0.00  126.50  0.43  126.50      0   203 -2378 T 103 QPN ZG 0.00  780.00
0.43  780.00
   0 -1558 -1559 S 500 QPN ZG 0.00  257.20  0.48  257.20      0 -1560 -1561 S 500 QPN ZG 0.00  257.20
0.48  257.20
   0 -2580 -1602 S 500 QPN ZG 0.00  257.20  0.32  257.20      0 -2580 -1602 S 503 QPN ZG 0.00  126.50
0.32  126.50
   0 -1602 -1603 S 500 QPN ZG 0.00  257.20  0.49  257.20      0 -1602 -1603 S 503 QPN ZG 0.00  126.50
0.49  126.50
   0 -2378 -2379 S 205 QPN ZG 0.00  126.50  0.43  126.50      0 -2378 -2379 T 103 QPN ZG 0.00  780.00
0.43  780.00
   0 -2379 -2380 S 205 QPN ZG 0.00  126.50  0.43  126.50      0 -2379 -2380 T 103 QPN ZG 0.00  780.00
0.43  780.00
   0 -1656 -1657 S 502 QPN ZG 0.00  126.50  0.45  126.50      0 -2334 -2335 S 205 QPN ZG 0.00  126.50
0.43  126.50
   0 -1603 -1604 S 500 QPN ZG 0.00  257.20  0.49  257.20      0 -1603 -1604 S 503 QPN ZG 0.00  126.50
0.49  126.50
   0 -1604 -1605 S 500 QPN ZG 0.00  257.20  0.49  257.20      0 -1604 -1605 S 503 QPN ZG 0.00  126.50
0.49  126.50
   0 -1659 -1660 S 502 QPN ZG 0.00  126.50  0.26  126.50      0 -2381 -2382 S 205 QPN ZG 0.00  126.50
0.28  126.50
   0 -2381 -2382 T 103 QPN ZG 0.00  780.00  0.28  780.00      0 -1605 -1606 S 500 QPN ZG 0.00  257.20
0.49  257.20
   0 -1605 -1606 S 503 QPN ZG 0.00  126.50  0.49  126.50      0 -1606 -1607 S 500 QPN ZG 0.00  257.20
0.49  257.20
   0 -1606 -1607 S 503 QPN ZG 0.00  126.50  0.49  126.50      0 -1607 -1608 S 500 QPN ZG 0.00  257.20
0.49  257.20
   0 -1607 -1608 S 503 QPN ZG 0.00  126.50  0.49  126.50      0 -1662 -1663 S 503 QPN ZG 0.00  126.50
0.49  126.50
   0 -1663 -1664 S 503 QPN ZG 0.00  126.50  0.49  126.50      0 -2380 -2381 S 205 QPN ZG 0.00  126.50
0.43  126.50
   0 -2380 -2381 T 103 QPN ZG 0.00  780.00  0.43  780.00      0 -1561 -1562 S 500 QPN ZG 0.00  257.20
0.48  257.20
   0 -1658 -1659 S 502 QPN ZG 0.00  126.50  0.45  126.50      0 -1661 -1662 S 503 QPN ZG 0.00  126.50
0.49  126.50
   0 -1664 -1665 S 503 QPN ZG 0.00  126.50  0.49  126.50      0 -1559 -1560 S 500 QPN ZG 0.00  257.20
0.48  257.20
   0   217 -2590 S 206 QPN ZG 0.00    0.00  0.15  126.50      0   217 -2590 S 206 QPN ZG 0.15  126.50
0.32  126.50
   0   217   204 S 205 QPN ZG 0.00    7.49  2.53    0.00      0   217   204 S 206 QPN ZG 0.00    0.00
2.53    7.49
   0 -1608 -1609 S 500 QPN ZG 0.00  257.20  0.49  257.20      0 -1608 -1609 S 503 QPN ZG 0.00  126.50
0.49  126.50
   0 -1665 -1666 S 503 QPN ZG 0.00  126.50  0.49  126.50      0 -1666 -1667 S 503 QPN ZG 0.00  126.50
0.49  126.50
   0 -1610 -1611 S 500 QPN ZG 0.00  257.20  0.49  257.20      0 -1610 -1611 S 503 QPN ZG 0.00  126.50
0.49  126.50
   0 -2590 -2338 S 206 QPN ZG 0.00  126.50  0.32  126.50      0 -2339 -2340 S 206 QPN ZG 0.00  126.50
0.49  126.50
   0 -2384   204 S 205 QPN ZG 0.00  126.50  0.10  126.50      0 -2384   204 T 103 QPN ZG 0.00  780.00
0.26  780.00
   0 -2384   204 S 205 QPN ZG 0.10  126.50  0.26    0.00      0 -1609 -1610 S 500 QPN ZG 0.00  257.20
0.49  257.20
   0 -1609 -1610 S 503 QPN ZG 0.00  126.50  0.49  126.50      0 -1611 -1615 S 501 QPN ZG 0.00   60.00
```

```
0.42   60.00
   0 -1615 -1623 S 501 QPN ZG 0.00   60.00  0.42   60.00      0 -1611 -1612 S 500 QPN ZG 0.00  257.20
1.50  257.20
   0 -1667 -1668 S 503 QPN ZG 0.00  126.50  0.49  126.50      0 -1623 -1630 S 501 QPN ZG 0.00   60.00
0.42   60.00
   0 -1668 -1669 S 503 QPN ZG 0.00  126.50  0.49  126.50      0 -1616 -1612 S 501 QPN ZG 0.00   60.00
0.42   60.00
   0 -1669 -1670 S 503 QPN ZG 0.00  126.50  0.49  126.50      0 -2383 -2384 S 205 QPN ZG 0.00  126.50
0.26  126.50
   0 -2383 -2384 T 103 QPN ZG 0.00  780.00  0.26  780.00      0 -1630 -1634 S 501 QPN ZG 0.00   60.00
0.42   60.00
   0 -1634 -1641 S 501 QPN ZG 0.00   60.00  0.42   60.00      0 -1641 -1671 S 501 QPN ZG 0.00   60.00
0.42   60.00
   0   204 -2385 S 206 QPN ZG 0.00  126.50  0.49  126.50      0   204 -2385 T 104 QPN ZG 0.00  780.00
0.49  780.00
   0 -2338 -2339 S 206 QPN ZG 0.00  126.50  0.49  126.50      0 -1624 -1616 S 501 QPN ZG 0.00   60.00
0.42   60.00
   0 -1670 -1671 S 503 QPN ZG 0.00  126.50  0.49  126.50      0 -1631 -1624 S 501 QPN ZG 0.00   60.00
0.42   60.00
   0 -2340 -2341 S 206 QPN ZG 0.00  126.50  0.49  126.50      0 -2386 -2387 S 206 QPN ZG 0.00  126.50
0.49  126.50
   0 -2386 -2387 T 104 QPN ZG 0.00  780.00  0.49  780.00      0 -1635 -1631 S 501 QPN ZG 0.00   60.00
0.42   60.00
   0 -1674 -1642 S 501 QPN ZG 0.00   60.00  0.42   60.00      0 -2342 -2343 S 206 QPN ZG 0.00  126.50
0.49  126.50
   0 -2343 -2344 S 206 QPN ZG 0.00  126.50  0.49  126.50      0 -2385 -2386 S 206 QPN ZG 0.00  126.50
0.49  126.50
   0 -2385 -2386 T 104 QPN ZG 0.00  780.00  0.49  780.00      0 -1642 -1635 S 501 QPN ZG 0.00   60.00
0.42   60.00
   0 -2341 -2342 S 206 QPN ZG 0.00  126.50  0.49  126.50      0 -2344 -2345 S 206 QPN ZG 0.00  126.50
0.49  126.50
   0 -2345 -2346 S 206 QPN ZG 0.00  126.50  0.49  126.50      0 -2387 -2388 S 206 QPN ZG 0.00  126.50
0.49  126.50
   0 -2387 -2388 T 104 QPN ZG 0.00  780.00  0.49  780.00      0 -2346 -2347 S 206 QPN ZG 0.00  126.50
0.49  126.50
   0 -2388 -2389 S 206 QPN ZG 0.00  126.50  0.49  126.50      0 -2388 -2389 T 104 QPN ZG 0.00  780.00
0.49  780.00
   0 -2389 -2390 S 206 QPN ZG 0.00  126.50  0.49  126.50      0 -2389 -2390 T 104 QPN ZG 0.00  780.00
0.49  780.00
   0 -2390 -2391 S 206 QPN ZG 0.00  126.50  0.49  126.50      0 -2390 -2391 T 104 QPN ZG 0.00  780.00
0.49  780.00
   0 -2391 -2392 S 206 QPN ZG 0.00  126.50  0.49  126.50      0 -2391 -2392 T 104 QPN ZG 0.00  780.00
0.49  780.00
   0 -2392 -2393 S 206 QPN ZG 0.00  126.50  0.49  126.50      0 -2392 -2393 T 104 QPN ZG 0.00  780.00
0.49  780.00
   0 -2393   205 S 206 QPN ZG 0.00  126.50  0.49  126.50      0 -2393   205 T 104 QPN ZG 0.00  780.00
0.49  780.00
 201 -2337   217 S 205 QPN ZG 0.00  126.50  2.61  126.50    204 -2382 -2383 S 205 QPN ZG 0.00  126.50
2.40  126.50
 204 -2382 -2383 T 103 QPN ZG 0.00  780.00  2.40  780.00    212 -2394   212 T 105 QPN ZG 0.00  562.50
0.46  562.50
 212 -2395 -2394 T 105 QPN ZG 0.00  562.50  0.46  562.50    212 -2396 -2395 T 105 QPN ZG 0.00  562.50
0.46  562.50
 212 -2397 -2396 T 105 QPN ZG 0.00  562.50  0.46  562.50    212 -2398 -2397 T 105 QPN ZG 0.00  562.50
0.46  562.50
 212 -2399 -2398 T 105 QPN ZG 0.00  562.50  0.46  562.50    212   213   214 T 106 QPN ZG 0.00  562.50
5.04  562.50
 212   214   215 T 107 QPN ZG 0.00  562.50  4.90  562.50    212   215   216 T 108 QPN ZG 0.00  562.50
4.90  562.50
 215   218   211 S 202 QPN ZG 0.00    0.00  0.05  205.00    215   218   211 S 202 QPN ZG 0.05  205.00
10.21  205.00
 216   206   201 S 202 QPN ZG 0.00  205.00  5.08  205.00    216   206   201 T 208 QPN ZG 0.00 1348.76
5.08  780.00
 216   206   201 S 207 QPN ZG 0.00  246.50  5.08  246.50    216   212   206 S 202 QPN ZG 0.00  205.00
5.08  205.00
 216   212   206 T 208 QPN ZG 4.60 1402.50  5.08 1348.76    216   212   206 T 208 QPN ZG 0.00  562.50
4.60 1402.50
 216   212   206 S 207 QPN ZG 0.00  246.50  5.08  246.50    217   207   202 S 204 QPN ZG 0.00  252.00
5.08  252.00
 217   207   202 S 207 QPN ZG 0.00  246.50  5.08  246.50    217   213   207 S 204 QPN ZG 0.00  252.00
5.08  252.00
 217   213   207 S 207 QPN ZG 0.00  246.50  5.08  246.50    218   208   203 S 200 QPN ZG 0.00  171.50
5.08  171.50
```

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 218   208   203 S 204 QPN ZG 0.00  252.00  5.08  252.00    218   214   208 S 200 QPN ZG 0.00  171.50
5.08  171.50
 218   214   208 S 204 QPN ZG 0.00  252.00  5.08  252.00    219   209   204 S 200 QPN ZG 0.00  171.50
5.08  171.50
 219   209   204 S 201 QPN ZG 0.00  171.50  5.08  171.50    219   215   209 S 200 QPN ZG 0.00  171.50
5.08  171.50
 219   215   209 S 201 QPN ZG 0.00  171.50  5.08  171.50    220   210   205 S 201 QPN ZG 0.00  171.50
5.08  171.50
 220   216   210 S 201 QPN ZG 0.00  171.50  5.08  171.50    222   201   202 T 101 QPN ZG 0.00  780.00
4.93  780.00
 222   202   203 T 102 QPN ZG 0.00  780.00  5.04  780.00    300   213 -2399 T 105 QPN ZG 0.00  562.50
2.15  562.50
 302 -2518 -2519 S 307 QPN ZG 0.00  123.75  4.22  123.75    302 -2519 -2520 S 320 QPN ZG 0.00  123.75
4.93  123.75
 302 -2520 -2521 S 319 QPN ZG 0.00  123.75  5.04  123.75    302 -2521 -2522 S 318 QPN ZG 0.00  123.75
4.90  123.75
 302 -2522 -2523 S 313 QPN ZG 0.00  123.75  4.90  123.75    302 -2523 -2524 S 324 QPN ZG 0.00  123.75
2.63  123.75
 303 -2525 -2526 S 307 QPN ZG 0.00  123.75  4.22  123.75    303 -2525 -2526 S 312 QPN ZG 0.00  123.60
4.22  123.60
 303 -2526 -2527 S 320 QPN ZG 0.00  123.75  4.93  123.75    303 -2526 -2527 S 323 QPN ZG 0.00  123.60
4.93  123.60
 303 -2527 -2528 S 319 QPN ZG 0.00  123.75  5.04  123.75    303 -2527 -2528 S 322 QPN ZG 0.00  123.60
5.04  123.60
 303 -2528 -2529 S 318 QPN ZG 0.00  123.75  4.90  123.75    303 -2528 -2529 S 321 QPN ZG 0.00  123.60
4.90  123.60
 303 -2529 -2530 S 304 QPN ZG 0.00  123.60  4.90  123.60    303 -2529 -2530 S 313 QPN ZG 0.00  123.75
4.90  123.75
 303 -2530 -2531 S 324 QPN ZG 0.00  123.75  2.63  123.75    303 -2530 -2531 S 325 QPN ZG 0.00  123.60
2.63  123.60
 305 -2532 -2533 S 306 QPN ZG 0.00  121.69  4.22  121.69    305 -2532 -2533 S 312 QPN ZG 0.00  123.60
4.22  123.60
 305 -2533 -2534 S 311 QPN ZG 0.00  121.69  4.93  121.69    305 -2533 -2534 S 323 QPN ZG 0.00  123.60
4.93  123.60
 305 -2534 -2535 S 311 QPN ZG 0.00  121.69  5.04  121.69    305 -2534 -2535 S 322 QPN ZG 0.00  123.60
5.04  123.60
 305 -2535 -2536 S 311 QPN ZG 0.00  121.69  4.90  121.69    305 -2535 -2536 S 321 QPN ZG 0.00  123.60
4.90  123.60
 305 -2536 -2537 S 304 QPN ZG 0.00  123.60  4.90  123.60    305 -2536 -2537 S 311 QPN ZG 0.00  121.69
4.90  121.69
 305 -2537 -2538 S 325 QPN ZG 0.00  123.60  2.63  123.60    305 -2537 -2538 S 326 QPN ZG 0.00  121.69
2.63  121.69
 306 -2546 -2547 S 305 QPN ZG 0.00  121.69  4.22  121.69    306 -2546 -2547 S 306 QPN ZG 0.00  121.69
4.22  121.69
 306 -2547 -2548 S 310 QPN ZG 0.00  121.69  4.93  121.69    306 -2547 -2548 S 311 QPN ZG 0.00  121.69
4.93  121.69
 306 -2548 -2549 S 310 QPN ZG 0.00  121.69  5.04  121.69    306 -2548 -2549 S 311 QPN ZG 0.00  121.69
5.04  121.69
 306 -2549 -2550 S 310 QPN ZG 0.00  121.69  4.90  121.69    306 -2549 -2550 S 311 QPN ZG 0.00  121.69
4.90  121.69
 306 -2550 -2551 S 310 QPN ZG 0.00  121.69  4.90  121.69    306 -2550 -2551 S 311 QPN ZG 0.00  121.69
4.90  121.69
 306 -2551 -2552 S 326 QPN ZG 0.00  121.69  2.63  121.69    306 -2551 -2552 S 327 QPN ZG 0.00  121.69
2.63  121.69
 307 -2553 -2554 S 300 QPN ZG 0.00  121.69  4.22  121.69    307 -2553 -2554 S 305 QPN ZG 0.00  121.69
4.22  121.69
 307 -2554 -2555 S 309 QPN ZG 0.00  121.69  4.93  121.69    307 -2554 -2555 S 310 QPN ZG 0.00  121.69
4.93  121.69
 307 -2555 -2556 S 309 QPN ZG 0.00  121.69  5.04  121.69    307 -2555 -2556 S 310 QPN ZG 0.00  121.69
5.04  121.69
 307 -2556 -2557 S 309 QPN ZG 0.00  121.69  4.90  121.69    307 -2556 -2557 S 310 QPN ZG 0.00  121.69
4.90  121.69
 307 -2557 -2558 S 309 QPN ZG 0.00  121.69  4.90  121.69    307 -2557 -2558 S 310 QPN ZG 0.00  121.69
4.90  121.69
 307 -2558 -2559 S 327 QPN ZG 0.00  121.69  2.63  121.69    307 -2558 -2559 S 328 QPN ZG 0.00  121.69
2.63  121.69
 308 -2567 -2568 S 300 QPN ZG 0.00  121.69  4.22  121.69    308 -2567 -2568 S 303 QPN ZG 0.00  121.69
4.22  121.69
 308 -2568 -2569 S 308 QPN ZG 0.00  121.69  4.93  121.69    308 -2568 -2569 S 309 QPN ZG 0.00  121.69
4.93  121.69
 308 -2569 -2570 S 308 QPN ZG 0.00  121.69  5.04  121.69    308 -2569 -2570 S 309 QPN ZG 0.00  121.69
5.04  121.69
 308 -2570 -2571 S 308 QPN ZG 0.00  121.69  4.90  121.69    308 -2570 -2571 S 309 QPN ZG 0.00  121.69
```

4.90 121.69
 308 -2571 -2572 S 308 QPN ZG 0.00 121.69 4.90 121.69   308 -2571 -2572 S 309 QPN ZG 0.00 121.69
4.90 121.69
 308 -2572 -2573 S 328 QPN ZG 0.00 121.69 2.63 121.69   308 -2572 -2573 S 329 QPN ZG 0.00 121.69
2.63 121.69
 309   322   323 S 303 QPN ZG 0.00 121.69 4.22 121.69   309   322   323 S 331 QPN ZG 0.00 181.76
4.22 181.76
 309   323   324 S 308 QPN ZG 0.00 121.69 4.93 121.69   309   323   324 S 317 QPN ZG 0.00 181.76
4.93 181.76
 309   324   325 S 308 QPN ZG 0.00 121.69 5.04 121.69   309   324   325 S 317 QPN ZG 0.00 181.76
5.04 181.76
 309   325   326 S 308 QPN ZG 0.00 121.69 4.90 121.69   309   325   326 S 317 QPN ZG 0.00 181.76
4.90 181.76
 309   326   327 S 308 QPN ZG 0.00 121.69 4.90 121.69   309   326   327 S 317 QPN ZG 0.00 181.76
4.90 181.76
 309   327   328 S 329 QPN ZG 0.00 121.69 2.63 121.69   309   327   328 S 332 QPN ZG 0.00 181.76
2.63 181.76
 310 -2560 -2561 S 316 QPN ZG 0.00 180.26 4.22 180.26   310 -2560 -2561 S 331 QPN ZG 0.00 181.76
4.22 181.76
 310 -2561 -2562 S 301 QPN ZG 0.00 180.26 4.93 180.26   310 -2561 -2562 S 317 QPN ZG 0.00 181.76
4.93 181.76
 310 -2562 -2563 S 301 QPN ZG 0.00 180.26 5.04 180.26   310 -2562 -2563 S 317 QPN ZG 0.00 181.76
5.04 181.76
 310 -2563 -2564 S 301 QPN ZG 0.00 180.26 4.90 180.26   310 -2563 -2564 S 317 QPN ZG 0.00 181.76
4.90 181.76
 310 -2564 -2565 S 301 QPN ZG 0.00 180.26 4.90 180.26   310 -2564 -2565 S 317 QPN ZG 0.00 181.76
4.90 181.76
 310 -2565 -2566 S 314 QPN ZG 0.00 180.26 2.63 180.26   310 -2565 -2566 S 332 QPN ZG 0.00 181.76
2.63 181.76
 311 -2539 -2540 S 302 QPN ZG 0.00 181.50 4.22 181.50   311 -2539 -2540 S 316 QPN ZG 0.00 180.26
4.22 180.26
 311 -2540 -2541 S 301 QPN ZG 0.00 180.26 4.93 180.26   311 -2540 -2541 S 315 QPN ZG 0.00 181.50
4.93 181.50
 311 -2541 -2542 S 301 QPN ZG 0.00 180.26 5.04 180.26   311 -2541 -2542 S 315 QPN ZG 0.00 181.50
5.04 181.50
 311 -2542 -2543 S 301 QPN ZG 0.00 180.26 4.90 180.26   311 -2542 -2543 S 315 QPN ZG 0.00 181.50
4.90 181.50
 311 -2543 -2544 S 301 QPN ZG 0.00 180.26 4.90 180.26   311 -2543 -2544 S 315 QPN ZG 0.00 181.50
4.90 181.50
 311 -2544 -2545 S 314 QPN ZG 0.00 180.26 2.63 180.26   311 -2544 -2545 S 330 QPN ZG 0.00 181.50
2.63 181.50
 312   317   312 S 302 QPN ZG 0.00 181.50 4.22 181.50   312   312   313 S 315 QPN ZG 0.00 181.50
4.93 181.50
 312   313   314 S 315 QPN ZG 0.00 181.50 5.04 181.50   312   314   315 S 315 QPN ZG 0.00 181.50
4.90 181.50
 312   315   316 S 315 QPN ZG 0.00 181.50 4.90 181.50   312   316   318 S 330 QPN ZG 0.00 181.50
2.63 181.50
 501 -1601 -1600 S 500 QPN ZG 0.00 257.20 2.61 257.20   501 -1601 -1600 S 502 QPN ZG 0.00 126.50
2.61 126.50
2000   218   201 S 202 QPN ZG 0.00   0.00 4.10   2.50

ELENCO CARICHI ASTE

CONDIZIONE DI CARICO 3: ACCIDENTALI

CARICHI DISTRIBUITI

Asta	N1	N2	E	NE	T	DC	Xi	Qi	Xf	Qf	Asta	N1	N2	E	NE	T	DC	Xi	Qi	Xf	Qf
							<m>	<daN/m>	<m>	<daN/m>								<m>	<daN/m>	<m>	<daN/m>
0	-2327	-2348	S	209	QA	ZG	0.00	1260.00	0.34	1260.00	0	-2348	-2351	S	209	QA	ZG	0.00	1260.00	0.34	1260.00
0	-2351	-2355	S	209	QA	ZG	0.00	1260.00	0.34	1260.00	0	-2355	-2358	S	209	QA	ZG	0.00	1260.00	0.34	1260.00
0	-2358	-2364	S	209	QA	ZG	0.00	1260.00	0.34	1260.00	0	-2364	-2367	S	209	QA	ZG	0.00	1260.00	0.34	1260.00
0	-2367	-2373	S	209	QA	ZG	0.00	1260.00	0.34	1260.00	0	-2373	-2374	S	209	QA	ZG	0.00	1260.00	0.34	1260.00
0	-2352	-2328	S	209	QA	ZG	0.00	1260.00	0.68	1260.00	0	-2359	-2352	S	209	QA	ZG	0.00	1260.00	0.68	1260.00

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   0 -2368 -2359 S 209 QA  ZG 0.00 1260.00  0.68 1260.00      0 -2353 -2330 S 208 QA  ZG 0.00 1326.00
0.68 1326.00
   0 -2375 -2368 S 209 QA  ZG 0.00 1260.00  0.68 1260.00      0 -2360 -2353 S 208 QA  ZG 0.00 1326.00
0.68 1326.00
   0 -2369 -2360 S 208 QA  ZG 0.00 1326.00  0.68 1326.00      0 -2377 -2369 S 208 QA  ZG 0.00 1326.00
0.68 1326.00
   0 -2331 -2354 S 203 QA  ZG 0.00    0.00  0.22 2814.00      0 -2331 -2354 S 208 QA  ZG 0.00 1326.00
0.68 1326.00
   0 -2331 -2354 S 203 QA  ZG 0.22 2814.00  0.68 2814.00      0 -2354 -2361 S 203 QA  ZG 0.00 2814.00
0.68 2814.00
   0 -2354 -2361 S 208 QA  ZG 0.00 1326.00  0.68 1326.00      0 -2361 -2370 S 203 QA  ZG 0.00 2814.00
0.68 2814.00
   0 -2361 -2370 S 208 QA  ZG 0.00 1326.00  0.68 1326.00      0 -2370   218 S 203 QA  ZG 0.00 2814.00
0.68 2814.00
   0 -2370   218 S 208 QA  ZG 0.00 1326.00  0.68 1326.00      0 -1536 -1537 S 500 QA  ZG 0.00  964.50
0.48  964.50
   0 -2331 -2332 S 203 QA  ZG 0.00    0.00 14.07   43.99      0 -1537 -1538 S 500 QA  ZG 0.00  964.50
0.48  964.50
   0 -1538 -1539 S 500 QA  ZG 0.00  964.50  0.48  964.50      0 -1539 -1540 S 500 QA  ZG 0.00  964.50
0.48  964.50
   0 -1540 -1541 S 500 QA  ZG 0.00  964.50  0.48  964.50      0 -1541 -1542 S 500 QA  ZG 0.00  964.50
0.48  964.50
   0 -1542 -1543 S 500 QA  ZG 0.00  964.50  0.48  964.50      0   218   203 S 203 QA  ZG 0.00   10.00
14.07    0.00
   0 -1543 -1544 S 500 QA  ZG 0.00  964.50  0.48  964.50      0 -1544 -1545 S 500 QA  ZG 0.00  964.50
0.48  964.50
   0 -1545 -1546 S 500 QA  ZG 0.00  964.50  0.48  964.50      0 -1546 -1547 S 500 QA  ZG 0.00  964.50
0.48  964.50
   0 -1547 -1548 S 500 QA  ZG 0.00  964.50  0.48  964.50      0 -1548 -1549 S 500 QA  ZG 0.00  964.50
0.48  964.50
   0 -1549 -1550 S 500 QA  ZG 0.00  964.50  0.48  964.50      0 -1593 -1592 S 500 QA  ZG 0.00  964.50
0.43  964.50
   0 -1550 -1551 S 500 QA  ZG 0.00  964.50  0.48  964.50      0 -1594 -1593 S 500 QA  ZG 0.00  964.50
0.43  964.50
   0 -1551 -1552 S 500 QA  ZG 0.00  964.50  0.48  964.50      0 -1595 -1594 S 500 QA  ZG 0.00  964.50
0.43  964.50
   0 -1596 -1595 S 500 QA  ZG 0.00  964.50  0.43  964.50      0 -1596 -1595 S 502 QA  ZG 0.00  506.00
0.43  506.00
   0 -1597 -1596 S 500 QA  ZG 0.00  964.50  0.43  964.50      0 -1597 -1596 S 502 QA  ZG 0.00  506.00
0.43  506.00
   0 -1553 -1554 S 500 QA  ZG 0.00  964.50  0.48  964.50      0 -1598 -1597 S 500 QA  ZG 0.00  964.50
0.43  964.50
   0 -1598 -1597 S 502 QA  ZG 0.00  506.00  0.43  506.00      0 -1599 -1598 S 500 QA  ZG 0.00  964.50
0.43  964.50
   0 -1599 -1598 S 502 QA  ZG 0.00  506.00  0.43  506.00      0 -1601 -2580 S 500 QA  ZG 0.00  964.50
0.32  964.50
   0 -1601 -2580 S 503 QA  ZG 0.15  506.00  0.32  506.00      0 -1601 -2580 S 503 QA  ZG 0.00    0.00
0.15  506.00
   0 -2332 -2333 S 205 QA  ZG 0.00  506.00  0.43  506.00      0 -1552 -1553 S 500 QA  ZG 0.00  964.50
0.48  964.50
   0 -1600 -1599 S 500 QA  ZG 0.00  964.50  0.43  964.50      0 -1600 -1599 S 502 QA  ZG 0.00  506.00
0.43  506.00
   0 -1653 -1654 S 502 QA  ZG 0.00  506.00  0.28  506.00      0 -2333 -2334 S 205 QA  ZG 0.00  506.00
0.43  506.00
   0 -1554 -1555 S 500 QA  ZG 0.00  964.50  0.48  964.50      0 -1555 -1556 S 500 QA  ZG 0.00  964.50
0.48  964.50
   0 -1649 -1650 S 502 QA  ZG 0.00  506.00  0.43  506.00      0 -1651 -1652 S 502 QA  ZG 0.00  506.00
0.43  506.00
   0 -1652 -1653 S 502 QA  ZG 0.00  506.00  0.43  506.00      0 -1654 -1655 S 502 QA  ZG 0.00  506.00
0.60  506.00
   0 -1655 -1656 S 502 QA  ZG 0.00  506.00  0.45  506.00      0 -1601 -1661 S 502 QA  ZG 0.00   29.95
2.53    0.00
   0 -1601 -1661 S 503 QA  ZG 0.00    0.00  2.53   29.95      0 -1660 -1661 S 502 QA  ZG 0.00  506.00
0.10  506.00
   0 -1660 -1661 S 502 QA  ZG 0.10  506.00  0.26    0.00      0 -2356 -2349 S 203 QA  ZG 0.00 2814.00
0.42 2814.00
   0 -2365 -2362 S 203 QA  ZG 0.00 2814.00  0.42 2814.00      0 -1556 -1557 S 500 QA  ZG 0.00  964.50
0.48  964.50
   0 -1657 -1658 S 502 QA  ZG 0.00  506.00  0.45  506.00      0 -2349 -2332 S 203 QA  ZG 0.00 2814.00
0.42 2814.00
   0 -2362 -2356 S 203 QA  ZG 0.00 2814.00  0.42 2814.00      0 -2335 -2336 S 205 QA  ZG 0.00  506.00
0.43  506.00
   0 -1557 -1558 S 500 QA  ZG 0.00  964.50  0.48  964.50      0 -1650 -1651 S 502 QA  ZG 0.00  506.00
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0.43  506.00
   0 -2371 -2365 S 203 QA  ZG 0.00 2814.00  0.42 2814.00      0 -2336 -2337 S 205 QA  ZG 0.00  506.00
0.43  506.00
   0   203 -2371 S 203 QA  ZG 0.00    0.00  0.05 2814.00      0   203 -2371 S 203 QA  ZG 0.05 2814.00
0.42 2814.00
   0   203 -2378 S 205 QA  ZG 0.00  506.00  0.43  506.00      0 -1558 -1559 S 500 QA  ZG 0.00  964.50
0.48  964.50
   0 -1560 -1561 S 500 QA  ZG 0.00  964.50  0.48  964.50      0 -2580 -1602 S 500 QA  ZG 0.00  964.50
0.32  964.50
   0 -2580 -1602 S 503 QA  ZG 0.00  506.00  0.32  506.00      0 -1602 -1603 S 500 QA  ZG 0.00  964.50
0.49  964.50
   0 -1602 -1603 S 503 QA  ZG 0.00  506.00  0.49  506.00      0 -2378 -2379 S 205 QA  ZG 0.00  506.00
0.43  506.00
   0 -2379 -2380 S 205 QA  ZG 0.00  506.00  0.43  506.00      0 -1656 -1657 S 502 QA  ZG 0.00  506.00
0.45  506.00
   0 -2334 -2335 S 205 QA  ZG 0.00  506.00  0.43  506.00      0 -1603 -1604 S 500 QA  ZG 0.00  964.50
0.49  964.50
   0 -1603 -1604 S 503 QA  ZG 0.00  506.00  0.49  506.00      0 -1604 -1605 S 500 QA  ZG 0.00  964.50
0.49  964.50
   0 -1604 -1605 S 503 QA  ZG 0.00  506.00  0.49  506.00      0 -1659 -1660 S 502 QA  ZG 0.00  506.00
0.26  506.00
   0 -2381 -2382 S 205 QA  ZG 0.00  506.00  0.28  506.00      0 -1605 -1606 S 500 QA  ZG 0.00  964.50
0.49  964.50
   0 -1605 -1606 S 503 QA  ZG 0.00  506.00  0.49  506.00      0 -1606 -1607 S 500 QA  ZG 0.00  964.50
0.49  964.50
   0 -1606 -1607 S 503 QA  ZG 0.00  506.00  0.49  506.00      0 -1607 -1608 S 500 QA  ZG 0.00  964.50
0.49  964.50
   0 -1607 -1608 S 503 QA  ZG 0.00  506.00  0.49  506.00      0 -1662 -1663 S 503 QA  ZG 0.00  506.00
0.49  506.00
   0 -1663 -1664 S 503 QA  ZG 0.00  506.00  0.49  506.00      0 -2380 -2381 S 205 QA  ZG 0.00  506.00
0.43  506.00
   0 -1561 -1562 S 500 QA  ZG 0.00  964.50  0.48  964.50      0 -1658 -1659 S 502 QA  ZG 0.00  506.00
0.45  506.00
   0 -1661 -1662 S 503 QA  ZG 0.00  506.00  0.49  506.00      0 -1664 -1665 S 503 QA  ZG 0.00  506.00
0.49  506.00
   0 -1559 -1560 S 500 QA  ZG 0.00  964.50  0.48  964.50      0   217 -2590 S 206 QA  ZG 0.00    0.00
0.15  506.00
   0   217 -2590 S 206 QA  ZG 0.15  506.00  0.32  506.00      0   217   204 S 205 QA  ZG 0.00   29.95
2.53    0.00
   0   217   204 S 206 QA  ZG 0.00    0.00  2.53   29.95      0 -1608 -1609 S 500 QA  ZG 0.00  964.50
0.49  964.50
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0.49  506.00
   0 -1666 -1667 S 503 QA  ZG 0.00  506.00  0.49  506.00      0 -1610 -1611 S 500 QA  ZG 0.00  964.50
0.49  964.50
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0.32  506.00
   0 -2339 -2340 S 206 QA  ZG 0.00  506.00  0.49  506.00      0 -2384   204 S 205 QA  ZG 0.00  506.00
0.10  506.00
   0 -2384   204 S 205 QA  ZG 0.10  506.00  0.26    0.00      0 -1609 -1610 S 500 QA  ZG 0.00  964.50
0.49  964.50
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0.42  225.00
   0 -1615 -1623 S 501 QA  ZG 0.00  225.00  0.42  225.00      0 -1611 -1612 S 500 QA  ZG 0.00  964.50
1.50  964.50
   0 -1667 -1668 S 503 QA  ZG 0.00  506.00  0.49  506.00      0 -1623 -1630 S 501 QA  ZG 0.00  225.00
0.42  225.00
   0 -1668 -1669 S 503 QA  ZG 0.00  506.00  0.49  506.00      0 -1616 -1612 S 501 QA  ZG 0.00  225.00
0.42  225.00
   0 -1669 -1670 S 503 QA  ZG 0.00  506.00  0.49  506.00      0 -2383 -2384 S 205 QA  ZG 0.00  506.00
0.26  506.00
   0 -1630 -1634 S 501 QA  ZG 0.00  225.00  0.42  225.00      0 -1634 -1641 S 501 QA  ZG 0.00  225.00
0.42  225.00
   0 -1641 -1671 S 501 QA  ZG 0.00  225.00  0.42  225.00      0   204 -2385 S 206 QA  ZG 0.00  506.00
0.49  506.00
   0 -2338 -2339 S 206 QA  ZG 0.00  506.00  0.49  506.00      0 -1624 -1616 S 501 QA  ZG 0.00  225.00
0.42  225.00
   0 -1670 -1671 S 503 QA  ZG 0.00  506.00  0.49  506.00      0 -1631 -1624 S 501 QA  ZG 0.00  225.00
0.42  225.00
   0 -2340 -2341 S 206 QA  ZG 0.00  506.00  0.49  506.00      0 -2386 -2387 S 206 QA  ZG 0.00  506.00
0.49  506.00
   0 -1635 -1631 S 501 QA  ZG 0.00  225.00  0.42  225.00      0 -1674 -1642 S 501 QA  ZG 0.00  225.00
0.42  225.00
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   0 -2342 -2343 S 206 QA  ZG 0.00  506.00  0.49  506.00      0 -2343 -2344 S 206 QA  ZG 0.00  506.00
0.49  506.00
   0 -2385 -2386 S 206 QA  ZG 0.00  506.00  0.49  506.00      0 -1642 -1635 S 501 QA  ZG 0.00  225.00
0.42  225.00
   0 -2341 -2342 S 206 QA  ZG 0.00  506.00  0.49  506.00      0 -2344 -2345 S 206 QA  ZG 0.00  506.00
0.49  506.00
   0 -2345 -2346 S 206 QA  ZG 0.00  506.00  0.49  506.00      0 -2387 -2388 S 206 QA  ZG 0.00  506.00
0.49  506.00
   0 -2346 -2347 S 206 QA  ZG 0.00  506.00  0.49  506.00      0 -2388 -2389 S 206 QA  ZG 0.00  506.00
0.49  506.00
   0 -2389 -2390 S 206 QA  ZG 0.00  506.00  0.49  506.00      0 -2390 -2391 S 206 QA  ZG 0.00  506.00
0.49  506.00
   0 -2391 -2392 S 206 QA  ZG 0.00  506.00  0.49  506.00      0 -2392 -2393 S 206 QA  ZG 0.00  506.00
0.49  506.00
   0 -2393   205 S 206 QA  ZG 0.00  506.00  0.49  506.00    201 -2337   217 S 205 QA  ZG 0.00  506.00
2.61  506.00
 204 -2382 -2383 S 205 QA  ZG 0.00  506.00  2.40  506.00    215   218   211 S 202 QA  ZG 0.00    0.00
0.05  615.00
 215   218   211 S 202 QA  ZG 0.05  615.00 10.21  615.00    216   206   201 S 202 QA  ZG 0.00  615.00
5.08  615.00
 216   206   201 S 207 QA  ZG 0.00  739.50  5.08  739.50    216   212   206 S 202 QA  ZG 0.00  615.00
5.08  615.00
 216   212   206 S 207 QA  ZG 0.00  739.50  5.08  739.50    217   207   202 S 204 QA  ZG 0.00  756.00
5.08  756.00
 217   207   202 S 207 QA  ZG 0.00  739.50  5.08  739.50    217   213   207 S 204 QA  ZG 0.00  756.00
5.08  756.00
 217   213   207 S 207 QA  ZG 0.00  739.50  5.08  739.50    218   208   203 S 200 QA  ZG 0.00  196.00
5.08  196.00
 218   208   203 S 204 QA  ZG 0.00  756.00  5.08  756.00    218   214   208 S 200 QA  ZG 0.00  196.00
5.08  196.00
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5.08  196.00
 219   209   204 S 201 QA  ZG 0.00  196.00  5.08  196.00    219   215   209 S 200 QA  ZG 0.00  196.00
5.08  196.00
 219   215   209 S 201 QA  ZG 0.00  196.00  5.08  196.00    220   210   205 S 201 QA  ZG 0.00  196.00
5.08  196.00
 220   216   210 S 201 QA  ZG 0.00  196.00  5.08  196.00    302 -2518 -2519 S 307 QA2 ZG 0.00   33.06
4.22   33.06
 302 -2519 -2520 S 320 QA2 ZG 0.00   33.06  4.93   33.06    302 -2520 -2521 S 319 QA2 ZG 0.00   33.06
5.04   33.06
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4.90   33.06
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4.22   33.06
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4.93   33.06
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5.04   33.06
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4.90   33.06
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4.90   33.02
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2.63   33.06
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4.22   32.51
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4.93   32.51
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5.04   32.51
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4.90   32.51
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4.90   33.02
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2.63   33.02
 305 -2537 -2538 S 326 QA2 ZG 0.00   32.51  2.63   32.51    306 -2546 -2547 S 305 QA2 ZG 0.00   32.51
4.22   32.51
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4.93   32.51
 306 -2547 -2548 S 311 QA2 ZG 0.00   32.51  4.93   32.51    306 -2548 -2549 S 310 QA2 ZG 0.00   32.51
5.04   32.51
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4.90   32.51
 306 -2549 -2550 S 311 QA2 ZG 0.00   32.51  4.90   32.51    306 -2550 -2551 S 310 QA2 ZG 0.00   32.51
4.90   32.51
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2.63   32.51
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4.22   32.51
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4.93   32.51
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5.04   32.51
 307 -2555 -2556 S 310 QA2 ZG 0.00   32.51  5.04   32.51    307 -2556 -2557 S 309 QA2 ZG 0.00   32.51
4.90   32.51
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4.90   32.51
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2.63   32.51
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4.93   32.51
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5.04   32.51
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4.90   32.51
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4.90   32.51
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2.63   32.51
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4.22   32.51
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4.93   32.51
 309   323   324 S 317 QA2 ZG 0.00   38.46  4.93   38.46    309   324   325 S 308 QA2 ZG 0.00   32.51
5.04   32.51
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4.90   32.51
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4.90   32.51
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2.63   32.51
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4.22   38.14
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4.93   38.14
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4.90   38.14
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4.90   38.14
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2.63   38.14
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4.22   38.40
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4.93   38.14
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5.04   38.14
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4.90   38.14
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4.90   38.14
 311 -2543 -2544 S 315 QA2 ZG 0.00   38.40  4.90   38.40    311 -2544 -2545 S 314 QA2 ZG 0.00   38.14
2.63   38.14
 311 -2544 -2545 S 330 QA2 ZG 0.00   38.40  2.63   38.40    312   317   312 S 302 QA2 ZG 0.00   38.40
4.22   38.40
 312   312   313 S 315 QA2 ZG 0.00   38.40  4.93   38.40    312   313   314 S 315 QA2 ZG 0.00   38.40
5.04   38.40
 312   314   315 S 315 QA2 ZG 0.00   38.40  4.90   38.40    312   315   316 S 315 QA2 ZG 0.00   38.40
4.90   38.40
 312   316   318 S 330 QA2 ZG 0.00   38.40  2.63   38.40    501 -1601 -1600 S 500 QA  ZG 0.00  964.50
2.61  964.50
```

501 -1601 -1600 S 502 QA ZG 0.00 506.00 2.61 506.00 2000 218 201 S 202 QA ZG 0.00 0.00
4.10 7.50

ELENCO CARICHI ASTE

CONDIZIONE DI CARICO 4: NEVE

CARICHI DISTRIBUITI

Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>	Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>
0	-2327	-2348	S	209	QA2	ZG	0.00	252.00	0.34	252.00	0	-2348	-2351	S	209	QA2	ZG	0.00	252.00	0.34	252.00
0	-2351	-2355	S	209	QA2	ZG	0.00	252.00	0.34	252.00	0	-2355	-2358	S	209	QA2	ZG	0.00	252.00	0.34	252.00
0	-2358	-2364	S	209	QA2	ZG	0.00	252.00	0.34	252.00	0	-2364	-2367	S	209	QA2	ZG	0.00	252.00	0.34	252.00
0	-2367	-2373	S	209	QA2	ZG	0.00	252.00	0.34	252.00	0	-2373	-2374	S	209	QA2	ZG	0.00	252.00	0.34	252.00
0	-2352	-2328	S	209	QA2	ZG	0.00	252.00	0.68	252.00	0	-2359	-2352	S	209	QA2	ZG	0.00	252.00	0.68	252.00
0	-2368	-2359	S	209	QA2	ZG	0.00	252.00	0.68	252.00	0	-2353	-2330	S	208	QA2	ZG	0.00	265.20	0.68	265.20
0	-2375	-2368	S	209	QA2	ZG	0.00	252.00	0.68	252.00	0	-2360	-2353	S	208	QA2	ZG	0.00	265.20	0.68	265.20
0	-2369	-2360	S	208	QA2	ZG	0.00	265.20	0.68	265.20	0	-2377	-2369	S	208	QA2	ZG	0.00	265.20	0.68	265.20
0	-2331	-2354	S	208	QA2	ZG	0.00	265.20	0.68	265.20	0	-2354	-2361	S	208	QA2	ZG	0.00	265.20	0.68	265.20
0	-2361	-2370	S	208	QA2	ZG	0.00	265.20	0.68	265.20	0	-2370	218	S	208	QA2	ZG	0.00	265.20	0.68	265.20
0	-1536	-1537	S	500	QA2	ZG	0.00	257.20	0.48	257.20	0	-1537	-1538	S	500	QA2	ZG	0.00	257.20	0.48	257.20
0	-1538	-1539	S	500	QA2	ZG	0.00	257.20	0.48	257.20	0	-1539	-1540	S	500	QA2	ZG	0.00	257.20	0.48	257.20
0	-1540	-1541	S	500	QA2	ZG	0.00	257.20	0.48	257.20	0	-1541	-1542	S	500	QA2	ZG	0.00	257.20	0.48	257.20
0	-1542	-1543	S	500	QA2	ZG	0.00	257.20	0.48	257.20	0	-1543	-1544	S	500	QA2	ZG	0.00	257.20	0.48	257.20
0	-1544	-1545	S	500	QA2	ZG	0.00	257.20	0.48	257.20	0	-1545	-1546	S	500	QA2	ZG	0.00	257.20	0.48	257.20
0	-1546	-1547	S	500	QA2	ZG	0.00	257.20	0.48	257.20	0	-1547	-1548	S	500	QA2	ZG	0.00	257.20	0.48	257.20
0	-1548	-1549	S	500	QA2	ZG	0.00	257.20	0.48	257.20	0	-1549	-1550	S	500	QA2	ZG	0.00	257.20	0.48	257.20
0	-1593	-1592	S	500	QA2	ZG	0.00	257.20	0.43	257.20	0	-1550	-1551	S	500	QA2	ZG	0.00	257.20	0.48	257.20
0	-1594	-1593	S	500	QA2	ZG	0.00	257.20	0.43	257.20	0	-1551	-1552	S	500	QA2	ZG	0.00	257.20	0.48	257.20
0	-1595	-1594	S	500	QA2	ZG	0.00	257.20	0.43	257.20	0	-1596	-1595	S	500	QA2	ZG	0.00	257.20	0.43	257.20
0	-1597	-1596	S	500	QA2	ZG	0.00	257.20	0.43	257.20	0	-1553	-1554	S	500	QA2	ZG	0.00	257.20	0.48	257.20
0	-1598	-1597	S	500	QA2	ZG	0.00	257.20	0.43	257.20	0	-1599	-1598	S	500	QA2	ZG	0.00	257.20	0.43	257.20
0	-1601	-2580	S	500	QA2	ZG	0.00	257.20	0.32	257.20	0	-1552	-1553	S	500	QA2	ZG	0.00	257.20	0.48	257.20
0	-1600	-1599	S	500	QA2	ZG	0.00	257.20	0.43	257.20	0	-1554	-1555	S	500	QA2	ZG	0.00	257.20	0.48	257.20
0	-1555	-1556	S	500	QA2	ZG	0.00	257.20	0.48	257.20	0	-1556	-1557	S	500	QA2	ZG	0.00	257.20	0.48	257.20
0	-1557	-1558	S	500	QA2	ZG	0.00	257.20	0.48	257.20	0	-1558	-1559	S	500	QA2	ZG	0.00	257.20	0.48	257.20
0	-1560	-1561	S	500	QA2	ZG	0.00	257.20	0.48	257.20	0	-2580	-1602	S	500	QA2	ZG	0.00	257.20	0.32	257.20
0	-1602	-1603	S	500	QA2	ZG	0.00	257.20	0.49	257.20	0	-1603	-1604	S	500	QA2	ZG	0.00	257.20	0.49	257.20
0	-1604	-1605	S	500	QA2	ZG	0.00	257.20	0.49	257.20	0	-1605	-1606	S	500	QA2	ZG	0.00	257.20	0.49	257.20

```
   0 -1606 -1607 S 500 QA2 ZG 0.00  257.20 0.49  257.20      0 -1607 -1608 S 500 QA2 ZG 0.00  257.20
0.49  257.20
   0 -1561 -1562 S 500 QA2 ZG 0.00  257.20 0.48  257.20      0 -1559 -1560 S 500 QA2 ZG 0.00  257.20
0.48  257.20
   0 -1608 -1609 S 500 QA2 ZG 0.00  257.20 0.49  257.20      0 -1610 -1611 S 500 QA2 ZG 0.00  257.20
0.49  257.20
   0 -1609 -1610 S 500 QA2 ZG 0.00  257.20 0.49  257.20      0 -1611 -1615 S 501 QA2 ZG 0.00   60.00
0.42   60.00
   0 -1615 -1623 S 501 QA2 ZG 0.00   60.00 0.42   60.00      0 -1611 -1612 S 500 QA2 ZG 0.00  257.20
1.50  257.20
   0 -1623 -1630 S 501 QA2 ZG 0.00   60.00 0.42   60.00      0 -1616 -1612 S 501 QA2 ZG 0.00   60.00
0.42   60.00
   0 -1630 -1634 S 501 QA2 ZG 0.00   60.00 0.42   60.00      0 -1634 -1641 S 501 QA2 ZG 0.00   60.00
0.42   60.00
   0 -1641 -1671 S 501 QA2 ZG 0.00   60.00 0.42   60.00      0 -1624 -1616 S 501 QA2 ZG 0.00   60.00
0.42   60.00
   0 -1631 -1624 S 501 QA2 ZG 0.00   60.00 0.42   60.00      0 -1635 -1631 S 501 QA2 ZG 0.00   60.00
0.42   60.00
   0 -1674 -1642 S 501 QA2 ZG 0.00   60.00 0.42   60.00      0 -1642 -1635 S 501 QA2 ZG 0.00   60.00
0.42   60.00
 218   208   203 S 200 QA2 ZG 0.00  122.50 5.08  122.50    218   214   208 S 200 QA2 ZG 0.00  122.50
5.08  122.50
 219   209   204 S 200 QA2 ZG 0.00  122.50 5.08  122.50    219   209   204 S 201 QA2 ZG 0.00  122.50
5.08  122.50
 219   215   209 S 200 QA2 ZG 0.00  122.50 5.08  122.50    219   215   209 S 201 QA2 ZG 0.00  122.50
5.08  122.50
 220   210   205 S 201 QA2 ZG 0.00  122.50 5.08  122.50    220   216   210 S 201 QA2 ZG 0.00  122.50
5.08  122.50
 302 -2518 -2519 S 307 QA  ZG 0.00   52.89 4.22   52.89    302 -2519 -2520 S 320 QA  ZG 0.00   52.89
4.93   52.89
 302 -2520 -2521 S 319 QA  ZG 0.00   52.89 5.04   52.89    302 -2521 -2522 S 318 QA  ZG 0.00   52.89
4.90   52.89
 302 -2522 -2523 S 313 QA  ZG 0.00   52.89 4.90   52.89    302 -2523 -2524 S 324 QA  ZG 0.00   52.89
2.63   52.89
 303 -2525 -2526 S 307 QA  ZG 0.00   52.89 4.22   52.89    303 -2525 -2526 S 312 QA  ZG 0.00   52.83
4.22   52.83
 303 -2526 -2527 S 320 QA  ZG 0.00   52.89 4.93   52.89    303 -2526 -2527 S 323 QA  ZG 0.00   52.83
4.93   52.83
 303 -2527 -2528 S 319 QA  ZG 0.00   52.89 5.04   52.89    303 -2527 -2528 S 322 QA  ZG 0.00   52.83
5.04   52.83
 303 -2528 -2529 S 318 QA  ZG 0.00   52.89 4.90   52.89    303 -2528 -2529 S 321 QA  ZG 0.00   52.83
4.90   52.83
 303 -2529 -2530 S 304 QA  ZG 0.00   52.83 4.90   52.83    303 -2529 -2530 S 313 QA  ZG 0.00   52.89
4.90   52.89
 303 -2530 -2531 S 324 QA  ZG 0.00   52.89 2.63   52.89    303 -2530 -2531 S 325 QA  ZG 0.00   52.83
2.63   52.83
 305 -2532 -2533 S 306 QA  ZG 0.00   52.01 4.22   52.01    305 -2532 -2533 S 312 QA  ZG 0.00   52.83
4.22   52.83
 305 -2533 -2534 S 311 QA  ZG 0.00   52.01 4.93   52.01    305 -2533 -2534 S 323 QA  ZG 0.00   52.83
4.93   52.83
 305 -2534 -2535 S 311 QA  ZG 0.00   52.01 5.04   52.01    305 -2534 -2535 S 322 QA  ZG 0.00   52.83
5.04   52.83
 305 -2535 -2536 S 311 QA  ZG 0.00   52.01 4.90   52.01    305 -2535 -2536 S 321 QA  ZG 0.00   52.83
4.90   52.83
 305 -2536 -2537 S 304 QA  ZG 0.00   52.83 4.90   52.83    305 -2536 -2537 S 311 QA  ZG 0.00   52.01
4.90   52.01
 305 -2537 -2538 S 325 QA  ZG 0.00   52.83 2.63   52.83    305 -2537 -2538 S 326 QA  ZG 0.00   52.01
2.63   52.01
 306 -2546 -2547 S 305 QA  ZG 0.00   52.01 4.22   52.01    306 -2546 -2547 S 306 QA  ZG 0.00   52.01
4.22   52.01
 306 -2547 -2548 S 310 QA  ZG 0.00   52.01 4.93   52.01    306 -2547 -2548 S 311 QA  ZG 0.00   52.01
4.93   52.01
 306 -2548 -2549 S 310 QA  ZG 0.00   52.01 5.04   52.01    306 -2548 -2549 S 311 QA  ZG 0.00   52.01
5.04   52.01
 306 -2549 -2550 S 310 QA  ZG 0.00   52.01 4.90   52.01    306 -2549 -2550 S 311 QA  ZG 0.00   52.01
4.90   52.01
 306 -2550 -2551 S 310 QA  ZG 0.00   52.01 4.90   52.01    306 -2550 -2551 S 311 QA  ZG 0.00   52.01
4.90   52.01
 306 -2551 -2552 S 326 QA  ZG 0.00   52.01 2.63   52.01    306 -2551 -2552 S 327 QA  ZG 0.00   52.01
2.63   52.01
 307 -2553 -2554 S 300 QA  ZG 0.00   52.01 4.22   52.01    307 -2553 -2554 S 305 QA  ZG 0.00   52.01
4.22   52.01
 307 -2554 -2555 S 309 QA  ZG 0.00   52.01 4.93   52.01    307 -2554 -2555 S 310 QA  ZG 0.00   52.01
```

4.93 52.01
307 -2555 -2556 S 309 QA ZG 0.00 52.01 5.04 52.01 307 -2555 -2556 S 310 QA ZG 0.00 52.01
5.04 52.01
307 -2556 -2557 S 309 QA ZG 0.00 52.01 4.90 52.01 307 -2556 -2557 S 310 QA ZG 0.00 52.01
4.90 52.01
307 -2557 -2558 S 309 QA ZG 0.00 52.01 4.90 52.01 307 -2557 -2558 S 310 QA ZG 0.00 52.01
4.90 52.01
307 -2558 -2559 S 327 QA ZG 0.00 52.01 2.63 52.01 307 -2558 -2559 S 328 QA ZG 0.00 52.01
2.63 52.01
308 -2567 -2568 S 300 QA ZG 0.00 52.01 4.22 52.01 308 -2567 -2568 S 303 QA ZG 0.00 52.01
4.22 52.01
308 -2568 -2569 S 308 QA ZG 0.00 52.01 4.93 52.01 308 -2568 -2569 S 309 QA ZG 0.00 52.01
4.93 52.01
308 -2569 -2570 S 308 QA ZG 0.00 52.01 5.04 52.01 308 -2569 -2570 S 309 QA ZG 0.00 52.01
5.04 52.01
308 -2570 -2571 S 308 QA ZG 0.00 52.01 4.90 52.01 308 -2570 -2571 S 309 QA ZG 0.00 52.01
4.90 52.01
308 -2571 -2572 S 308 QA ZG 0.00 52.01 4.90 52.01 308 -2571 -2572 S 309 QA ZG 0.00 52.01
4.90 52.01
308 -2572 -2573 S 328 QA ZG 0.00 52.01 2.63 52.01 308 -2572 -2573 S 329 QA ZG 0.00 52.01
2.63 52.01
309 322 323 S 303 QA ZG 0.00 52.01 4.22 52.01 309 322 323 S 331 QA ZG 0.00 15.38
4.22 15.38
309 323 324 S 308 QA ZG 0.00 52.01 4.93 52.01 309 323 324 S 317 QA ZG 0.00 15.38
4.93 15.38
309 324 325 S 308 QA ZG 0.00 52.01 5.04 52.01 309 324 325 S 317 QA ZG 0.00 15.38
5.04 15.38
309 325 326 S 308 QA ZG 0.00 52.01 4.90 52.01 309 325 326 S 317 QA ZG 0.00 15.38
4.90 15.38
309 326 327 S 308 QA ZG 0.00 52.01 4.90 52.01 309 326 327 S 317 QA ZG 0.00 15.38
4.90 15.38
309 327 328 S 329 QA ZG 0.00 52.01 2.63 52.01 309 327 328 S 332 QA ZG 0.00 15.38
2.63 15.38
310 -2560 -2561 S 316 QA ZG 0.00 15.26 4.22 15.26 310 -2560 -2561 S 331 QA ZG 0.00 15.38
4.22 15.38
310 -2561 -2562 S 301 QA ZG 0.00 15.26 4.93 15.26 310 -2561 -2562 S 317 QA ZG 0.00 15.38
4.93 15.38
310 -2562 -2563 S 301 QA ZG 0.00 15.26 5.04 15.26 310 -2562 -2563 S 317 QA ZG 0.00 15.38
5.04 15.38
310 -2563 -2564 S 301 QA ZG 0.00 15.26 4.90 15.26 310 -2563 -2564 S 317 QA ZG 0.00 15.38
4.90 15.38
310 -2564 -2565 S 301 QA ZG 0.00 15.26 4.90 15.26 310 -2564 -2565 S 317 QA ZG 0.00 15.38
4.90 15.38
310 -2565 -2566 S 314 QA ZG 0.00 15.26 2.63 15.26 310 -2565 -2566 S 332 QA ZG 0.00 15.38
2.63 15.38
311 -2539 -2540 S 302 QA ZG 0.00 15.36 4.22 15.36 311 -2539 -2540 S 316 QA ZG 0.00 15.26
4.22 15.26
311 -2540 -2541 S 301 QA ZG 0.00 15.26 4.93 15.26 311 -2540 -2541 S 315 QA ZG 0.00 15.36
4.93 15.36
311 -2541 -2542 S 301 QA ZG 0.00 15.26 5.04 15.26 311 -2541 -2542 S 315 QA ZG 0.00 15.36
5.04 15.36
311 -2542 -2543 S 301 QA ZG 0.00 15.26 4.90 15.26 311 -2542 -2543 S 315 QA ZG 0.00 15.36
4.90 15.36
311 -2543 -2544 S 301 QA ZG 0.00 15.26 4.90 15.26 311 -2543 -2544 S 315 QA ZG 0.00 15.36
4.90 15.36
311 -2544 -2545 S 314 QA ZG 0.00 15.26 2.63 15.26 311 -2544 -2545 S 330 QA ZG 0.00 15.36
2.63 15.36
312 317 312 S 302 QA ZG 0.00 15.36 4.22 15.36 312 312 313 S 315 QA ZG 0.00 15.36
4.93 15.36
312 313 314 S 315 QA ZG 0.00 15.36 5.04 15.36 312 314 315 S 315 QA ZG 0.00 15.36
4.90 15.36
312 315 316 S 315 QA ZG 0.00 15.36 4.90 15.36 312 316 318 S 330 QA ZG 0.00 15.36
2.63 15.36
501 -1601 -1600 S 500 QA2 ZG 0.00 257.20 2.61 257.20

ELENCO CARICHI ASTE

CONDIZIONE DI CARICO 5: VENTO

CARICHI DISTRIBUITI

Asta N1 N2 E NE T DC Xi Qi Xf Qf Asta N1 N2 E NE T DC Xi Qi
Xf Qf

```
                                  <m> <daN/m>  <m> <daN/m>                                  <m> <daN/m>
<m> <daN/m>
-------------------------------------------------------   ------------------------------------------
----------
 302 -2518 -2519 S --  M   ZL 0.00  102.00 4.22  102.00    302 -2518 -2519 S 307 QA3 ZG 0.00   39.67
4.22   39.67
 302 -2519 -2520 S --  M   ZL 0.00  102.00 4.93  102.00    302 -2519 -2520 S 320 QA3 ZG 0.00   39.67
4.93   39.67
 302 -2520 -2521 S --  M   ZL 0.00  102.00 5.04  102.00    302 -2520 -2521 S 319 QA3 ZG 0.00   39.67
5.04   39.67
 302 -2521 -2522 S --  M   ZL 0.00  102.00 4.90  102.00    302 -2521 -2522 S 318 QA3 ZG 0.00   39.67
4.90   39.67
 302 -2522 -2523 S --  M   ZL 0.00  102.00 4.90  102.00    302 -2522 -2523 S 313 QA3 ZG 0.00   39.67
4.90   39.67
 302 -2523 -2524 S --  M   ZL 0.00  102.00 2.63  102.00    302 -2523 -2524 S 324 QA3 ZG 0.00   39.67
2.63   39.67
 303 -2525 -2526 S --  M   ZL 0.00  102.00 4.22  102.00    303 -2525 -2526 S 307 QA3 ZG 0.00   39.67
4.22   39.67
 303 -2525 -2526 S 312 QA3 ZG 0.00   39.62 4.22   39.62    303 -2526 -2527 S --  M   ZL 0.00  102.00
4.93  102.00
 303 -2526 -2527 S 320 QA3 ZG 0.00   39.67 4.93   39.67    303 -2526 -2527 S 323 QA3 ZG 0.00   39.62
4.93   39.62
 303 -2527 -2528 S --  M   ZL 0.00  102.00 5.04  102.00    303 -2527 -2528 S 319 QA3 ZG 0.00   39.67
5.04   39.67
 303 -2527 -2528 S 322 QA3 ZG 0.00   39.62 5.04   39.62    303 -2528 -2529 S --  M   ZL 0.00  102.00
4.90  102.00
 303 -2528 -2529 S 318 QA3 ZG 0.00   39.67 4.90   39.67    303 -2528 -2529 S 321 QA3 ZG 0.00   39.62
4.90   39.62
 303 -2529 -2530 S --  M   ZL 0.00  102.00 4.90  102.00    303 -2529 -2530 S 304 QA3 ZG 0.00   39.62
4.90   39.62
 303 -2529 -2530 S 313 QA3 ZG 0.00   39.67 4.90   39.67    303 -2530 -2531 S --  M   ZL 0.00  102.00
2.63  102.00
 303 -2530 -2531 S 324 QA3 ZG 0.00   39.67 2.63   39.67    303 -2530 -2531 S 325 QA3 ZG 0.00   39.62
2.63   39.62
 305 -2532 -2533 S --  M   ZL 0.00  102.00 4.22  102.00    305 -2532 -2533 S 306 QA3 ZG 0.00   39.01
4.22   39.01
 305 -2532 -2533 S 312 QA3 ZG 0.00   39.62 4.22   39.62    305 -2533 -2534 S --  M   ZL 0.00  102.00
4.93  102.00
 305 -2533 -2534 S 311 QA3 ZG 0.00   39.01 4.93   39.01    305 -2533 -2534 S 323 QA3 ZG 0.00   39.62
4.93   39.62
 305 -2534 -2535 S --  M   ZL 0.00  102.00 5.04  102.00    305 -2534 -2535 S 311 QA3 ZG 0.00   39.01
5.04   39.01
 305 -2534 -2535 S 322 QA3 ZG 0.00   39.62 5.04   39.62    305 -2535 -2536 S --  M   ZL 0.00  102.00
4.90  102.00
 305 -2535 -2536 S 311 QA3 ZG 0.00   39.01 4.90   39.01    305 -2535 -2536 S 321 QA3 ZG 0.00   39.62
4.90   39.62
 305 -2536 -2537 S --  M   ZL 0.00  102.00 4.90  102.00    305 -2536 -2537 S 304 QA3 ZG 0.00   39.62
4.90   39.62
 305 -2536 -2537 S 311 QA3 ZG 0.00   39.01 4.90   39.01    305 -2537 -2538 S --  M   ZL 0.00  102.00
2.63  102.00
 305 -2537 -2538 S 325 QA3 ZG 0.00   39.62 2.63   39.62    305 -2537 -2538 S 326 QA3 ZG 0.00   39.01
2.63   39.01
 306 -2546 -2547 S --  M   ZL 0.00  102.00 4.22  102.00    306 -2546 -2547 S 305 QA3 ZG 0.00   39.01
4.22   39.01
 306 -2546 -2547 S 306 QA3 ZG 0.00   39.01 4.22   39.01    306 -2547 -2548 S --  M   ZL 0.00  102.00
4.93  102.00
 306 -2547 -2548 S 310 QA3 ZG 0.00   39.01 4.93   39.01    306 -2547 -2548 S 311 QA3 ZG 0.00   39.01
4.93   39.01
 306 -2548 -2549 S --  M   ZL 0.00  102.00 5.04  102.00    306 -2548 -2549 S 310 QA3 ZG 0.00   39.01
5.04   39.01
 306 -2548 -2549 S 311 QA3 ZG 0.00   39.01 5.04   39.01    306 -2549 -2550 S --  M   ZL 0.00  102.00
4.90  102.00
 306 -2549 -2550 S 310 QA3 ZG 0.00   39.01 4.90   39.01    306 -2549 -2550 S 311 QA3 ZG 0.00   39.01
4.90   39.01
 306 -2550 -2551 S --  M   ZL 0.00  102.00 4.90  102.00    306 -2550 -2551 S 310 QA3 ZG 0.00   39.01
4.90   39.01
 306 -2550 -2551 S 311 QA3 ZG 0.00   39.01 4.90   39.01    306 -2551 -2552 S --  M   ZL 0.00  102.00
2.63  102.00
 306 -2551 -2552 S 326 QA3 ZG 0.00   39.01 2.63   39.01    306 -2551 -2552 S 327 QA3 ZG 0.00   39.01
2.63   39.01
 307 -2553 -2554 S --  M   ZL 0.00  102.00 4.22  102.00    307 -2553 -2554 S 300 QA3 ZG 0.00   39.01
4.22   39.01
 307 -2553 -2554 S 305 QA3 ZG 0.00   39.01 4.22   39.01    307 -2554 -2555 S --  M   ZL 0.00  102.00
```

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4.93  102.00
 307 -2554 -2555 S 309 QA3 ZG 0.00   39.01 4.93   39.01    307 -2554 -2555 S 310 QA3 ZG 0.00   39.01
4.93   39.01
 307 -2555 -2556 S --  M   ZL 0.00  102.00 5.04  102.00    307 -2555 -2556 S 309 QA3 ZG 0.00   39.01
5.04   39.01
 307 -2555 -2556 S 310 QA3 ZG 0.00   39.01 5.04   39.01    307 -2556 -2557 S --  M   ZL 0.00  102.00
4.90  102.00
 307 -2556 -2557 S 309 QA3 ZG 0.00   39.01 4.90   39.01    307 -2556 -2557 S 310 QA3 ZG 0.00   39.01
4.90   39.01
 307 -2557 -2558 S --  M   ZL 0.00  102.00 4.90  102.00    307 -2557 -2558 S 309 QA3 ZG 0.00   39.01
4.90   39.01
 307 -2557 -2558 S 310 QA3 ZG 0.00   39.01 4.90   39.01    307 -2558 -2559 S --  M   ZL 0.00  102.00
2.63  102.00
 307 -2558 -2559 S 327 QA3 ZG 0.00   39.01 2.63   39.01    307 -2558 -2559 S 328 QA3 ZG 0.00   39.01
2.63   39.01
 308 -2567 -2568 S --  M   ZL 0.00  102.00 4.22  102.00    308 -2567 -2568 S 300 QA3 ZG 0.00   39.01
4.22   39.01
 308 -2567 -2568 S 303 QA3 ZG 0.00   39.01 4.22   39.01    308 -2568 -2569 S --  M   ZL 0.00  102.00
4.93  102.00
 308 -2568 -2569 S 308 QA3 ZG 0.00   39.01 4.93   39.01    308 -2568 -2569 S 309 QA3 ZG 0.00   39.01
4.93   39.01
 308 -2569 -2570 S --  M   ZL 0.00  102.00 5.04  102.00    308 -2569 -2570 S 308 QA3 ZG 0.00   39.01
5.04   39.01
 308 -2569 -2570 S 309 QA3 ZG 0.00   39.01 5.04   39.01    308 -2570 -2571 S --  M   ZL 0.00  102.00
4.90  102.00
 308 -2570 -2571 S 308 QA3 ZG 0.00   39.01 4.90   39.01    308 -2570 -2571 S 309 QA3 ZG 0.00   39.01
4.90   39.01
 308 -2571 -2572 S --  M   ZL 0.00  102.00 4.90  102.00    308 -2571 -2572 S 308 QA3 ZG 0.00   39.01
4.90   39.01
 308 -2571 -2572 S 309 QA3 ZG 0.00   39.01 4.90   39.01    308 -2572 -2573 S --  M   ZL 0.00  102.00
2.63  102.00
 308 -2572 -2573 S 328 QA3 ZG 0.00   39.01 2.63   39.01    308 -2572 -2573 S 329 QA3 ZG 0.00   39.01
2.63   39.01
 309   322   323 S --  M   ZL 0.00 -290.00 4.22 -290.00    309   322   323 S 303 QA3 ZG 0.00   39.01
4.22   39.01
 309   322   323 S 331 QA3 ZG 0.00   61.53 4.22   61.53    309   323   324 S --  M   ZL 0.00 -290.00
4.93 -290.00
 309   323   324 S 308 QA3 ZG 0.00   39.01 4.93   39.01    309   323   324 S 317 QA3 ZG 0.00   61.53
4.93   61.53
 309   324   325 S --  M   ZL 0.00 -290.00 5.04 -290.00    309   324   325 S 308 QA3 ZG 0.00   39.01
5.04   39.01
 309   324   325 S 317 QA3 ZG 0.00   61.53 5.04   61.53    309   325   326 S --  M   ZL 0.00 -290.00
4.90 -290.00
 309   325   326 S 308 QA3 ZG 0.00   39.01 4.90   39.01    309   325   326 S 317 QA3 ZG 0.00   61.53
4.90   61.53
 309   326   327 S --  M   ZL 0.00 -290.00 4.90 -290.00    309   326   327 S 308 QA3 ZG 0.00   39.01
4.90   39.01
 309   326   327 S 317 QA3 ZG 0.00   61.53 4.90   61.53    309   327   328 S --  M   ZL 0.00 -290.00
2.63 -290.00
 309   327   328 S 329 QA3 ZG 0.00   39.01 2.63   39.01    309   327   328 S 332 QA3 ZG 0.00   61.53
2.63   61.53
 310 -2560 -2561 S --  M   ZL 0.00 -290.00 4.22 -290.00    310 -2560 -2561 S 316 QA3 ZG 0.00   61.02
4.22   61.02
 310 -2560 -2561 S 331 QA3 ZG 0.00   61.53 4.22   61.53    310 -2561 -2562 S --  M   ZL 0.00 -290.00
4.93 -290.00
 310 -2561 -2562 S 301 QA3 ZG 0.00   61.02 4.93   61.02    310 -2561 -2562 S 317 QA3 ZG 0.00   61.53
4.93   61.53
 310 -2562 -2563 S --  M   ZL 0.00 -290.00 5.04 -290.00    310 -2562 -2563 S 301 QA3 ZG 0.00   61.02
5.04   61.02
 310 -2562 -2563 S 317 QA3 ZG 0.00   61.53 5.04   61.53    310 -2563 -2564 S --  M   ZL 0.00 -290.00
4.90 -290.00
 310 -2563 -2564 S 301 QA3 ZG 0.00   61.02 4.90   61.02    310 -2563 -2564 S 317 QA3 ZG 0.00   61.53
4.90   61.53
 310 -2564 -2565 S --  M   ZL 0.00 -290.00 4.90 -290.00    310 -2564 -2565 S 301 QA3 ZG 0.00   61.02
4.90   61.02
 310 -2564 -2565 S 317 QA3 ZG 0.00   61.53 4.90   61.53    310 -2565 -2566 S --  M   ZL 0.00 -290.00
2.63 -290.00
 310 -2565 -2566 S 314 QA3 ZG 0.00   61.02 2.63   61.02    310 -2565 -2566 S 332 QA3 ZG 0.00   61.53
2.63   61.53
 311 -2539 -2540 S --  M   ZL 0.00 -290.00 4.22 -290.00    311 -2539 -2540 S 302 QA3 ZG 0.00   61.44
4.22   61.44
 311 -2539 -2540 S 316 QA3 ZG 0.00   61.02 4.22   61.02    311 -2540 -2541 S --  M   ZL 0.00 -290.00
4.93 -290.00
```

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 311 -2540 -2541 S 301 QA3 ZG 0.00   61.02 4.93   61.02    311 -2540 -2541 S 315 QA3 ZG 0.00   61.44
4.93   61.44
 311 -2541 -2542 S --  M   ZL 0.00 -290.00 5.04 -290.00    311 -2541 -2542 S 301 QA3 ZG 0.00   61.02
5.04   61.02
 311 -2541 -2542 S 315 QA3 ZG 0.00   61.44 5.04   61.44    311 -2542 -2543 S --  M   ZL 0.00 -290.00
4.90 -290.00
 311 -2542 -2543 S 301 QA3 ZG 0.00   61.02 4.90   61.02    311 -2542 -2543 S 315 QA3 ZG 0.00   61.44
4.90   61.44
 311 -2543 -2544 S --  M   ZL 0.00 -290.00 4.90 -290.00    311 -2543 -2544 S 301 QA3 ZG 0.00   61.02
4.90   61.02
 311 -2543 -2544 S 315 QA3 ZG 0.00   61.44 4.90   61.44    311 -2544 -2545 S --  M   ZL 0.00 -290.00
2.63 -290.00
 311 -2544 -2545 S 314 QA3 ZG 0.00   61.02 2.63   61.02    311 -2544 -2545 S 330 QA3 ZG 0.00   61.44
2.63   61.44
 312   317   312 S --  M   ZL 0.00 -290.00 4.22 -290.00    312   317   312 S 302 QA3 ZG 0.00   61.44
4.22   61.44
 312   312   313 S --  M   ZL 0.00 -290.00 4.93 -290.00    312   312   313 S 315 QA3 ZG 0.00   61.44
4.93   61.44
 312   313   314 S --  M   ZL 0.00 -290.00 5.04 -290.00    312   313   314 S 315 QA3 ZG 0.00   61.44
5.04   61.44
 312   314   315 S --  M   ZL 0.00 -290.00 4.90 -290.00    312   314   315 S 315 QA3 ZG 0.00   61.44
4.90   61.44
 312   315   316 S --  M   ZL 0.00 -290.00 4.90 -290.00    312   315   316 S 315 QA3 ZG 0.00   61.44
4.90   61.44
 312   316   318 S --  M   ZL 0.00 -290.00 2.63 -290.00    312   316   318 S 330 QA3 ZG 0.00   61.44
2.63   61.44
```

ELENCO PESO PROPRIO BIDIMENSIONALI

Simbologia

Tb = Numero del tipo muro/elemento bidimensionale
Comm. = Commento
Spess. = Spessore
Mat. = Materiale
P = Peso specifico
PQ = Peso specifico per unità di superficie

Tb	Comm.	Spess. <cm>	Mat.	P <daN/mc>	PQ <daN/mq>
2	SETTO 40	40.00	Calcestruzzo	2500.00	1000.00
4	SETTO 30	30.00	Calcestruzzo	2500.00	750.00
5	fondazione scantinato 25	25.00	Calcestruzzo	2500.00	625.00
6	SETTO 20	20.00	Calcestruzzo	2500.00	500.00

Analisi dei carichi da vento

VENTO LATO MLCalcolo delle azioni del vento

Normativa di riferimento:
Norme tecniche per le costruzioni D.M. 14 gennaio 2008 e Circolare 2 febbraio 2009, n. 617 del Ministero delle Infrastrutture e dei Trasporti

Area di ubicazione dell'edificio: Area 3
Toscana, Marche, Umbria, Lazio, Abruzzo, Molise, Puglia, Campania, Basilicata, Calabria(esclusa la Provincia di Reggio Calabria)

Tempo di ritorno 50 <anni>

Altitudine sul livello del mare: 60 <m>

Altezza dell'edificio: 18 <m>

Parametri derivati dall'area di ubicazione (tab. 3.3.I):
Vb,0 (Velocità media del vento): 27 <m/sec>
a0 (Altitudine media): 500 <m>
Ka: 0.020 <1/sec>

Velocità di riferimento: 27.00 <m/sec>

Classificazione della costruzione: Pianta rettangolare con coperture piane, a falde, inclinate o curve

Categoria di esposizione del sito: IV

Parametri derivati dalla categoria di esposizione del sito (tab. 3.3.II):
kr: 0.22 <m>
z0: 0.30 <m>
zmin: 8 <m>

Classe di rugosità del terreno: A
 Aree urbane in cui almeno il 15% della superficie sia coperto
 da edifici la cui altezza media superi i 15 m

Angolo alfa: 53.0 <grad>

Pressione del vento = qb*ce*cp*cd
qb (Pressione cinetica di riferimento): 45.56 <daN/mq>
ct (Coefficiente topografico): 1.00
ce (Coefficiente di esposizione): 2.20
cd (Coefficiente dinamico): 1.00

Tipologia di superficie:
 Una parete con aperture di superficie minore di 1/3 di quella totale

Coefficiente di forma o aerodinamico interno cpi: 0.20
Coefficienti di forma o aerodinamici esterni cpe:
sopravento: 0.80 sopravento su falda: 0.59 sottovento su falda: -0.40 sottovento: -0.40

Pressione interna: 20.03 <daN/mq>
Pressioni esterne:
sopravento: 80.14 <daN/mq> sopravento su falda: 59.10 <daN/mq> sottovento su falda: -40.07 <daN/mq>
sottovento: -40.07 <daN/mq>

VENTOCalcolo delle azioni del vento

Normativa di riferimento:
 Norme tecniche per le costruzioni D.M. 14 gennaio 2008 e Circolare 2 febbraio
 2009, n. 617 del Ministero delle Infrastrutture e dei Trasporti

Area di ubicazione dell'edificio: Area 3
 Toscana, Marche, Umbria, Lazio, Abruzzo, Molise, Puglia, Campania, Basilicata, Calabria(esclusa la Provincia di Reggio Calabria)

Tempo di ritorno 50 <anni>

Altitudine sul livello del mare: 60 <m>

Altezza dell'edificio: 18 <m>

Parametri derivati dall'area di ubicazione (tab. 3.3.I):
Vb,0 (Velocità media del vento): 27 <m/sec>
a0 (Altitudine media): 500 <m>
Ka: 0.020 <1/sec>

Velocità di riferimento: 27.00 <m/sec>

Classificazione della costruzione: Pianta rettangolare con coperture piane, a falde, inclinate o curve

Categoria di esposizione del sito: IV

Parametri derivati dalla categoria di esposizione del sito (tab. 3.3.II):
kr: 0.22 <m>
z0: 0.30 <m>
zmin: 8 <m>

Classe di rugosità del terreno: A
 Aree urbane in cui almeno il 15% della superficie sia coperto
 da edifici la cui altezza media superi i 15 m

Angolo alfa: 24.0 <grad>

Pressione del vento = qb*ce*cp*cd
qb (Pressione cinetica di riferimento): 45.56 <daN/mq>
ct (Coefficiente topografico): 1.00
ce (Coefficiente di esposizione): 2.20
cd (Coefficiente dinamico): 1.00

Tipologia di superficie:
Una parete con aperture di superficie minore di 1/3 di quella totale

Coefficiente di forma o aerodinamico interno cpi: 0.20
Coefficienti di forma o aerodinamici esterni cpe:
sopravento: 0.80 sopravento su falda: -0.28 sottovento su falda: -0.40 sottovento: -0.40

Pressione interna: 20.03 <daN/mq>
Pressioni esterne:
sopravento: 80.14 <daN/mq> sopravento su falda: -28.05 <daN/mq> sottovento su falda: -40.07 <daN/mq>
sottovento: -40.07 <daN/mq>

PRATOCalcolo delle azioni del vento

Normativa di riferimento:
Norme tecniche per le costruzioni D.M. 14 gennaio 2008 e Circolare 2 febbraio
2009, n. 617 del Ministero delle Infrastrutture e dei Trasporti

Area di ubicazione dell'edificio: 3
Toscana, Marche, Umbria, Lazio, Abruzzo, Molise, Puglia, Campania, Basilicata, Calabria (esclusa la Provincia di Reggio Calabria)

Tempo di ritorno 50 <anni>

Altitudine sul livello del mare: 60 <m>

Parametri derivati dall'area di ubicazione (tab. 3.3.I):
Vb,0 (Velocità media del vento): 27 <m/sec>
a0 (Altitudine media): 500 <m>
Ka: 0.020 <1/sec>

Velocità di riferimento: 27.00 <m/sec>

Classificazione della costruzione: Pianta rettangolare con coperture piane, a falde, inclinate o curve

Categoria di esposizione del sito: V

Parametri derivati dalla categoria di esposizione del sito (tab. 3.3.II):
kr: 0.23 <m>
z0: 0.70 <m>
zmin: 12 <m>

Classe di rugosità del terreno: A
Aree urbane in cui almeno il 15% della superficie sia coperto
da edifici la cui altezza media superi i 15 m

Pressione del vento = qb*ce*cp*cd
qb (Pressione cinetica di riferimento): 45.56 <daN/mq>
ct (Coefficiente topografico): 1.00
ce (Coefficiente di esposizione): 0.00
cd (Coefficiente dinamico): 1.00

Tipologia di superficie:
Una parete con aperture di superficie minore di 1/3 di quella totale

sopravento: 0.80 sopravento su falda: -0.40 sottovento su falda: -0.40 sottovento: -0.40

Nome dell'analisi dei carichi da neve

NEVECalcolo delle azioni della neve

Normativa di riferimento:
 Norme tecniche per le costruzioni D.M. 14 gennaio 2008 e Circolare 2 febbraio
 2009, n. 617 del Ministero delle Infrastrutture e dei Trasporti

Area di ubicazione dell'edificio: 2
 Arezzo, Ascoli Piceno, Bari, Campobasso, Chieti, Ferrara, Firenze, Foggia, Genova, Gorizia, Imperia, Isernia, La Spezia, Lucca, Macerata, Mantova, Massa Carrara, Padova, Perugia, Pescara, Pistoia, Prato, Rovigo, Savona, Teramo, Trieste, Venezia, Verona

Altitudine sul livello del mare: 60 <m>

Tipologia di copertura: A due falde

Pressione della neve ps = μ1*qsk*Ce*Ct

Parametri d'input ed intermedi:
 Categoria del coefficiente d'esposizione: Normale
Ce (Coefficiente d'esposizione): 1.0
Ct (Coefficiente termico): 1.0
Angolo sinistro di inclinazione della falda : 53.0 <grad>
Angolo destro di inclinazione della falda : 24.0 <grad>
μ1(alfa1) (Coefficiente di forma della copertura): 0.19
μ1(alfa2) (Coefficiente di forma della copertura): 0.80

Carichi agenti:
qsk (Valore di riferimento del carico neve al suolo): 100.00 <daN/mq>
qss (Carico sinistro provocato dalla neve sulle coperture): 18.67 <daN/mq>
qsd (Carico destro provocato dalla neve sulle coperture): 80.00 <daN/mq>

PARAMETRI DI CALCOLO
La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con:
ModeSt ver. 8.14, prodotto da Tecnisoft s.a.s. - Prato

La struttura è stata calcolata utilizzando come solutore agli elementi finiti:
Xfinest ver. 2014, prodotto da Ce.A.S. S.r.l. - Milano

Tipo di normativa: stati limite D.M. 08
Tipo di calcolo: analisi sismica dinamica
Vincoli esterni: Considera sempre vincoli assegnati in modellazione
Schematizzazione piani rigidi:
  Imp.1: impalcato non rigido
  Imp.2: metodo Master-Slave
Modalità di recupero masse secondarie: trasferire all'impalcato più vicino con modifica XY baricentro

Generazione combinazioni
- Lineari: Sì
- Valuta spostamenti e non sollecitazioni: No
- buckling: No

Opzioni di calcolo
- Sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali con una riduzione del 20%
- Calcolo con offset rigidi dai nodi: No
- Uniformare i carichi variabili: No
- Massimizzare i carichi variabili: No
- Minimo carico da considerare: 0.00 <daN/m>
- Recupero carichi zone rigide: taglio e momento flettente
- Modalità di combinazione momento torcente: disaccoppiare le azioni

Opzioni del solutore
- Tipo di elemento bidimensionale: QF46
- Calcolo sforzo nei nodi: No
- Trascura deformabilità a taglio delle aste: No
- Analisi dinamica con metodo di Lanczos: Sì
- Check sequenza di Sturm: Sì
- Soluzione matrice con metodo ver. 5.1: No
- Analisi non lineare con Newton modificato: No
- Usa formulazione secante per buckling: No
- Trascura buckling torsionale: No

Dati struttura

- Zona sismica: zona 2
- Sito di costruzione: PRATO LON. 11.10220 LAT. 43.87770
  Contenuto tra ID reticolo: 19613 19612 19391 19390

Simbologia

TCC = Tipo di combinazione di carico
      SLU = Stato limite ultimo
      SLU S = Stato limite ultimo (azione sismica)
      SLE R = Stato limite d'esercizio, combinazione rara
      SLE F = Stato limite d'esercizio, combinazione frequente
      SLE Q = Stato limite d'esercizio, combinazione quasi permanente
      SLD = Stato limite di danno
      SLV = Stato limite di salvaguardia della vita
      SLC = Stato limite di prevenzione del collasso
      SLO = Stato limite di operatività
      SLU I = Stato limite di resistenza al fuoco
T_R = Periodo di ritorno <anni>
Ag = Accelerazione orizzontale massima al sito
FO = Valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale
TC* = Periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale <sec>
S_S = Coefficiente di amplificazione stratigrafica
C_C = Coefficiente funzione della categoria del suolo

TCC	T_R	Ag <g>	FO	TC*	S_S	C_C
SLD	75	0.0709	2.54	0.27	1.20	1.43
SLV	712	0.1633	2.41	0.31	1.20	1.39

- Edificio esistente: No
- Tipo di opera: Opera ordinaria
- Vita nominale V_N: 50.00
- Classe d'uso: Classe III
- SL Esercizio: SLO-Pvr No, SLD-Pvr 63.00
- SL Ultimi: SLV-Pvr 10.00, SLC-Pvr No
- Classe di duttilità: Classe B
- Quota di riferimento: -3.15 <m>
- Altezza della struttura: 17.50 <m>
- Numero piani edificio: 2
- Coefficiente θ: 0.00
- Edificio regolare in altezza: No
- Edificio regolare in pianta: No
- Forze orizzontali convenzionali per stati limite non sismici: 1.00%
- Genera stati limite per verifiche di resistenza al fuoco: No

Dati di piano

Simbologia

Imp. = Numero dell'impalcato
Lx = Dimensione del piano in dir. X
Ly = Dimensione del piano in dir. Y
Ex = Eccentricità in dir. X
Ey = Eccentricità in dir. Y
Ea = Eccentricità complessiva

Imp.	Lx <m>	Ly <m>	Ex <m>	Ey <m>	Ea <m>
1	12.60	8.96	0.63	0.45	0.77
2	23.87	12.91	1.19	0.65	1.36

Dati di calcolo
- Categoria del suolo di fondazione: B
- Tipologia edificio: c.a. o prefabbricato a telaio a più piani e più campate

Coeff. C_1: 0.075
Periodo T_1: 0.72653
Coeff. λ SLD: 1.00
Coeff. λ SLV: 1.00
Rapporto di sovraresistenza (α_u/α_1): 1.15
Valore di riferimento del fattore di struttura (q_0): 3.45

Fattore riduttivo (K_w): 1.00
Fattore riduttivo regolarità in altezza (KR): 0.80
Fattore di struttura (q): 3.00

- Categoria topografica: T1 - Superficie pianeggiante, pendii e rilievi isolati con inclinazione media i<=15°
- Coeff. amplificazione topografica S_T: 1.00
- Fattore di struttura per sisma verticale (qv): 1.50
- Modalità di calcolo modi di vibrare: Autovalori
- Numero modi: 24
- Modi da considerare: Tali da movimentare una percentuale di massa pari a 85.00%
- Trascura modi con massa movimentata minore di: No
- Smorzamento spettro: 5.00%

- Angolo di ingresso del sisma: 0.00 <grad>

CONDIZIONI DI CARICO ELEMENTARI:

Simbologia

CCE = Numero della condizione di carico elementare
Comm. = Commento
Tipo CCE = Tipo di CCE per calcolo agli stati limite
Sic. = Contributo alla sicurezza
  F = a favore
  S = a sfavore
  A = ambigua
Var. = Tipo di variabilità
  B = di base
  I = indipendente
  A = ambigua
Dir. = Direzione del vento
Tipo = Tipologia di pressione vento
  M = Massimizzata
  E = Esterna
  I = Interna
Mx = Moltiplicatore della massa in dir. X
My = Moltiplicatore della massa in dir. Y
Mz = Moltiplicatore della massa in dir. Z
Jpx = Moltiplicatore del momento d'inerzia intorno all'asse X
Jpy = Moltiplicatore del momento d'inerzia intorno all'asse Y
Jpz = Moltiplicatore del momento d'inerzia intorno all'asse Z

CCE	Comm.	Tipo CCE	Sic.	Var.	Dir. <grad>	Tipo	Mx	My	Mz	Jpx	Jpy	Jpz
1	PERMANENTI ST	1	S	--	--	--	1.00	1.00	0.00	0.00	0.00	1.00
2	PERMANENTI NST	2	S	--	--	--	1.00	1.00	0.00	0.00	0.00	1.00
3	ACCIDENTALI	5	S	A	--	--	1.00	1.00	0.00	0.00	0.00	1.00
4	NEVE	11	S	A	--	--	1.00	1.00	0.00	0.00	0.00	1.00
5	VENTO	10	S	A	--	--	1.00	1.00	0.00	0.00	0.00	1.00

ELENCO TIPI CCE DEFINITI:

Simbologia

Tipo CCE = Tipo condizione di carico elementare
Comm. = Commento
Tipo = Tipologia
  G = Permanente
  Qv = Variabile vento
  Q = Variabile
  I = Da ignorare
  A = Azione eccezionale
  P = Precompressione
Durata = Durata del carico
  N = Non definita
  P = Permanente
  L = Lunga
  M = Media

B = Breve
I = Istantanea
γ min. = Coeff. $\gamma_{min.}$
γ max = Coeff. γ_{max}
ψ_0 = Coeff. ψ_0
ψ_1 = Coeff. ψ_1
ψ_2 = Coeff. ψ_2
$\psi_{0,s}$ = Coeff. ψ_0 sismico (D.M. 96)

Tipo CCE	Comm.	Tipo	Durata	γ min.	γ max	ψ_0	ψ_1	ψ_2	$\psi_{0,s}$
1	D.M. 08 Permanenti strutturali	G	N	1.00	1.30				
2	D.M. 08 Permanenti non strutturali	G	N	0.00	1.50				
5	D.M. 08 Variabili Categoria C Ambienti suscettibili di affollamento	Q	N	0.00	1.50	0.70	0.70	0.60	0.00
11	D.M. 08 Variabili Neve (a quota <= 1000 m s.l.m.)	Q	N	0.00	1.50	0.50	0.20	0.00	0.00
10	D.M. 08 Variabili Vento	Q	N	0.00	1.50	0.60	0.20	0.00	0.00

AMBIENTI DI CARICO:

Simbologia

N = Numero
Comm. = Commento
1 = PERMANENTI ST
2 = PERMANENTI NST
3 = ACCIDENTALI
4 = NEVE
5 = VENTO
F = azioni orizzontali convenzionali
SLU = Stato limite ultimo
SLR = Stato limite per combinazioni rare
SLF = Stato limite per combinazioni frequenti
SLQ/D = Stato limite per combinazioni quasi permanenti o di danno
S = Sì
N = No

N	Comm.	1	2	3	4	5	F	S	SLU	SLR	SLF	SLQ
1	Calcolo sismico	S	S	S	N	N	N	S	S	N	N	N
2	Calcolo statico	S	S	S	S	S	S	N	S	S	S	S

ELENCO COMBINAZIONI DI CARICO SIMBOLICHE:

Simbologia

CC = Numero della combinazione delle condizioni di carico elementari
Comm. = Commento
TCC = Tipo di combinazione di carico
SLU = Stato limite ultimo
SLU S = Stato limite ultimo (azione sismica)
SLE R = Stato limite d'esercizio, combinazione rara
SLE F = Stato limite d'esercizio, combinazione frequente
SLE Q = Stato limite d'esercizio, combinazione quasi permanente
SLD = Stato limite di danno
SLV = Stato limite di salvaguardia della vita
SLC = Stato limite di prevenzione del collasso
SLO = Stato limite di operatività
SLU I = Stato limite di resistenza al fuoco

CC	Comm.	TCC	1	2	3	4	5	F	S
1	Amb. 1 (Sisma)	SLU S	1	1	ψ_2	-----	-----	-----	1
2	Amb. 2 (SLU)	SLU	γ max	γ max	γ max	γ max	γ max	1	-----

3	Amb. 2 (SLU)	SLU	γ max	γ max	ψ_0*γ max	γ max	γ max	1	-----
4	Amb. 2 (SLU)	SLU	γ max	γ max	γ max	ψ_0*γ max	γ max	1	-----
5	Amb. 2 (SLU)	SLU	γ max	γ max	ψ_0*γ max	ψ_0*γ max	γ max	1	-----
6	Amb. 2 (SLU)	SLU	γ max	γ max	γ max	γ max	ψ_0*γ max	1	-----
7	Amb. 2 (SLU)	SLU	γ max	γ max	ψ_0*γ max	γ max	ψ_0*γ max	1	-----
8	Amb. 2 (SLU)	SLU	γ max	γ max	γ max	ψ_0*γ max	ψ_0*γ max	1	-----
9	Amb. 2 (SLE R)	SLE R	1	1	1	1	1	1	-----
10	Amb. 2 (SLE R)	SLE R	1	1	ψ_0	1	1	1	-----
11	Amb. 2 (SLE R)	SLE R	1	1	1	ψ_0	1	1	-----
12	Amb. 2 (SLE R)	SLE R	1	1	ψ_0	ψ_0	1	1	-----
13	Amb. 2 (SLE R)	SLE R	1	1	1	1	ψ_0	1	-----
14	Amb. 2 (SLE R)	SLE R	1	1	ψ_0	1	ψ_0	1	-----
15	Amb. 2 (SLE R)	SLE R	1	1	1	ψ_0	ψ_0	1	-----
16	Amb. 2 (SLE F)	SLE F	1	1	ψ_1	ψ_1	ψ_1	1	-----
17	Amb. 2 (SLE F)	SLE F	1	1	ψ_2	ψ_1	ψ_1	1	-----
18	Amb. 2 (SLE F)	SLE F	1	1	ψ_1	ψ_2	ψ_1	1	-----
19	Amb. 2 (SLE F)	SLE F	1	1	ψ_2	ψ_2	ψ_1	1	-----
20	Amb. 2 (SLE F)	SLE F	1	1	ψ_1	ψ_1	ψ_2	1	-----
21	Amb. 2 (SLE F)	SLE F	1	1	ψ_2	ψ_1	ψ_2	1	-----
22	Amb. 2 (SLE F)	SLE F	1	1	ψ_1	ψ_2	ψ_2	1	-----
23	Amb. 2 (SLE Q)	SLE Q	1	1	ψ_2	ψ_2	ψ_2	1	-----

Genera le combinazioni con un solo carico di tipo variabile come di base: No

Considera sollecitazioni dinamiche con segno dei modi principali: No

COMBINAZIONI DELLE CCE:

Simbologia

CC = Numero della combinazione delle condizioni di carico elementari
Comm. = Commento
TCC = Tipo di combinazione di carico
- SLU = Stato limite ultimo
- SLU S = Stato limite ultimo (azione sismica)
- SLE R = Stato limite d'esercizio, combinazione rara
- SLE F = Stato limite d'esercizio, combinazione frequente
- SLE Q = Stato limite d'esercizio, combinazione quasi permanente
- SLD = Stato limite di danno
- SLV = Stato limite di salvaguardia della vita
- SLC = Stato limite di prevenzione del collasso
- SLO = Stato limite di operatività
- SLU I = Stato limite di resistenza al fuoco

An. = Tipo di analisi
- L = Lineare
- NL = Non lineare

Bk = buckling
- S = Sì
- N = No

CC	Comm.	TCC	An.	Bk	1	2	3	4	5	F X	F Y	Mt	±S X	±S Y
1	CC 1 - Amb. 1 (SLU S) S Mt+X+0.3Y	SLV	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	1.00	1.00	0.30
2	CC 2 - Amb. 1 (SLE) S Mt+X+0.3Y	SLD	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	1.00	1.00	0.30
3	CC 3 - Amb. 1 (SLU S) S Mt+X-0.3Y	SLV	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	1.00	1.00	-0.30
4	CC 4 - Amb. 1 (SLE) S Mt+X-0.3Y	SLD	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	1.00	1.00	-0.30
5	CC 5 - Amb. 1 (SLU S) S Mt+0.3X+Y	SLV	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	1.00	0.30	1.00
6	CC 6 - Amb. 1 (SLE) S Mt+0.3X+Y	SLD	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	1.00	0.30	1.00
7	CC 7 - Amb. 1 (SLU S) S Mt-0.3X+Y	SLV	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	1.00	-0.30	

1.00
  8 CC 8 - Amb. 1 (SLE) S Mt-0.3X+Y SLD L N 1.00 1.00 0.60 0.00 0.00 0.00 0.00 1.00 -0.30
1.00
  9 CC 9 - Amb. 1 (SLU S) S -Mt+X+0.3Y SLV L N 1.00 1.00 0.60 0.00 0.00 0.00 0.00 -1.00 1.00
0.30
 10 CC 10 - Amb. 1 (SLE) S -Mt+X+0.3Y SLD L N 1.00 1.00 0.60 0.00 0.00 0.00 0.00 -1.00 1.00
0.30
 11 CC 11 - Amb. 1 (SLU S) S -Mt+X-0.3Y SLV L N 1.00 1.00 0.60 0.00 0.00 0.00 0.00 -1.00 1.00 -
0.30
 12 CC 12 - Amb. 1 (SLE) S -Mt+X-0.3Y SLD L N 1.00 1.00 0.60 0.00 0.00 0.00 0.00 -1.00 1.00 -
0.30
 13 CC 13 - Amb. 1 (SLU S) S -Mt+0.3X+Y SLV L N 1.00 1.00 0.60 0.00 0.00 0.00 0.00 -1.00 0.30
1.00
 14 CC 14 - Amb. 1 (SLE) S -Mt+0.3X+Y SLD L N 1.00 1.00 0.60 0.00 0.00 0.00 0.00 -1.00 0.30
1.00
 15 CC 15 - Amb. 1 (SLU S) S -Mt-0.3X+Y SLV L N 1.00 1.00 0.60 0.00 0.00 0.00 0.00 -1.00 -0.30
1.00
 16 CC 16 - Amb. 1 (SLE) S -Mt-0.3X+Y SLD L N 1.00 1.00 0.60 0.00 0.00 0.00 0.00 -1.00 -0.30
1.00
 17 CC 17 - Amb. 2 (SLU) F X SLU L N 1.30 1.50 1.50 1.50 1.50 1.00 0.00 0.00 0.00
0.00
 18 CC 18 - Amb. 2 (SLU) F -X SLU L N 1.30 1.50 1.50 1.50 1.50 -1.00 0.00 0.00 0.00
0.00
 19 CC 19 - Amb. 2 (SLU) F Y SLU L N 1.30 1.50 1.50 1.50 1.50 0.00 1.00 0.00 0.00
0.00
 20 CC 20 - Amb. 2 (SLU) F -Y SLU L N 1.30 1.50 1.50 1.50 1.50 0.00 -1.00 0.00 0.00
0.00
 21 CC 21 - Amb. 2 (SLU) F X SLU L N 1.30 1.50 1.05 1.50 1.50 1.00 0.00 0.00 0.00
0.00
 22 CC 22 - Amb. 2 (SLU) F -X SLU L N 1.30 1.50 1.05 1.50 1.50 -1.00 0.00 0.00 0.00
0.00
 23 CC 23 - Amb. 2 (SLU) F Y SLU L N 1.30 1.50 1.05 1.50 1.50 0.00 1.00 0.00 0.00
0.00
 24 CC 24 - Amb. 2 (SLU) F -Y SLU L N 1.30 1.50 1.05 1.50 1.50 0.00 -1.00 0.00 0.00
0.00
 25 CC 25 - Amb. 2 (SLU) F X SLU L N 1.30 1.50 1.50 0.75 1.50 1.00 0.00 0.00 0.00
0.00
 26 CC 26 - Amb. 2 (SLU) F -X SLU L N 1.30 1.50 1.50 0.75 1.50 -1.00 0.00 0.00 0.00
0.00
 27 CC 27 - Amb. 2 (SLU) F Y SLU L N 1.30 1.50 1.50 0.75 1.50 0.00 1.00 0.00 0.00
0.00
 28 CC 28 - Amb. 2 (SLU) F -Y SLU L N 1.30 1.50 1.50 0.75 1.50 0.00 -1.00 0.00 0.00
0.00
 29 CC 29 - Amb. 2 (SLU) F X SLU L N 1.30 1.50 1.05 0.75 1.50 1.00 0.00 0.00 0.00
0.00
 30 CC 30 - Amb. 2 (SLU) F -X SLU L N 1.30 1.50 1.05 0.75 1.50 -1.00 0.00 0.00 0.00
0.00
 31 CC 31 - Amb. 2 (SLU) F Y SLU L N 1.30 1.50 1.05 0.75 1.50 0.00 1.00 0.00 0.00
0.00
 32 CC 32 - Amb. 2 (SLU) F -Y SLU L N 1.30 1.50 1.05 0.75 1.50 0.00 -1.00 0.00 0.00
0.00
 33 CC 33 - Amb. 2 (SLU) F X SLU L N 1.30 1.50 1.50 1.50 0.90 1.00 0.00 0.00 0.00
0.00
 34 CC 34 - Amb. 2 (SLU) F -X SLU L N 1.30 1.50 1.50 1.50 0.90 -1.00 0.00 0.00 0.00
0.00
 35 CC 35 - Amb. 2 (SLU) F Y SLU L N 1.30 1.50 1.50 1.50 0.90 0.00 1.00 0.00 0.00
0.00
 36 CC 36 - Amb. 2 (SLU) F -Y SLU L N 1.30 1.50 1.50 1.50 0.90 0.00 -1.00 0.00 0.00
0.00
 37 CC 37 - Amb. 2 (SLU) F X SLU L N 1.30 1.50 1.05 1.50 0.90 1.00 0.00 0.00 0.00
0.00
 38 CC 38 - Amb. 2 (SLU) F -X SLU L N 1.30 1.50 1.05 1.50 0.90 -1.00 0.00 0.00 0.00
0.00
 39 CC 39 - Amb. 2 (SLU) F Y SLU L N 1.30 1.50 1.05 1.50 0.90 0.00 1.00 0.00 0.00
0.00
 40 CC 40 - Amb. 2 (SLU) F -Y SLU L N 1.30 1.50 1.05 1.50 0.90 0.00 -1.00 0.00 0.00
0.00
 41 CC 41 - Amb. 2 (SLU) F X SLU L N 1.30 1.50 1.50 0.75 0.90 1.00 0.00 0.00 0.00
0.00
 42 CC 42 - Amb. 2 (SLU) F -X SLU L N 1.30 1.50 1.50 0.75 0.90 -1.00 0.00 0.00 0.00
0.00
 43 CC 43 - Amb. 2 (SLU) F Y SLU L N 1.30 1.50 1.50 0.75 0.90 0.00 1.00 0.00 0.00
0.00

44	CC 44 - Amb. 2 (SLU) F -Y	SLU		L	N	1.30	1.50	1.50	0.75	0.90	0.00	-1.00	0.00	0.00	0.00
45	CC 45 - Amb. 2 (SLE R) F X	SLE	R	L	N	1.00	1.00	1.00	1.00	1.00	1.00	0.00	0.00	0.00	0.00
46	CC 46 - Amb. 2 (SLE R) F -X	SLE	R	L	N	1.00	1.00	1.00	1.00	1.00	-1.00	0.00	0.00	0.00	0.00
47	CC 47 - Amb. 2 (SLE R) F Y	SLE	R	L	N	1.00	1.00	1.00	1.00	1.00	0.00	1.00	0.00	0.00	0.00
48	CC 48 - Amb. 2 (SLE R) F -Y	SLE	R	L	N	1.00	1.00	1.00	1.00	1.00	0.00	-1.00	0.00	0.00	0.00
49	CC 49 - Amb. 2 (SLE R) F X	SLE	R	L	N	1.00	1.00	0.70	1.00	1.00	1.00	0.00	0.00	0.00	0.00
50	CC 50 - Amb. 2 (SLE R) F -X	SLE	R	L	N	1.00	1.00	0.70	1.00	1.00	-1.00	0.00	0.00	0.00	0.00
51	CC 51 - Amb. 2 (SLE R) F Y	SLE	R	L	N	1.00	1.00	0.70	1.00	1.00	0.00	1.00	0.00	0.00	0.00
52	CC 52 - Amb. 2 (SLE R) F -Y	SLE	R	L	N	1.00	1.00	0.70	1.00	1.00	0.00	-1.00	0.00	0.00	0.00
53	CC 53 - Amb. 2 (SLE R) F X	SLE	R	L	N	1.00	1.00	1.00	0.50	1.00	1.00	0.00	0.00	0.00	0.00
54	CC 54 - Amb. 2 (SLE R) F -X	SLE	R	L	N	1.00	1.00	1.00	0.50	1.00	-1.00	0.00	0.00	0.00	0.00
55	CC 55 - Amb. 2 (SLE R) F Y	SLE	R	L	N	1.00	1.00	1.00	0.50	1.00	0.00	1.00	0.00	0.00	0.00
56	CC 56 - Amb. 2 (SLE R) F -Y	SLE	R	L	N	1.00	1.00	1.00	0.50	1.00	0.00	-1.00	0.00	0.00	0.00
57	CC 57 - Amb. 2 (SLE R) F X	SLE	R	L	N	1.00	1.00	0.70	0.50	1.00	1.00	0.00	0.00	0.00	0.00
58	CC 58 - Amb. 2 (SLE R) F -X	SLE	R	L	N	1.00	1.00	0.70	0.50	1.00	-1.00	0.00	0.00	0.00	0.00
59	CC 59 - Amb. 2 (SLE R) F Y	SLE	R	L	N	1.00	1.00	0.70	0.50	1.00	0.00	1.00	0.00	0.00	0.00
60	CC 60 - Amb. 2 (SLE R) F -Y	SLE	R	L	N	1.00	1.00	0.70	0.50	1.00	0.00	-1.00	0.00	0.00	0.00
61	CC 61 - Amb. 2 (SLE R) F X	SLE	R	L	N	1.00	1.00	1.00	1.00	0.60	1.00	0.00	0.00	0.00	0.00
62	CC 62 - Amb. 2 (SLE R) F -X	SLE	R	L	N	1.00	1.00	1.00	1.00	0.60	-1.00	0.00	0.00	0.00	0.00
63	CC 63 - Amb. 2 (SLE R) F Y	SLE	R	L	N	1.00	1.00	1.00	1.00	0.60	0.00	1.00	0.00	0.00	0.00
64	CC 64 - Amb. 2 (SLE R) F -Y	SLE	R	L	N	1.00	1.00	1.00	1.00	0.60	0.00	-1.00	0.00	0.00	0.00
65	CC 65 - Amb. 2 (SLE R) F X	SLE	R	L	N	1.00	1.00	0.70	1.00	0.60	1.00	0.00	0.00	0.00	0.00
66	CC 66 - Amb. 2 (SLE R) F -X	SLE	R	L	N	1.00	1.00	0.70	1.00	0.60	-1.00	0.00	0.00	0.00	0.00
67	CC 67 - Amb. 2 (SLE R) F Y	SLE	R	L	N	1.00	1.00	0.70	1.00	0.60	0.00	1.00	0.00	0.00	0.00
68	CC 68 - Amb. 2 (SLE R) F -Y	SLE	R	L	N	1.00	1.00	0.70	1.00	0.60	0.00	-1.00	0.00	0.00	0.00
69	CC 69 - Amb. 2 (SLE R) F X	SLE	R	L	N	1.00	1.00	1.00	0.50	0.60	1.00	0.00	0.00	0.00	0.00
70	CC 70 - Amb. 2 (SLE R) F -X	SLE	R	L	N	1.00	1.00	1.00	0.50	0.60	-1.00	0.00	0.00	0.00	0.00
71	CC 71 - Amb. 2 (SLE R) F Y	SLE	R	L	N	1.00	1.00	1.00	0.50	0.60	0.00	1.00	0.00	0.00	0.00
72	CC 72 - Amb. 2 (SLE R) F -Y	SLE	R	L	N	1.00	1.00	1.00	0.50	0.60	0.00	-1.00	0.00	0.00	0.00
73	CC 73 - Amb. 2 (SLE F) F X	SLE	F	L	N	1.00	1.00	0.70	0.20	0.20	1.00	0.00	0.00	0.00	0.00
74	CC 74 - Amb. 2 (SLE F) F -X	SLE	F	L	N	1.00	1.00	0.70	0.20	0.20	-1.00	0.00	0.00	0.00	0.00
75	CC 75 - Amb. 2 (SLE F) F Y	SLE	F	L	N	1.00	1.00	0.70	0.20	0.20	0.00	1.00	0.00	0.00	0.00
76	CC 76 - Amb. 2 (SLE F) F -Y	SLE	F	L	N	1.00	1.00	0.70	0.20	0.20	0.00	-1.00	0.00	0.00	0.00
77	CC 77 - Amb. 2 (SLE F) F X	SLE	F	L	N	1.00	1.00	0.60	0.20	0.20	1.00	0.00	0.00	0.00	0.00
78	CC 78 - Amb. 2 (SLE F) F -X	SLE	F	L	N	1.00	1.00	0.60	0.20	0.20	-1.00	0.00	0.00	0.00	0.00
79	CC 79 - Amb. 2 (SLE F) F Y	SLE	F	L	N	1.00	1.00	0.60	0.20	0.20	0.00	1.00	0.00	0.00	0.00
80	CC 80 - Amb. 2 (SLE F) F -Y	SLE	F	L	N	1.00	1.00	0.60	0.20	0.20	0.00	-1.00	0.00	0.00	0.00

0.00
 81 CC 81 - Amb. 2 (SLE F) F X SLE F L N 1.00 1.00 0.70 0.00 0.20 1.00 0.00 0.00 0.00
0.00
 82 CC 82 - Amb. 2 (SLE F) F -X SLE F L N 1.00 1.00 0.70 0.00 0.20 -1.00 0.00 0.00 0.00
0.00
 83 CC 83 - Amb. 2 (SLE F) F Y SLE F L N 1.00 1.00 0.70 0.00 0.20 0.00 1.00 0.00 0.00
0.00
 84 CC 84 - Amb. 2 (SLE F) F -Y SLE F L N 1.00 1.00 0.70 0.00 0.20 0.00 -1.00 0.00 0.00
0.00
 85 CC 85 - Amb. 2 (SLE F) F X SLE F L N 1.00 1.00 0.60 0.00 0.20 1.00 0.00 0.00 0.00
0.00
 86 CC 86 - Amb. 2 (SLE F) F -X SLE F L N 1.00 1.00 0.60 0.00 0.20 -1.00 0.00 0.00 0.00
0.00
 87 CC 87 - Amb. 2 (SLE F) F Y SLE F L N 1.00 1.00 0.60 0.00 0.20 0.00 1.00 0.00 0.00
0.00
 88 CC 88 - Amb. 2 (SLE F) F -Y SLE F L N 1.00 1.00 0.60 0.00 0.20 0.00 -1.00 0.00 0.00
0.00
 89 CC 89 - Amb. 2 (SLE F) F X SLE F L N 1.00 1.00 0.70 0.20 0.00 1.00 0.00 0.00 0.00
0.00
 90 CC 90 - Amb. 2 (SLE F) F -X SLE F L N 1.00 1.00 0.70 0.20 0.00 -1.00 0.00 0.00 0.00
0.00
 91 CC 91 - Amb. 2 (SLE F) F Y SLE F L N 1.00 1.00 0.70 0.20 0.00 0.00 1.00 0.00 0.00
0.00
 92 CC 92 - Amb. 2 (SLE F) F -Y SLE F L N 1.00 1.00 0.70 0.20 0.00 0.00 -1.00 0.00 0.00
0.00
 93 CC 93 - Amb. 2 (SLE F) F X SLE F L N 1.00 1.00 0.60 0.20 0.00 1.00 0.00 0.00 0.00
0.00
 94 CC 94 - Amb. 2 (SLE F) F -X SLE F L N 1.00 1.00 0.60 0.20 0.00 -1.00 0.00 0.00 0.00
0.00
 95 CC 95 - Amb. 2 (SLE F) F Y SLE F L N 1.00 1.00 0.60 0.20 0.00 0.00 1.00 0.00 0.00
0.00
 96 CC 96 - Amb. 2 (SLE F) F -Y SLE F L N 1.00 1.00 0.60 0.20 0.00 0.00 -1.00 0.00 0.00
0.00
 97 CC 97 - Amb. 2 (SLE F) F X SLE F L N 1.00 1.00 0.70 0.00 0.00 1.00 0.00 0.00 0.00
0.00
 98 CC 98 - Amb. 2 (SLE F) F -X SLE F L N 1.00 1.00 0.70 0.00 0.00 -1.00 0.00 0.00 0.00
0.00
 99 CC 99 - Amb. 2 (SLE F) F Y SLE F L N 1.00 1.00 0.70 0.00 0.00 0.00 1.00 0.00 0.00
0.00
100 CC 100 - Amb. 2 (SLE F) F -Y SLE F L N 1.00 1.00 0.70 0.00 0.00 0.00 -1.00 0.00 0.00
0.00
101 CC 101 - Amb. 2 (SLE Q) F X SLE Q L N 1.00 1.00 0.60 0.00 0.00 1.00 0.00 0.00 0.00
0.00
102 CC 102 - Amb. 2 (SLE Q) F -X SLE Q L N 1.00 1.00 0.60 0.00 0.00 -1.00 0.00 0.00 0.00
0.00
103 CC 103 - Amb. 2 (SLE Q) F Y SLE Q L N 1.00 1.00 0.60 0.00 0.00 0.00 1.00 0.00 0.00
0.00
104 CC 104 - Amb. 2 (SLE Q) F -Y SLE Q L N 1.00 1.00 0.60 0.00 0.00 0.00 -1.00 0.00 0.00
0.00

ELENCO BARICENTRI E MASSE IMPALCATI:

Simbologia

Imp. = Numero dell'impalcato
X = Coordinata X
Y = Coordinata Y
Z = Coordinata Z
Mo = Massa orizzontale
Jpz = Momento d'inerzia polare intorno all'asse Z

Imp.	X <m>	Y <m>	Z <m>	Mo <kg>	Jpz <kg*mq>
2	31.24	-19.55	5.00	546718.00	66033300.00

TOTALI MASSE IMPALCATI:

Mo <kg>	Jpz <kg*mq>

546718.00 66033300.00

ELENCO BARICENTRI E MASSE IMPALCATI:

Simbologia

Nodo = Numero del nodo
Mo = Massa orizzontale

Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>
-2580	1100.35	-2579	119.27	-2578	110.09	-2577	100.92	-2576	110.09	-2575	110.09	-2574	110.09
-1674	179.21	-1673	86.01	-1672	86.01	-1671	573.86	-1670	708.70	-1669	708.70	-1668	708.70
-1667	708.70	-1666	708.70	-1665	708.70	-1664	708.70	-1663	708.70	-1662	708.70	-1661	554.69
-1660	352.88	-1659	466.83	-1658	564.84	-1657	564.84	-1656	564.84	-1655	658.98	-1654	577.60
-1653	510.55	-1652	619.03	-1651	619.03	-1650	619.03	-1649	386.08	-1642	272.41	-1641	353.00
-1640	153.13	-1635	272.41	-1634	353.00	-1633	153.13	-1631	272.41	-1630	353.00	-1629	153.13
-1624	272.41	-1623	353.00	-1622	153.13	-1616	272.41	-1615	353.00	-1614	153.13	-1612	1702.67
-1611	2552.60	-1610	1704.34	-1609	1704.33	-1608	1704.33	-1607	1704.33	-1606	1704.34	-1605	1704.33
-1604	1704.33	-1603	1704.33	-1602	1408.69	-1601	5033.48	-1600	5222.24	-1599	1495.50	-1598	1488.68
-1597	1488.68	-1596	1488.68	-1595	1298.42	-1594	955.03	-1593	955.03	-1592	520.06	-1586	85.08
-1585	85.08	-1584	85.08	-1583	85.08	-1582	85.08	-1581	85.08	-1580	85.08	-1579	85.08
-1578	85.08	-1577	85.08	-1576	85.08	-1575	85.08	-1574	85.08	-1573	85.08	-1572	85.08
-1571	85.08	-1570	85.08	-1569	85.08	-1568	85.08	-1567	85.08	-1566	85.08	-1565	85.08
-1564	85.08	-1563	85.08	-1562	576.57	-1561	1068.06	-1560	1068.06	-1559	1068.06	-1558	1068.06
-1557	1068.06	-1556	1068.06	-1555	1068.06	-1554	1068.06	-1553	1068.06	-1552	1068.06	-1551	1068.06
-1550	1068.06	-1549	1068.06	-1548	1068.06	-1547	1068.06	-1546	1068.06	-1545	1068.06	-1544	1068.06
-1543	1068.06	-1542	1068.06	-1541	1068.06	-1540	1068.06	-1539	1068.06	-1538	1068.06	-1537	1068.06
-1536	576.57	-1534	158.54	-1533	172.02	-1532	172.02	-1531	242.83	-1530	168.58	-1529	168.58
-1528	168.58	-1527	168.58	-1526	168.58	-1525	168.58	-1524	168.58	-1523	168.58	-1522	168.58
-1521	128.15	-1520	87.73	-1519	121.27	-1518	154.82	-1517	154.82	-1516	154.82	-1515	180.62
-1514	151.03	-1513	121.44	-1512	147.25	-1511	147.25	-1510	147.25	-1509	146.16	-1508	145.07
-1507	145.07	-1506	145.07	-1505	145.07	-1504	145.07	-1503	145.07	-1502	145.07	-1501	145.07
-1500	145.07	-1499	145.07	-1498	145.07	-1497	145.07	-1496	145.07	-1495	145.07	-1494	145.07
-1493	157.62	-1492	156.82	-1491	168.58	-1490	168.58	-1489	168.58	-1488	168.58	-1487	168.58
-1486	168.58	-1485	168.58	-1484	168.58	-1483	140.86	-1482	62.69	-1481	151.34	-1480	147.25
-1479	147.25	-1478	147.25	-1477	220.70	-1476	149.08	-1475	149.08	-1474	159.62	-1473	170.17
-1472	170.17	-1471	170.17	-1470	170.17	-1469	170.17	-1468	170.17	-1467	170.17	-1466	170.17
-1465	170.17	-1464	170.17	-1463	170.17	-1462	170.17	-1461	170.17	-1460	170.17	-1459	170.17
-1458	170.17	-1457	170.17	-1456	170.17	-1455	170.17	-1454	170.17	-1453	170.17	-1452	170.17
-1451	170.17	-1450	170.17	-1449	168.44	-1448	166.72	-1447	166.72	-1446	166.73	-1445	166.73
-1444	166.72	-1443	166.72	-1442	166.72	-1441	166.72	-1440	166.72	-1439	166.72	-1438	166.72
-1437	166.72	-1436	166.72	-1435	166.72	-1434	166.72	-1433	166.72	-1432	166.72	-1431	166.72
-1430	166.72	-1429	166.72	-1428	166.72	-1427	166.72	-1426	166.72	-1425	166.72	-1424	166.72
-1423	168.45												

-1422 81.80 -1420 158.54 -1419 172.02 -1418 172.02 -1417 242.83 -1416 168.58 -1415
168.58 -1414 168.58
-1413 168.58 -1412 168.58 -1411 168.58 -1410 168.58 -1409 168.58 -1408 168.58 -1407
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-1325 166.72 -1324 166.72 -1323 166.72 -1322 166.72 -1321 166.72 -1320 166.72 -1319
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166.72 -1310 168.44
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168.58 -1301 168.58
-1300 168.58 -1299 168.58 -1298 168.58 -1297 168.58 -1296 168.58 -1295 168.58 -1294
168.58 -1293 128.15
-1292 87.73 -1291 121.27 -1290 154.82 -1289 154.82 -1288 154.82 -1287 180.62 -1286
151.03 -1285 121.44
-1284 147.25 -1283 147.25 -1282 147.25 -1281 146.16 -1280 145.07 -1279 145.07 -1278
145.07 -1277 145.07
-1276 145.07 -1275 145.07 -1274 145.07 -1273 145.07 -1272 145.07 -1271 145.07 -1270
145.07 -1269 145.07
-1268 145.07 -1267 145.07 -1266 145.07 -1265 157.62 -1264 156.82 -1263 168.58 -1262
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-1204 166.72 -1203 166.72 -1202 166.72 -1201 166.72 -1200 166.72 -1199 166.72 -1198
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-1196 166.72 -1195 168.44 -1193 70.35 -1192 158.54 -1191 172.02 -1190 172.02 -1189
242.83 -1188 168.58
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168.58 -1180 168.58
-1179 128.15 -1178 87.73 -1177 121.27 -1176 154.82 -1175 154.82 -1174 154.82 -1173
180.62 -1172 151.03
-1171 121.44 -1170 147.25 -1169 147.25 -1168 147.25 -1167 146.16 -1166 145.07 -1165
145.07 -1164 145.07
-1163 145.07 -1162 145.07 -1161 145.07 -1160 145.07 -1159 145.07 -1158 145.07 -1157
145.07 -1156 145.07
-1155 145.07 -1154 145.07 -1153 145.07 -1152 145.07 -1151 157.62 -1150 156.82 -1149
168.58 -1148 168.58
-1147 168.58 -1146 168.58 -1145 168.58 -1144 168.58 -1143 168.58 -1142 168.58 -1141
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149.08 -1132 159.62
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-1123 170.17 -1122 170.17 -1121 170.17 -1120 170.17 -1119 170.17 -1118 170.17 -1117
170.17 -1116 170.17
-1115 170.17 -1114 170.17 -1113 170.17 -1112 170.17 -1111 170.17 -1110 170.17 -1109
170.17 -1108 170.17
-1107 168.44 -1106 166.72 -1105 166.72 -1104 166.73 -1103 166.73 -1102 166.72 -1101
166.72 -1100 166.72
-1099 166.72 -1098 166.72 -1097 166.72 -1096 166.72 -1095 166.72 -1094 166.72 -1093
166.72 -1092 166.72
-1091 166.72 -1090 166.72 -1089 166.72 -1088 166.72 -1087 166.72 -1086 166.72 -1085
166.72 -1084 166.72
-1083 166.72 -1082 166.72 -1081 168.44 -1079 70.35 -1077 158.54 -1076 172.02 -1075
172.02 -1074 242.83
-1073 168.58 -1072 168.58 -1071 168.58 -1070 168.58 -1069 168.58 -1068 168.58 -1067
168.58 -1066 168.58
-1065 168.58 -1064 128.15 -1063 87.73 -1062 121.27 -1061 154.82 -1060 154.82 -1059
154.82 -1058 180.62
-1057 151.03 -1056 121.44 -1055 147.25 -1054 147.25 -1053 147.25 -1052 146.16 -1051
145.07 -1050 145.07
-1049 145.07 -1048 145.07 -1047 145.07 -1046 145.07 -1045 145.07 -1044 145.07 -1043
145.07 -1042 145.07
-1041 145.07 -1040 145.07 -1039 145.07 -1038 145.07 -1037 145.07 -1036 157.62 -1035
156.82 -1034 168.58
-1033 168.58 -1032 168.58 -1031 168.58 -1030 168.58 -1029 168.58 -1028 168.58 -1027
168.58 -1026 139.34
-1025 55.05 -1024 145.61 -1023 147.25 -1022 147.25 -1021 147.25 -1020 220.70 -1019
149.08 -1018 149.08
-1017 159.62 -1016 170.17 -1015 170.17 -1014 170.17 -1013 170.17 -1012 170.17 -1011
170.17 -1010 170.17
-1009 170.17 -1008 170.17 -1007 170.17 -1006 170.17 -1005 170.17 -1004 170.17 -1003
170.17 -1002 170.17
-1001 170.17 -1000 170.17 -999 170.17 -998 170.17 -997 170.17 -996 170.17 -995
170.17 -994 170.17
-993 170.17 -992 168.44 -991 166.72 -990 166.72 -989 166.73 -988 166.73 -987
166.72 -986 166.72
-985 166.72 -984 166.72 -983 166.72 -982 166.72 -981 166.72 -980 166.72 -979
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166.72 -970 166.72
-969 166.72 -968 166.72 -967 166.72 -966 168.44 -965 70.35 -963 158.54 -962
172.02 -961 172.02
-960 242.83 -959 168.58 -958 168.58 -957 168.58 -956 168.58 -955 168.58 -954
168.58 -953 168.58
-952 168.58 -951 168.58 -950 128.15 -949 87.73 -948 121.27 -947 154.82 -946
154.82 -945 154.82
-944 180.62 -943 151.03 -942 121.44 -941 147.25 -940 147.25 -939 147.25 -938
146.16 -937 145.07
-936 145.07 -935 145.07 -934 145.07 -933 145.07 -932 145.07 -931 145.07 -930
145.07 -929 145.07
-928 145.07 -927 145.07 -926 145.07 -925 145.07 -924 145.07 -923 145.07 -922
157.62 -921 156.82
-920 168.58 -919 168.58 -918 168.58 -917 168.58 -916 168.58 -915 168.58 -914
168.58 -913 168.58
-912 139.34 -911 55.05 -910 145.61 -909 147.25 -908 147.25 -907 147.25 -906
220.70 -905 149.08
-904 149.08 -903 159.62 -902 170.17 -901 170.17 -900 170.17 -899 170.17 -898
170.17 -897 170.17
-896 170.17 -895 170.17 -894 170.17 -893 170.17 -892 170.17 -891 170.17 -890
170.17 -889 170.17
-888 170.17 -887 170.17 -886 170.17 -885 170.17 -884 170.17 -883 170.17 -882
170.17 -881 170.17
-880 170.17 -879 170.17 -878 168.44 -877 166.72 -876 166.72 -875 166.73 -874
166.73 -873 166.72
-872 166.72 -871 166.72 -870 166.72 -869 166.72 -868 166.72 -867 166.72 -866
166.72 -865 166.72
-864 166.72 -863 166.72 -862 166.72 -861 166.72 -860 166.72 -859 166.72 -858
166.72 -857 166.72
-856 166.72 -855 166.72 -854 166.72 -853 166.72 -852 168.45 -851 70.35

TOTALI MASSE NODI:

Mo <kg>

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197551.00
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ELENCO FORZE SISMICHE DI IMPALCATO

Simbologia

Imp. = Numero dell'impalcato
cx = Coeff. c in dir. X
cy = Coeff. c in dir. Y
Mz = Momento intorno all'asse Z

Imp.	cx	cy	Mz <daNm>
2	0.91	0.91	104298.00

TOTALI FORZE SISMICHE:

Mz <daNm>
104298.00

ELENCO FORZE SISMICHE DI IMPALCATO

Imp.	cx	cy	Mz <daNm>
2	0.91	0.91	83033.20

TOTALI FORZE SISMICHE:

Mz <daNm>
83033.20

ELENCO PESI E FORZE FITTIZIE IMPALCATI:

Simbologia

Imp. = Numero dell'impalcato
Peso = Peso
Fx = Forza in dir. X
Fy = Forza in dir. Y

Imp.	Peso <daN>	Fx <daN>	Fy <daN>
2	641012.00	6410.12	6410.12

ELENCO PESI E FORZE FITTIZIE IMPALCATI:

Simbologia

Nodo = Numero del nodo
Peso = Peso
Fx = Forza in dir. X
Fy = Forza in dir. Y

Nodo	Peso <daN>	Fx <daN>	Fy <daN>	Nodo	Peso <daN>	Fx <daN>	Fy <daN>	Nodo	Peso <daN>	Fx <daN>	Fy <daN>	Nodo	Peso <daN>	Fx <daN>	Fy <daN>
-2580	1347.60	13.48	13.48	-2579	117.00	1.17	1.17	-2578	108.00	1.08	1.08	-2577	99.00	0.99	0.99
-2576	108.00	1.08	1.08	-2575	108.00	1.08	1.08	-2574	108.00	1.08	1.08	-1674	207.43	2.07	

2.07
-1673 84.38 0.84 0.84 -1672 84.38 0.84 0.84 -1671 644.17 6.44 6.44 -1670 794.41 7.94
7.94
-1669 794.41 7.94 7.94 -1668 794.41 7.94 7.94 -1667 794.41 7.94 7.94 -1666 794.41 7.94
7.94
-1665 794.41 7.94 7.94 -1664 794.41 7.94 7.94 -1663 794.41 7.94 7.94 -1662 794.41 7.94
7.94
-1661 622.52 6.23 6.23 -1660 394.81 3.95 3.95 -1659 529.30 5.29 5.29 -1658 645.19 6.45
6.45
-1657 645.19 6.45 6.45 -1656 645.19 6.45 6.45 -1655 752.72 7.53 7.53 -1654 655.48 6.55
6.55
-1653 572.30 5.72 5.72 -1652 693.89 6.94 6.94 -1651 693.89 6.94 6.94 -1650 693.89 6.94
6.94
-1649 422.06 4.22 4.22 -1642 330.48 3.30 3.30 -1641 409.54 4.10 4.10 -1640 150.22 1.50
1.50
-1635 330.48 3.30 3.30 -1634 409.54 4.10 4.10 -1633 150.22 1.50 1.50 -1631 330.48 3.30
3.30
-1630 409.54 4.10 4.10 -1629 150.22 1.50 1.50 -1624 330.48 3.30 3.30 -1623 409.54 4.10
4.10
-1622 150.22 1.50 1.50 -1616 330.48 3.30 3.30 -1615 409.54 4.10 4.10 -1614 150.22 1.50
1.50
-1612 2184.20 21.84 21.84 -1611 3225.10 32.25 32.25 -1610 2086.20 20.86 20.86 -1609 2086.20 20.86
20.86
-1608 2086.20 20.86 20.86 -1607 2086.20 20.86 20.86 -1606 2086.21 20.86 20.86 -1605 2086.20 20.86
20.86
-1604 2086.20 20.86 20.86 -1603 2086.20 20.86 20.86 -1602 1724.31 17.24 17.24 -1601 6178.72 61.79
61.79
-1600 6407.18 64.07 64.07 -1599 1828.92 18.29 18.29 -1598 1822.23 18.22 18.22 -1597 1822.23 18.22
18.22
-1596 1822.23 18.22 18.22 -1595 1593.98 15.94 15.94 -1594 1215.52 12.16 12.16 -1593 1215.52 12.16
12.16
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1.42														
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1.42														
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1.65														
-1490	165.38	1.65	1.65	-1489	165.38	1.65	1.65	-1488	165.38	1.65	1.65	-1487	165.38	1.65
1.65														
-1486	165.38	1.65	1.65	-1485	165.38	1.65	1.65	-1484	165.38	1.65	1.65	-1483	138.19	1.38
1.38														
-1482	61.50	0.61	0.61	-1481	148.46	1.48	1.48	-1480	144.45	1.44	1.44	-1479	144.45	1.44
1.44														
-1478	144.45	1.44	1.44	-1477	216.51	2.17	2.17	-1476	146.25	1.46	1.46	-1475	146.25	1.46
1.46														
-1474	156.59	1.57	1.57	-1473	166.93	1.67	1.67	-1472	166.93	1.67	1.67	-1471	166.93	1.67
1.67														
-1470	166.93	1.67	1.67	-1469	166.93	1.67	1.67	-1468	166.93	1.67	1.67	-1467	166.93	1.67
1.67														
-1466	166.93	1.67	1.67	-1465	166.93	1.67	1.67	-1464	166.93	1.67	1.67	-1463	166.93	1.67
1.67														
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1.67														
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1.67														
-1450	166.93	1.67	1.67	-1449	165.24	1.65	1.65	-1448	163.56	1.64	1.64	-1447	163.56	1.64
1.64														
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1.64														
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1.64														
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1.65														
-1422	80.25	0.80	0.80	-1420	155.53	1.56	1.56	-1419	168.75	1.69	1.69	-1418	168.75	1.69
1.69														
-1417	238.22	2.38	2.38	-1416	165.38	1.65	1.65	-1415	165.38	1.65	1.65	-1414	165.38	1.65
1.65														
-1413	165.38	1.65	1.65	-1412	165.38	1.65	1.65	-1411	165.38	1.65	1.65	-1410	165.38	1.65
1.65														
-1409	165.38	1.65	1.65	-1408	165.38	1.65	1.65	-1407	125.72	1.26	1.26	-1406	86.06	0.86
0.86														
-1405	118.97	1.19	1.19	-1404	151.88	1.52	1.52	-1403	151.88	1.52	1.52	-1402	151.88	1.52
1.52														
-1401	177.19	1.77	1.77	-1400	148.16	1.48	1.48	-1399	119.14	1.19	1.19	-1398	144.45	1.44
1.44														
-1397	144.45	1.44	1.44	-1396	144.45	1.44	1.44	-1395	143.38	1.43	1.43	-1394	142.31	1.42
1.42														
-1393	142.31	1.42	1.42	-1392	142.31	1.42	1.42	-1391	142.31	1.42	1.42	-1390	142.31	1.42
1.42														
-1389	142.31	1.42	1.42	-1388	142.31	1.42	1.42	-1387	142.31	1.42	1.42	-1386	142.31	1.42
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-1385	142.31	1.42	1.42	-1384	142.31	1.42	1.42	-1383	142.31	1.42	1.42	-1382	142.31	1.42
1.42														
-1381	142.31	1.42	1.42	-1380	142.31	1.42	1.42	-1379	154.62	1.55	1.55	-1378	153.84	1.54
1.54														
-1377	165.38	1.65	1.65	-1376	165.38	1.65	1.65	-1375	165.38	1.65	1.65	-1374	165.38	1.65
1.65														
-1373	165.38	1.65	1.65	-1372	165.38	1.65	1.65	-1371	165.38	1.65	1.65	-1370	165.38	1.65
1.65														
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1.44														
-1365	144.45	1.44	1.44	-1364	216.51	2.17	2.17	-1363	146.25	1.46	1.46	-1362	146.25	1.46
1.46														
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1.67														
-1357	166.93	1.67	1.67	-1356	166.93	1.67	1.67	-1355	166.93	1.67	1.67	-1354	166.93	1.67

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-1208	163.56	1.64	1.64	-1207	163.56	1.64	1.64	-1206	163.56	1.64	1.64	-1205	163.56	1.64
1.64														
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1.64														
-1200	163.56	1.64	1.64	-1199	163.56	1.64	1.64	-1198	163.56	1.64	1.64	-1197	163.56	1.64
1.64														
-1196	163.56	1.64	1.64	-1195	165.25	1.65	1.65	-1193	69.02	0.69	0.69	-1192	155.53	1.56
1.56														
-1191	168.75	1.69	1.69	-1190	168.75	1.69	1.69	-1189	238.22	2.38	2.38	-1188	165.38	1.65
1.65														
-1187	165.38	1.65	1.65	-1186	165.38	1.65	1.65	-1185	165.38	1.65	1.65	-1184	165.38	1.65
1.65														
-1183	165.38	1.65	1.65	-1182	165.38	1.65	1.65	-1181	165.38	1.65	1.65	-1180	165.38	1.65
1.65														
-1179	125.72	1.26	1.26	-1178	86.06	0.86	0.86	-1177	118.97	1.19	1.19	-1176	151.88	1.52
1.52														
-1175	151.88	1.52	1.52	-1174	151.88	1.52	1.52	-1173	177.19	1.77	1.77	-1172	148.16	1.48
1.48														
-1171	119.14	1.19	1.19	-1170	144.45	1.44	1.44	-1169	144.45	1.44	1.44	-1168	144.45	1.44
1.44														
-1167	143.38	1.43	1.43	-1166	142.31	1.42	1.42	-1165	142.31	1.42	1.42	-1164	142.31	1.42
1.42														
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1.42														
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1.42														
-1155	142.31	1.42	1.42	-1154	142.31	1.42	1.42	-1153	142.31	1.42	1.42	-1152	142.31	1.42
1.42														
-1151	154.62	1.55	1.55	-1150	153.84	1.54	1.54	-1149	165.38	1.65	1.65	-1148	165.38	1.65
1.65														
-1147	165.38	1.65	1.65	-1146	165.38	1.65	1.65	-1145	165.38	1.65	1.65	-1144	165.38	1.65
1.65														
-1143	165.38	1.65	1.65	-1142	165.38	1.65	1.65	-1141	136.69	1.37	1.37	-1140	54.00	0.54
0.54														
-1139	142.85	1.43	1.43	-1138	144.45	1.44	1.44	-1137	144.45	1.44	1.44	-1136	144.45	1.44
1.44														
-1135	216.51	2.17	2.17	-1134	146.25	1.46	1.46	-1133	146.25	1.46	1.46	-1132	156.59	1.57
1.57														
-1131	166.93	1.67	1.67	-1130	166.93	1.67	1.67	-1129	166.93	1.67	1.67	-1128	166.93	1.67
1.67														
-1127	166.93	1.67	1.67	-1126	166.93	1.67	1.67	-1125	166.93	1.67	1.67	-1124	166.93	1.67
1.67														
-1123	166.93	1.67	1.67	-1122	166.93	1.67	1.67	-1121	166.93	1.67	1.67	-1120	166.93	1.67
1.67														
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1.67														
-1115	166.93	1.67	1.67	-1114	166.93	1.67	1.67	-1113	166.93	1.67	1.67	-1112	166.93	1.67
1.67														
-1111	166.93	1.67	1.67	-1110	166.93	1.67	1.67	-1109	166.93	1.67	1.67	-1108	166.93	1.67
1.67														
-1107	165.24	1.65	1.65	-1106	163.56	1.64	1.64	-1105	163.56	1.64	1.64	-1104	163.56	1.64
1.64														
-1103	163.56	1.64	1.64	-1102	163.56	1.64	1.64	-1101	163.56	1.64	1.64	-1100	163.56	1.64
1.64														
-1099	163.56	1.64	1.64	-1098	163.56	1.64	1.64	-1097	163.56	1.64	1.64	-1096	163.56	1.64
1.64														
-1095	163.56	1.64	1.64	-1094	163.56	1.64	1.64	-1093	163.56	1.64	1.64	-1092	163.56	1.64
1.64														
-1091	163.56	1.64	1.64	-1090	163.56	1.64	1.64	-1089	163.56	1.64	1.64	-1088	163.56	1.64
1.64														
-1087	163.56	1.64	1.64	-1086	163.56	1.64	1.64	-1085	163.56	1.64	1.64	-1084	163.56	1.64
1.64														
-1083	163.56	1.64	1.64	-1082	163.56	1.64	1.64	-1081	165.25	1.65	1.65	-1079	69.02	0.69
0.69														
-1077	155.53	1.56	1.56	-1076	168.75	1.69	1.69	-1075	168.75	1.69	1.69	-1074	238.22	2.38
2.38														
-1073	165.38	1.65	1.65	-1072	165.38	1.65	1.65	-1071	165.38	1.65	1.65	-1070	165.38	1.65
1.65														
-1069	165.38	1.65	1.65	-1068	165.38	1.65	1.65	-1067	165.38	1.65	1.65	-1066	165.38	1.65
1.65														
-1065	165.38	1.65	1.65	-1064	125.72	1.26	1.26	-1063	86.06	0.86	0.86	-1062	118.97	1.19
1.19														
-1061	151.88	1.52	1.52	-1060	151.88	1.52	1.52	-1059	151.88	1.52	1.52	-1058	177.19	1.77

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-1053 144.45 1.44 1.44 -1052 143.38 1.43 1.43 -1051 142.31 1.42 1.42 -1050 142.31 1.42
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-1049 142.31 1.42 1.42 -1048 142.31 1.42 1.42 -1047 142.31 1.42 1.42 -1046 142.31 1.42
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-1037 142.31 1.42 1.42 -1036 154.62 1.55 1.55 -1035 153.84 1.54 1.54 -1034 165.38 1.65
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-1029 165.38 1.65 1.65 -1028 165.38 1.65 1.65 -1027 165.38 1.65 1.65 -1026 136.69 1.37
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-1025 54.00 0.54 0.54 -1024 142.84 1.43 1.43 -1023 144.45 1.44 1.44 -1022 144.45 1.44
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-1021 144.45 1.44 1.44 -1020 216.51 2.17 2.17 -1019 146.25 1.46 1.46 -1018 146.25 1.46
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-1017 156.59 1.57 1.57 -1016 166.93 1.67 1.67 -1015 166.93 1.67 1.67 -1014 166.93 1.67
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-1013 166.93 1.67 1.67 -1012 166.93 1.67 1.67 -1011 166.93 1.67 1.67 -1010 166.93 1.67
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-1009 166.93 1.67 1.67 -1008 166.93 1.67 1.67 -1007 166.93 1.67 1.67 -1006 166.93 1.67
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-1005 166.93 1.67 1.67 -1004 166.93 1.67 1.67 -1003 166.93 1.67 1.67 -1002 166.93 1.67
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-1001 166.93 1.67 1.67 -1000 166.93 1.67 1.67 -999 166.93 1.67 1.67 -998 166.93 1.67
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-993 166.93 1.67 1.67 -992 165.24 1.65 1.65 -991 163.56 1.64 1.64 -990 163.56 1.64
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-969 163.56 1.64 1.64 -968 163.56 1.64 1.64 -967 163.56 1.64 1.64 -966 165.25 1.65
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-965 69.02 0.69 0.69 -963 155.53 1.56 1.56 -962 168.75 1.69 1.69 -961 168.75 1.69
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-960 238.22 2.38 2.38 -959 165.38 1.65 1.65 -958 165.38 1.65 1.65 -957 165.38 1.65
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-944 177.19 1.77 1.77 -943 148.16 1.48 1.48 -942 119.14 1.19 1.19 -941 144.45 1.44
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-940 144.45 1.44 1.44 -939 144.45 1.44 1.44 -938 143.38 1.43 1.43 -937 142.31 1.42
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-936 142.31 1.42 1.42 -935 142.31 1.42 1.42 -934 142.31 1.42 1.42 -933 142.31 1.42
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-932 142.31 1.42 1.42 -931 142.31 1.42 1.42 -930 142.31 1.42 1.42 -929 142.31 1.42
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-928 142.31 1.42 1.42 -927 142.31 1.42 1.42 -926 142.31 1.42 1.42 -925 142.31 1.42
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-924 142.31 1.42 1.42 -923 142.31 1.42 1.42 -922 154.62 1.55 1.55 -921 153.84 1.54
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-920 165.38 1.65 1.65 -919 165.38 1.65 1.65 -918 165.38 1.65 1.65 -917 165.38 1.65
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-916 165.38 1.65 1.65 -915 165.38 1.65 1.65 -914 165.38 1.65 1.65 -913 165.38 1.65
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-912	136.69	1.37	1.37	-911	54.00	0.54	0.54	-910	142.84	1.43	1.43	-909	144.45	1.44
1.44														
-908	144.45	1.44	1.44	-907	144.45	1.44	1.44	-906	216.51	2.17	2.17	-905	146.25	1.46
1.46														
-904	146.25	1.46	1.46	-903	156.59	1.57	1.57	-902	166.93	1.67	1.67	-901	166.93	1.67
1.67														
-900	166.93	1.67	1.67	-899	166.93	1.67	1.67	-898	166.93	1.67	1.67	-897	166.93	1.67
1.67														
-896	166.93	1.67	1.67	-895	166.93	1.67	1.67	-894	166.93	1.67	1.67	-893	166.93	1.67
1.67														
-892	166.93	1.67	1.67	-891	166.93	1.67	1.67	-890	166.93	1.67	1.67	-889	166.93	1.67
1.67														
-888	166.93	1.67	1.67	-887	166.93	1.67	1.67	-886	166.93	1.67	1.67	-885	166.93	1.67
1.67														
-884	166.93	1.67	1.67	-883	166.93	1.67	1.67	-882	166.93	1.67	1.67	-881	166.93	1.67
1.67														
-880	166.93	1.67	1.67	-879	166.93	1.67	1.67	-878	165.24	1.65	1.65	-877	163.56	1.64
1.64														
-876	163.56	1.64	1.64	-875	163.56	1.64	1.64	-874	163.56	1.64	1.64	-873	163.56	1.64
1.64														
-872	163.56	1.64	1.64	-871	163.56	1.64	1.64	-870	163.56	1.64	1.64	-869	163.56	1.64
1.64														
-868	163.56	1.64	1.64	-867	163.56	1.64	1.64	-866	163.56	1.64	1.64	-865	163.56	1.64
1.64														
-864	163.56	1.64	1.64	-863	163.56	1.64	1.64	-862	163.56	1.64	1.64	-861	163.56	1.64
1.64														
-860	163.56	1.64	1.64	-859	163.56	1.64	1.64	-858	163.56	1.64	1.64	-857	163.56	1.64
1.64														
-856	163.56	1.64	1.64	-855	163.56	1.64	1.64	-854	163.56	1.64	1.64	-853	163.56	1.64
1.64														
-852	165.25	1.65	1.65	-851	69.02	0.69	0.69							

ELENCO MODI DI VIBRARE, MASSE PARTECIPANTI E COEFFICIENTI DI PARTECIPAZIONE

Simbologia

Modo = Numero del modo di vibrare
C = * indica che il modo è stato considerato
Per. = Periodo
Diff. = Minima differenza percentuale dagli altri periodi
Φx = Coefficiente di partecipazione in dir. X
Φy = Coefficiente di partecipazione in dir. Y
Φz = Coefficiente di partecipazione in dir. Z
%Mx = Percentuale massa partecipante in dir. X
%My = Percentuale massa partecipante in dir. Y
%Mz = Percentuale massa partecipante in dir. Z
%Jpz = Percentuale momento d'inerzia polare partecipante intorno all'asse Z

Modo	C	Per.	Diff.	**Φ**x	**Φ**y	**Φ**z	%Mx	%My	%Mz	%Jpz
1	*	0.7832	71.89	28.08	-183.40	0.00	1.060	45.191	0.000	39.663
2	*	0.4556	5.55	10.80	-165.86	0.00	0.157	36.964	0.000	58.250
3	*	0.4317	5.55	246.47	28.55	0.00	81.623	1.095	0.000	0.088
4	*	0.1459	65.11	-1.43	-52.72	0.00	0.003	3.735	0.000	0.112
5		0.0884	7.08	-8.13	31.80	0.00	0.089	1.358	0.000	0.421
6		0.0825	7.08	29.89	5.90	0.00	1.201	0.047	0.000	0.027
7	*	0.0639	9.08	-53.49	-4.97	0.00	3.845	0.033	0.000	0.003
8		0.0586	9.08	5.29	-31.10	0.00	0.038	1.300	0.000	0.346
9		0.0536	4.43	-29.75	9.71	0.00	1.189	0.127	0.000	0.068
10		0.0513	4.24	-10.11	6.23	0.00	0.137	0.052	0.000	0.001
11		0.0493	4.24	2.57	-29.04	0.00	0.009	1.133	0.000	0.016
12		0.0362	7.70	-20.25	1.63	0.00	0.551	0.004	0.000	0.016
13		0.0336	3.06	2.76	25.09	0.00	0.010	0.846	0.000	0.193
14		0.0326	2.13	3.03	10.51	0.00	0.012	0.148	0.000	0.011
15		0.0319	2.13	-4.13	-10.50	0.00	0.023	0.148	0.000	0.030
16		0.0295	6.47	3.06	36.47	0.00	0.013	1.787	0.000	0.035
17		0.0277	6.47	-4.36	18.74	0.00	0.026	0.472	0.000	0.021
18		0.0214	3.52	-16.83	14.54	0.00	0.381	0.284	0.000	0.007
19		0.0207	3.52	-16.20	-23.29	0.00	0.353	0.729	0.000	0.199
20		0.0195	5.75	-31.84	0.22	0.00	1.362	0.000	0.000	0.016

21	0.0178	5.14	-12.88	-0.69	0.00	0.223	0.001	0.000	0.006
22	0.0170	2.28	-16.72	-5.36	0.00	0.376	0.039	0.000	0.112
23	0.0166	2.28	5.30	-14.47	0.00	0.038	0.281	0.000	0.009
24	0.0159	4.35	1.42	5.54	0.00	0.003	0.041	0.000	0.002
Tot.cons.						86.69	87.02	0.00	98.12

ELENCO COEFFICIENTI DI RISPOSTA

Simbologia

Modo = Numero del modo di vibrare
Sx = Coefficiente di risposta (moltiplicato per 100) in dir. X
Sy = Coefficiente di risposta (moltiplicato per 100) in dir. Y

Stato limite di dannoModo Sx Sy

Modo	Sx	Sy
1	10.75	10.75
2	18.48	18.48
3	19.51	19.51
4	21.57	21.57
5	17.38	17.38
6	16.79	16.79
7	14.92	14.92
8	14.39	14.39
9	13.89	13.89
10	13.66	13.66
11	13.45	13.45
12	12.14	12.14
13	11.88	11.88
14	11.78	11.78
15	11.71	11.71
16	11.47	11.47
17	11.29	11.29
18	10.65	10.65
19	10.58	10.58
20	10.47	10.47
21	10.30	10.30
22	10.21	10.21
23	10.17	10.17
24	10.10	10.10

Stato limite di salvaguardia della vitaModo Sx Sy

Modo	Sx	Sy
1	8.56	8.56
2	14.71	14.71
3	15.53	15.53
4	15.74	15.74
5	17.19	17.19
6	17.35	17.35
7	17.86	17.86
8	18.00	18.00
9	18.14	18.14
10	18.20	18.20
11	18.26	18.26
12	18.61	18.61
13	18.68	18.68
14	18.71	18.71
15	18.73	18.73
16	18.79	18.79
17	18.84	18.84
18	19.02	19.02
19	19.04	19.04
20	19.07	19.07
21	19.11	19.11
22	19.14	19.14
23	19.15	19.15
24	19.17	19.17

Verifica pushover
REAZIONI VINCOLARI

Simbologia

Nodo = Numero del nodo
Rx = Reazione vincolare (forza) in dir. X
CC = Numero della combinazione delle condizioni di carico elementari
Ry = Reazione vincolare (forza) in dir. Y
Rz = Reazione vincolare (forza) in dir. Z
Mx = Reazione vincolare (momento) intorno all'asse X
My = Reazione vincolare (momento) intorno all'asse Y
Mz = Reazione vincolare (momento) intorno all'asse Z

Nodo	Rx <daN>	CC	Ry <daN>	CC	Rz <daN>	CC	Mx <daNm>	CC	My <daNm>	CC	Mz <daNm>	CC
-1680 Max	-944.14	1	618.04	13	0.00	47	0.00	5	0.00	25	39.44	13
-1680 Min.	-1959.04	17	-1613.59	5	0.00	32	0.00	13	0.00	9	-112.65	5
-1679 Max	105.02	9	433.63	13	0.00	5	0.00	5	0.00	18	135.59	13
-1679 Min.	-202.53	1	-1045.18	5	0.00	32	0.00	13	0.00	1	-413.99	5
-1678 Max	-1275.64	1	355.69	19	0.00	22	0.00	13	0.00	32	144.49	13
-1678 Min.	-3150.36	17	-114.33	5	0.00	69	0.00	5	0.00	1	-443.37	5
-1677 Max	-1971.11	1	443.90	19	0.00	1	0.00	5	0.00	9	137.81	13
-1677 Min.	-4705.95	17	39.97	5	0.00	34	0.00	13	0.00	17	-439.12	5
-1676 Max	-2245.64	1	346.19	19	0.00	34	0.00	13	0.00	13	137.36	13
-1676 Min.	-4901.68	17	-50.38	5	0.00	1	0.00	5	0.00	5	-452.44	5
-1675 Max	-2084.16	1	898.78	20	0.00	5	0.00	103	0.00	1	127.52	13
-1675 Min.	-4154.70	17	0.58	13	0.00	13	0.00	20	0.00	9	-424.01	5
-1648 Max	4103.27	5	291.37	5	0.00	35	0.00	19	0.00	1	220.06	13
-1648 Min.	-1470.54	13	-823.82	19	0.00	88	0.00	5	0.00	9	-614.04	5
-1647 Max	-171.81	1	-203.17	1	4925.92	17	-106.12	1	375.42	17	0.19	17
-1647 Min.	-260.98	17	-313.09	17	3254.65	1	-161.35	17	246.71	1	0.12	1
-1646 Max	3.30	17	-23.32	1	5447.99	17	15.33	17	-3.56	1	-0.01	1
-1646 Min.	1.75	1	-36.06	17	3614.53	1	9.89	1	-6.73	17	-0.03	17
-1645 Max	257.99	17	-197.67	1	4804.20	17	-103.44	1	-243.59	1	-0.15	1
-1645 Min.	170.23	1	-302.71	17	3190.21	1	-156.28	17	-369.54	17	-0.23	17
-1644 Max	0.00	1	-149.54	1	0.00	81	0.00	77	0.00	1	0.00	1
-1644 Min.	0.00	1	-221.51	17	0.00	21	0.00	25	0.00	1	0.00	1
-1643 Max	0.00	1	-93.33	1	0.00	17	0.00	1	0.00	1	0.00	1
-1643 Min.	0.00	1	-139.53	17	0.00	1	0.00	17	0.00	1	0.00	1
-1639 Max	1938.90	5	1089.90	5	0.00	32	0.00	5	0.00	9	550.76	13
-1639 Min.	-694.87	13	-347.87	13	0.00	63	0.00	35	0.00	1	-1536.80	5
-1638 Max	-13.04	1	-39.24	1	3948.31	17	2.84	29	-4.95	1	0.68	17
-1638 Min.	-20.34	17	-61.32	17	2611.77	1	2.15	45	-7.70	17	0.46	1
-1637 Max	20.03	17	-38.04	1	3828.42	17	2.74	29	7.13	17	-0.46	1
-1637 Min.	12.87	1	-59.04	17	2548.30	1	2.07	45	4.65	1	-0.68	17
-1636 Max	0.00	1	-57.03	1	0.00	77	0.00	1	0.00	1	0.00	1
-1636 Min.	0.00	1	-85.22	17	0.00	25	0.00	17	0.00	1	0.00	1
-1632 Max	0.00	1	-25.15	1	0.00	21	0.00	77	0.00	1	0.00	1
-1632 Min.	0.00	1	-37.56	17	0.00	53	0.00	25	0.00	1	0.00	1
-1628 Max	0.05	13	1700.01	5	0.00	13	0.00	44	0.00	1	590.77	13
-1628 Min.	-0.13	5	-215.40	13	0.00	36	0.00	13	0.00	9	-1648.44	5
-1627 Max	7.25	17	0.00	1	3924.50	17	0.00	1	0.21	17	0.00	17
-1627 Min.	4.57	1	0.00	17	2596.05	1	0.00	17	0.11	1	0.00	1
-1626 Max	-4.58	1	0.00	45	3805.35	17	0.00	1	-0.37	1	0.00	49
-1626 Min.	-7.26	17	0.00	29	2532.97	1	0.00	17	-0.70	17	0.00	25
-1625 Max	0.00	1	0.00	81	0.00	49	0.00	49	0.00	1	0.00	1
-1625 Min.	0.00	1	0.00	21	0.00	25	0.00	25	0.00	1	0.00	1
-1621 Max	0.00	1	37.56	17	0.00	53	0.00	21	0.00	1	0.00	1
-1621 Min.	0.00	1	25.15	1	0.00	21	0.00	81	0.00	1	0.00	1
-1620 Max	694.98	13	1548.65	5	0.00	5	0.00	13	0.00	1	550.77	13
-1620 Min.	-1939.22	5	-17.22	13	0.00	35	0.00	24	0.00	9	-1536.82	5
-1619 Max	-13.04	1	61.32	17	3948.31	17	-2.15	45	-4.95	1	-0.46	1
-1619 Min.	-20.34	17	39.24	1	2611.77	1	-2.84	29	-7.70	17	-0.68	17
-1618 Max	20.03	17	59.04	17	3828.42	17	-2.07	45	7.13	17	0.68	17
-1618 Min.	12.87	1	38.04	1	2548.30	1	-2.74	29	4.65	1	0.46	1
-1617 Max	0.00	1	85.22	17	0.00	21	0.00	1	0.00	1	0.00	1
-1617 Min.	0.00	1	57.03	1	0.00	81	0.00	17	0.00	1	0.00	1
-1613 Max	0.00	1	139.53	17	0.00	17	0.00	25	0.00	1	0.00	1
-1613 Min.	0.00	1	93.33	1	0.00	1	0.00	49	0.00	1	0.00	1
-1591 Max	1470.62	13	1370.75	5	0.00	20	0.00	13	0.00	1	220.07	13
-1591 Min.	-4103.52	5	237.27	13	0.00	103	0.00	5	0.00	9	-614.06	5

-1590	Max	-171.81	1	313.09	17	4925.92	17	161.35	17	375.42	17	-0.12	1
-1590	Min.	-260.98	17	203.17	1	3254.65	1	106.12	1	246.71	1	-0.19	17
-1589	Max	3.30	17	36.06	17	5447.99	17	-9.89	1	-3.56	1	0.03	17
-1589	Min.	1.75	1	23.32	1	3614.53	1	-15.33	17	-6.73	17	0.01	1
-1588	Max	257.99	17	302.71	17	4804.20	17	156.28	17	-243.59	1	0.23	17
-1588	Min.	170.23	1	197.67	1	3190.21	1	103.44	1	-369.54	17	0.15	1
-1587	Max	0.00	1	221.51	17	0.00	21	0.00	17	0.00	1	0.00	1
-1587	Min.	0.00	1	149.54	1	0.00	25	0.00	1	0.00	1	0.00	1
-850	Max	0.00	1	0.00	1	0.00	13	0.00	17	0.00	9	0.00	1
-850	Min.	0.00	1	0.00	1	0.00	5	0.00	102	0.00	1	0.00	1
-849	Max	0.00	1	0.00	1	0.00	1	0.00	5	0.00	57	0.00	1
-849	Min.	0.00	1	0.00	1	0.00	9	0.00	13	0.00	1	0.00	1
-848	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	5	0.00	1
-848	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	13	0.00	1
-847	Max	0.00	1	0.00	1	0.00	5	0.00	43	0.00	1	0.00	1
-847	Min.	0.00	1	0.00	1	0.00	13	0.00	1	0.00	9	0.00	1
-846	Max	0.00	1	0.00	1	0.00	1	0.00	13	0.00	1	0.00	1
-846	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	9	0.00	1
-845	Max	0.00	1	0.00	1	0.00	5	0.00	21	0.00	39	0.00	1
-845	Min.	0.00	1	0.00	1	0.00	29	0.00	13	0.00	13	0.00	1
-844	Max	0.00	1	0.00	1	0.00	25	0.00	30	0.00	13	0.00	1
-844	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	5	0.00	1
-843	Max	0.00	1	0.00	1	0.00	27	0.00	13	0.00	26	0.00	1
-843	Min.	0.00	1	0.00	1	0.00	1	0.00	5	0.00	1	0.00	1
-842	Max	0.00	1	0.00	1	0.00	20	0.00	9	0.00	5	0.00	1
-842	Min.	0.00	1	0.00	1	0.00	13	0.00	17	0.00	13	0.00	1
-841	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	13	0.00	1
-841	Min.	0.00	1	0.00	1	0.00	13	0.00	23	0.00	5	0.00	1
-840	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	13	0.00	1
-840	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	5	0.00	1
-839	Max	0.00	1	0.00	1	0.00	27	0.00	5	0.00	5	0.00	1
-839	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	13	0.00	1
-838	Max	0.00	1	0.00	1	0.00	19	0.00	13	0.00	13	0.00	1
-838	Min.	0.00	1	0.00	1	0.00	5	0.00	24	0.00	5	0.00	1
-837	Max	0.00	1	0.00	1	0.00	23	0.00	23	0.00	13	0.00	1
-837	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	5	0.00	1
-836	Max	0.00	1	0.00	1	0.00	20	0.00	13	0.00	13	0.00	1
-836	Min.	0.00	1	0.00	1	0.00	13	0.00	24	0.00	5	0.00	1
-835	Max	0.00	1	0.00	1	0.00	49	0.00	5	0.00	5	0.00	1
-835	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	13	0.00	1
-834	Max	0.00	1	0.00	1	0.00	31	0.00	5	0.00	13	0.00	1
-834	Min.	0.00	1	0.00	1	0.00	5	0.00	59	0.00	25	0.00	1
-833	Max	0.00	1	0.00	1	0.00	1	0.00	13	0.00	35	0.00	1
-833	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	13	0.00	1
-832	Max	0.00	1	0.00	1	0.00	34	0.00	5	0.00	13	0.00	1
-832	Min.	0.00	1	0.00	1	0.00	57	0.00	51	0.00	19	0.00	1
-831	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	1	0.00	1
-831	Min.	0.00	1	0.00	1	0.00	19	0.00	31	0.00	9	0.00	1
-830	Max	0.00	1	0.00	1	0.00	19	0.00	5	0.00	50	0.00	1
-830	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	41	0.00	1
-829	Max	0.00	1	0.00	1	0.00	1	0.00	32	0.00	55	0.00	1
-829	Min.	0.00	1	0.00	1	0.00	24	0.00	9	0.00	40	0.00	1
-828	Max	0.00	1	0.00	1	0.00	1	0.00	13	0.00	5	0.00	1
-828	Min.	0.00	1	0.00	1	0.00	18	0.00	5	0.00	25	0.00	1
-827	Max	0.00	1	0.00	1	0.00	24	0.00	1	0.00	9	0.00	1
-827	Min.	0.00	1	0.00	1	0.00	5	0.00	9	0.00	1	0.00	1
-826	Max	0.00	1	0.00	1	0.00	13	0.00	9	0.00	50	0.00	1
-826	Min.	0.00	1	0.00	1	0.00	5	0.00	1	0.00	5	0.00	1
-825	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	13	0.00	1
-825	Min.	0.00	1	0.00	1	0.00	17	0.00	13	0.00	18	0.00	1
-824	Max	0.00	1	0.00	1	0.00	19	0.00	31	0.00	5	0.00	1
-824	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	23	0.00	1
-823	Max	0.00	1	0.00	1	0.00	20	0.00	1	0.00	5	0.00	1
-823	Min.	0.00	1	0.00	1	0.00	9	0.00	26	0.00	26	0.00	1
-822	Max	0.00	1	0.00	1	0.00	19	0.00	19	0.00	13	0.00	1
-822	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	23	0.00	1
-821	Max	0.00	1	0.00	1	0.00	20	0.00	9	0.00	1	0.00	1
-821	Min.	0.00	1	0.00	1	0.00	13	0.00	1	0.00	9	0.00	1
-820	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	22	0.00	1
-820	Min.	0.00	1	0.00	1	0.00	19	0.00	17	0.00	9	0.00	1
-819	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	5	0.00	1
-819	Min.	0.00	1	0.00	1	0.00	27	0.00	5	0.00	13	0.00	1
-818	Max	0.00	1	0.00	1	0.00	5	0.00	27	0.00	13	0.00	1

-818	Min.	0.00	1	0.00	1	0.00	23	0.00	13	0.00	49	0.00	1
-817	Max	0.00	1	0.00	1	0.00	9	0.00	27	0.00	1	0.00	1
-817	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-816	Max	0.00	1	0.00	1	0.00	40	0.00	5	0.00	1	0.00	1
-816	Min.	0.00	1	0.00	1	0.00	9	0.00	13	0.00	9	0.00	1
-815	Max	0.00	1	0.00	1	0.00	1	0.00	5	0.00	9	0.00	1
-815	Min.	0.00	1	0.00	1	0.00	9	0.00	13	0.00	1	0.00	1
-814	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	32	0.00	1
-814	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	5	0.00	1
-813	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	19	0.00	1
-813	Min.	0.00	1	0.00	1	0.00	51	0.00	19	0.00	5	0.00	1
-812	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	13	0.00	1
-812	Min.	0.00	1	0.00	1	0.00	19	0.00	13	0.00	19	0.00	1
-811	Max	0.00	1	0.00	1	0.00	13	0.00	1	0.00	24	0.00	1
-811	Min.	0.00	1	0.00	1	0.00	35	0.00	9	0.00	5	0.00	1
-810	Max	0.00	1	0.00	1	0.00	13	0.00	47	0.00	5	0.00	1
-810	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	13	0.00	1
-809	Max	0.00	1	0.00	1	0.00	9	0.00	17	0.00	1	0.00	1
-809	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-808	Max	0.00	1	0.00	1	0.00	25	0.00	9	0.00	26	0.00	1
-808	Min.	0.00	1	0.00	1	0.00	5	0.00	1	0.00	5	0.00	1
-807	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	9	0.00	1
-807	Min.	0.00	1	0.00	1	0.00	20	0.00	5	0.00	27	0.00	1
-806	Max	0.00	1	0.00	1	0.00	13	0.00	19	0.00	13	0.00	1
-806	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1
-805	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	9	0.00	1
-805	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	1	0.00	1
-804	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1	0.00	1
-804	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	18	0.00	1
-803	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	13	0.00	1
-803	Min.	0.00	1	0.00	1	0.00	13	0.00	30	0.00	19	0.00	1
-802	Max	0.00	1	0.00	1	0.00	5	0.00	1	0.00	9	0.00	1
-802	Min.	0.00	1	0.00	1	0.00	25	0.00	9	0.00	1	0.00	1
-801	Max	0.00	1	0.00	1	0.00	13	0.00	1	0.00	5	0.00	1
-801	Min.	0.00	1	0.00	1	0.00	5	0.00	9	0.00	13	0.00	1
-800	Max	0.00	1	0.00	1	0.00	5	0.00	1	0.00	13	0.00	1
-800	Min.	0.00	1	0.00	1	0.00	33	0.00	9	0.00	17	0.00	1
-799	Max	0.00	1	0.00	1	0.00	33	0.00	18	0.00	18	0.00	1
-799	Min.	0.00	1	0.00	1	0.00	5	0.00	1	0.00	1	0.00	1
-798	Max	0.00	1	0.00	1	0.00	48	0.00	27	0.00	1	0.00	1
-798	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	19	0.00	1
-797	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1
-797	Min.	0.00	1	0.00	1	0.00	23	0.00	19	0.00	13	0.00	1
-796	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	18	0.00	1
-796	Min.	0.00	1	0.00	1	0.00	13	0.00	25	0.00	5	0.00	1
-795	Max	0.00	1	0.00	1	0.00	24	0.00	19	0.00	9	0.00	1
-795	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1	0.00	1
-794	Max	0.00	1	0.00	1	0.00	5	0.00	20	0.00	13	0.00	1
-794	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	5	0.00	1
-793	Max	0.00	1	0.00	1	0.00	9	0.00	37	0.00	9	0.00	1
-793	Min.	0.00	1	0.00	1	0.00	29	0.00	13	0.00	1	0.00	1
-792	Max	0.00	1	0.00	1	0.00	5	0.00	1	0.00	13	0.00	1
-792	Min.	0.00	1	0.00	1	0.00	21	0.00	9	0.00	23	0.00	1
-791	Max	0.00	1	0.00	1	0.00	1	0.00	13	0.00	13	0.00	1
-791	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	5	0.00	1
-790	Max	0.00	1	0.00	1	0.00	13	0.00	36	0.00	22	0.00	1
-790	Min.	0.00	1	0.00	1	0.00	27	0.00	13	0.00	5	0.00	1
-789	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	13	0.00	1
-789	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	5	0.00	1
-788	Max	0.00	1	0.00	1	0.00	9	0.00	13	0.00	5	0.00	1
-788	Min.	0.00	1	0.00	1	0.00	1	0.00	5	0.00	13	0.00	1
-787	Max	0.00	1	0.00	1	0.00	32	0.00	5	0.00	9	0.00	1
-787	Min.	0.00	1	0.00	1	0.00	1	0.00	13	0.00	1	0.00	1
-786	Max	0.00	1	0.00	1	0.00	9	0.00	19	0.00	5	0.00	1
-786	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	13	0.00	1
-785	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	5	0.00	1
-785	Min.	0.00	1	0.00	1	0.00	57	0.00	13	0.00	13	0.00	1
-784	Max	0.00	1	0.00	1	0.00	1	0.00	19	0.00	9	0.00	1
-784	Min.	0.00	1	0.00	1	0.00	9	0.00	13	0.00	1	0.00	1
-783	Max	0.00	1	0.00	1	0.00	20	0.00	57	0.00	13	0.00	1
-783	Min.	0.00	1	0.00	1	0.00	5	0.00	34	0.00	5	0.00	1
-782	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	13	0.00	1
-782	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	5	0.00	1

-781	Max	0.00	1	0.00	1	0.00	19	0.00	18	0.00	1	0.00	1
-781	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	20	0.00	1
-780	Max	0.00	1	0.00	1	0.00	41	0.00	28	0.00	13	0.00	1
-780	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	5	0.00	1
-779	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	9	0.00	1
-779	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	1	0.00	1
-778	Max	0.00	1	0.00	1	0.00	17	0.00	5	0.00	13	0.00	1
-778	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	5	0.00	1
-777	Max	0.00	1	0.00	1	0.00	13	0.00	26	0.00	5	0.00	1
-777	Min.	0.00	1	0.00	1	0.00	5	0.00	1	0.00	13	0.00	1
-776	Max	0.00	1	0.00	1	0.00	1	0.00	26	0.00	18	0.00	1
-776	Min.	0.00	1	0.00	1	0.00	9	0.00	13	0.00	9	0.00	1
-775	Max	0.00	1	0.00	1	0.00	13	0.00	54	0.00	24	0.00	1
-775	Min.	0.00	1	0.00	1	0.00	5	0.00	37	0.00	13	0.00	1
-774	Max	0.00	1	0.00	1	0.00	13	0.00	34	0.00	5	0.00	1
-774	Min.	0.00	1	0.00	1	0.00	5	0.00	9	0.00	13	0.00	1
-773	Max	0.00	1	0.00	1	0.00	13	0.00	9	0.00	1	0.00	1
-773	Min.	0.00	1	0.00	1	0.00	28	0.00	1	0.00	9	0.00	1
-772	Max	0.00	1	0.00	1	0.00	9	0.00	13	0.00	1	0.00	1
-772	Min.	0.00	1	0.00	1	0.00	1	0.00	5	0.00	9	0.00	1
-771	Max	0.00	1	0.00	1	0.00	25	0.00	13	0.00	13	0.00	1
-771	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	25	0.00	1
-770	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	13	0.00	1
-770	Min.	0.00	1	0.00	1	0.00	5	0.00	40	0.00	5	0.00	1
-769	Max	0.00	1	0.00	1	0.00	5	0.00	17	0.00	5	0.00	1
-769	Min.	0.00	1	0.00	1	0.00	13	0.00	5	0.00	13	0.00	1
-768	Max	0.00	1	0.00	1	0.00	13	0.00	9	0.00	1	0.00	1
-768	Min.	0.00	1	0.00	1	0.00	5	0.00	28	0.00	9	0.00	1
-767	Max	0.00	1	0.00	1	0.00	9	0.00	13	0.00	13	0.00	1
-767	Min.	0.00	1	0.00	1	0.00	1	0.00	5	0.00	5	0.00	1
-766	Max	0.00	1	0.00	1	0.00	5	0.00	27	0.00	13	0.00	1
-766	Min.	0.00	1	0.00	1	0.00	44	0.00	13	0.00	18	0.00	1
-765	Max	0.00	1	0.00	1	0.00	29	0.00	20	0.00	1	0.00	1
-765	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	44	0.00	1
-764	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-764	Min.	0.00	1	0.00	1	0.00	25	0.00	18	0.00	1	0.00	1
-763	Max	0.00	1	0.00	1	0.00	13	0.00	1	0.00	5	0.00	1
-763	Min.	0.00	1	0.00	1	0.00	5	0.00	9	0.00	13	0.00	1
-762	Max	0.00	1	0.00	1	0.00	13	0.00	28	0.00	46	0.00	1
-762	Min.	0.00	1	0.00	1	0.00	5	0.00	1	0.00	1	0.00	1
-761	Max	0.00	1	0.00	1	0.00	9	0.00	13	0.00	20	0.00	1
-761	Min.	0.00	1	0.00	1	0.00	19	0.00	5	0.00	5	0.00	1
-760	Max	0.00	1	0.00	1	0.00	9	0.00	5	0.00	9	0.00	1
-760	Min.	0.00	1	0.00	1	0.00	1	0.00	13	0.00	1	0.00	1
-759	Max	0.00	1	0.00	1	0.00	9	0.00	44	0.00	36	0.00	1
-759	Min.	0.00	1	0.00	1	0.00	1	0.00	47	0.00	13	0.00	1
-758	Max	0.00	1	0.00	1	0.00	31	0.00	59	0.00	19	0.00	1
-758	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	13	0.00	1
-757	Max	0.00	1	0.00	1	0.00	5	0.00	39	0.00	24	0.00	1
-757	Min.	0.00	1	0.00	1	0.00	35	0.00	5	0.00	13	0.00	1
-756	Max	0.00	1	0.00	1	0.00	13	0.00	44	0.00	41	0.00	1
-756	Min.	0.00	1	0.00	1	0.00	5	0.00	9	0.00	5	0.00	1
-755	Max	0.00	1	0.00	1	0.00	1	0.00	5	0.00	9	0.00	1
-755	Min.	0.00	1	0.00	1	0.00	9	0.00	20	0.00	20	0.00	1
-754	Max	0.00	1	0.00	1	0.00	13	0.00	1	0.00	1	0.00	1
-754	Min.	0.00	1	0.00	1	0.00	5	0.00	20	0.00	29	0.00	1
-753	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	13	0.00	1
-753	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	29	0.00	1
-752	Max	305.38	13	7715.81	19	0.00	29	0.00	5	0.00	9	782.74	19
-752	Min.	-5177.47	19	-3414.23	13	0.00	9	0.00	19	0.00	1	-306.52	13
-751	Max	763.25	13	2389.85	19	0.00	1	0.00	9	0.00	9	1949.76	19
-751	Min.	-8605.77	19	-1094.00	9	0.00	9	0.00	1	0.00	1	-612.48	13
-750	Max	23.14	13	324.97	13	0.00	29	0.00	17	0.00	13	1960.89	19
-750	Min.	-7914.88	19	-1867.34	19	0.00	13	0.00	1	0.00	26	-586.54	13
-749	Max	379.30	13	541.25	13	0.00	1	0.00	9	0.00	13	1251.36	19
-749	Min.	-9470.19	19	-3292.78	5	0.00	9	0.00	1	0.00	5	-369.30	13
-748	Max	1708.40	1	142.75	13	0.00	1	0.00	5	0.00	1	787.98	19
-748	Min.	-7605.53	19	-1259.46	19	0.00	28	0.00	13	0.00	9	-168.36	13
-747	Max	1244.88	1	412.00	9	0.00	13	0.00	13	0.00	9	572.64	19
-747	Min.	-5383.78	19	-608.20	19	0.00	18	0.00	5	0.00	1	-76.04	13
-746	Max	1194.79	1	474.98	9	0.00	5	0.00	5	0.00	9	369.20	19
-746	Min.	-4034.92	9	-412.32	1	0.00	13	0.00	13	0.00	1	-18.45	13
-745	Max	1249.41	1	412.29	1	0.00	9	0.00	1	0.00	5	213.31	19

-745	Min.	-3414.44	9	-292.32	9	0.00	27	0.00	9	0.00	13	10.33	13
-744	Max	1369.58	1	364.97	1	0.00	9	0.00	5	0.00	13	113.36	19
-744	Min.	-2708.57	9	-222.15	9	0.00	1	0.00	13	0.00	19	20.50	13
-743	Max	1335.95	1	455.08	5	0.00	5	0.00	13	0.00	9	90.72	13
-743	Min.	-1778.60	9	-260.65	13	0.00	13	0.00	24	0.00	1	-35.40	5
-742	Max	1540.00	5	628.04	5	0.00	60	0.00	13	0.00	5	132.41	13
-742	Min.	-983.01	13	-352.04	13	0.00	35	0.00	39	0.00	28	-146.69	5
-741	Max	2605.34	5	888.03	5	0.00	47	0.00	13	0.00	9	196.17	13
-741	Min.	-807.41	13	-471.73	13	0.00	13	0.00	5	0.00	19	-295.17	5
-740	Max	4760.94	1	1099.24	5	0.00	13	0.00	13	0.00	19	278.48	13
-740	Min.	-1872.14	9	-569.90	13	0.00	19	0.00	28	0.00	13	-482.70	5
-739	Max	5582.75	1	991.93	5	0.00	5	0.00	35	0.00	20	265.45	13
-739	Min.	-2132.88	9	-419.81	13	0.00	13	0.00	13	0.00	5	-500.11	5
-738	Max	4604.71	1	631.37	5	0.00	5	0.00	5	0.00	13	211.92	13
-738	Min.	-2247.41	9	-237.58	13	0.00	19	0.00	24	0.00	5	-430.57	5
-737	Max	7216.72	1	835.43	5	0.00	13	0.00	20	0.00	13	317.19	13
-737	Min.	-4225.51	9	-212.44	13	0.00	24	0.00	9	0.00	5	-701.13	5
-736	Max	10902.40	1	785.22	5	0.00	5	0.00	5	0.00	1	413.21	13
-736	Min.	-6271.64	9	-52.27	13	0.00	13	0.00	19	0.00	20	-1016.47	5
-735	Max	11595.00	1	588.46	18	0.00	5	0.00	13	0.00	5	388.48	13
-735	Min.	-7483.59	9	180.42	13	0.00	23	0.00	5	0.00	13	-1106.89	5
-734	Max	11640.40	1	596.05	19	0.00	55	0.00	5	0.00	5	323.44	13
-734	Min.	-7916.68	9	-303.94	5	0.00	40	0.00	19	0.00	13	-1111.41	5
-733	Max	12230.20	1	446.19	13	0.00	26	0.00	5	0.00	1	275.34	13
-733	Min.	-8945.37	9	-685.27	5	0.00	13	0.00	27	0.00	24	-1196.28	5
-732	Max	0.00	1	0.00	1	0.00	5	0.00	1	0.00	9	0.00	1
-732	Min.	0.00	1	0.00	1	0.00	13	0.00	19	0.00	1	0.00	1
-731	Max	8929.19	1	278.11	13	0.00	28	0.00	9	0.00	1	175.04	13
-731	Min.	-6326.72	9	-778.48	5	0.00	13	0.00	1	0.00	9	-901.40	5
-730	Max	5110.43	1	437.10	13	0.00	13	0.00	1	0.00	9	84.33	13
-730	Min.	-4245.77	9	-863.78	5	0.00	5	0.00	9	0.00	23	-596.30	5
-729	Max	4279.81	1	443.20	13	0.00	5	0.00	1	0.00	1	48.47	13
-729	Min.	-3825.28	9	-824.95	5	0.00	13	0.00	9	0.00	9	-601.40	5
-728	Max	1945.09	1	421.87	31	0.00	1	0.00	9	0.00	9	15.84	13
-728	Min.	-2539.92	9	-723.49	5	0.00	9	0.00	1	0.00	1	-493.10	5
-727	Max	1093.43	5	-12.08	1	0.00	1	0.00	9	0.00	9	7.96	13
-727	Min.	-2897.55	13	-1196.12	9	0.00	29	0.00	1	0.00	1	-394.00	5
-726	Max	5351.38	19	294.69	1	0.00	13	0.00	13	0.00	5	68.52	13
-726	Min.	430.81	13	-4591.02	9	0.00	24	0.00	5	0.00	13	-345.55	5
-725	Max	0.00	1	0.00	1	0.00	31	0.00	13	0.00	13	0.00	1
-725	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	32	0.00	1
-724	Max	0.00	1	0.00	1	0.00	13	0.00	28	0.00	5	0.00	1
-724	Min.	0.00	1	0.00	1	0.00	5	0.00	1	0.00	36	0.00	1
-723	Max	0.00	1	0.00	1	0.00	24	0.00	13	0.00	13	0.00	1
-723	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	5	0.00	1
-722	Max	0.00	1	0.00	1	0.00	39	0.00	43	0.00	5	0.00	1
-722	Min.	0.00	1	0.00	1	0.00	48	0.00	52	0.00	13	0.00	1
-721	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	5	0.00	1
-721	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	19	0.00	1
-720	Max	0.00	1	0.00	1	0.00	9	0.00	13	0.00	5	0.00	1
-720	Min.	0.00	1	0.00	1	0.00	1	0.00	5	0.00	13	0.00	1
-719	Max	0.00	1	0.00	1	0.00	9	0.00	5	0.00	9	0.00	1
-719	Min.	0.00	1	0.00	1	0.00	1	0.00	28	0.00	30	0.00	1
-718	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	9	0.00	1
-718	Min.	0.00	1	0.00	1	0.00	5	0.00	28	0.00	1	0.00	1
-717	Max	0.00	1	0.00	1	0.00	20	0.00	60	0.00	5	0.00	1
-717	Min.	0.00	1	0.00	1	0.00	13	0.00	35	0.00	13	0.00	1
-716	Max	0.00	1	0.00	1	0.00	32	0.00	13	0.00	22	0.00	1
-716	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	1	0.00	1
-715	Max	0.00	1	0.00	1	0.00	1	0.00	17	0.00	5	0.00	1
-715	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	13	0.00	1
-714	Max	0.00	1	0.00	1	0.00	13	0.00	32	0.00	5	0.00	1
-714	Min.	0.00	1	0.00	1	0.00	19	0.00	13	0.00	42	0.00	1
-713	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-713	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	24	0.00	1
-712	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	1	0.00	1
-712	Min.	0.00	1	0.00	1	0.00	20	0.00	13	0.00	31	0.00	1
-711	Max	2980.88	19	6279.89	19	0.00	29	0.00	1	0.00	21	10.41	5
-711	Min.	-1026.88	9	-220.65	13	0.00	5	0.00	9	0.00	13	-311.43	19
-710	Max	2772.45	19	8368.01	19	0.00	1	0.00	1	0.00	1	62.53	13
-710	Min.	-823.97	13	-2259.33	5	0.00	9	0.00	9	0.00	9	-290.09	5
-709	Max	0.00	1	0.00	1	0.00	5	0.00	9	0.00	5	0.00	1
-709	Min.	0.00	1	0.00	1	0.00	13	0.00	28	0.00	13	0.00	1

-708	Max	829.92	18	5166.50	23	0.00	1	0.00	5	0.00	1	163.66	13
-708	Min.	248.06	9	-4923.39	13	0.00	9	0.00	13	0.00	9	-402.50	5
-707	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	40	0.00	1
-707	Min.	0.00	1	0.00	1	0.00	27	0.00	43	0.00	55	0.00	1
-706	Max	0.00	1	0.00	1	0.00	27	0.00	13	0.00	28	0.00	1
-706	Min.	0.00	1	0.00	1	0.00	13	0.00	51	0.00	13	0.00	1
-705	Max	0.00	1	0.00	1	0.00	30	0.00	30	0.00	1	0.00	1
-705	Min.	0.00	1	0.00	1	0.00	13	0.00	5	0.00	9	0.00	1
-704	Max	0.00	1	0.00	1	0.00	13	0.00	55	0.00	13	0.00	1
-704	Min.	0.00	1	0.00	1	0.00	19	0.00	13	0.00	5	0.00	1
-703	Max	0.00	1	0.00	1	0.00	35	0.00	13	0.00	27	0.00	1
-703	Min.	0.00	1	0.00	1	0.00	1	0.00	5	0.00	1	0.00	1
-702	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1
-702	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1	0.00	1
-701	Max	0.00	1	0.00	1	0.00	34	0.00	1	0.00	1	0.00	1
-701	Min.	0.00	1	0.00	1	0.00	5	0.00	9	0.00	9	0.00	1
-700	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-700	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-699	Max	0.00	1	0.00	1	0.00	1	0.00	5	0.00	1	0.00	1
-699	Min.	0.00	1	0.00	1	0.00	9	0.00	13	0.00	9	0.00	1
-698	Max	0.00	1	0.00	1	0.00	50	0.00	1	0.00	1	0.00	1
-698	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-697	Max	0.00	1	0.00	1	0.00	23	0.00	9	0.00	21	0.00	1
-697	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	5	0.00	1
-696	Max	0.00	1	0.00	1	0.00	1	0.00	20	0.00	13	0.00	1
-696	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	27	0.00	1
-695	Max	0.00	1	0.00	1	0.00	20	0.00	5	0.00	13	0.00	1
-695	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	23	0.00	1
-694	Max	0.00	1	0.00	1	0.00	5	0.00	28	0.00	13	0.00	1
-694	Min.	0.00	1	0.00	1	0.00	31	0.00	5	0.00	5	0.00	1
-693	Max	0.00	1	0.00	1	0.00	36	0.00	27	0.00	5	0.00	1
-693	Min.	0.00	1	0.00	1	0.00	31	0.00	5	0.00	13	0.00	1
-692	Max	0.00	1	0.00	1	0.00	13	0.00	1	0.00	5	0.00	1
-692	Min.	0.00	1	0.00	1	0.00	5	0.00	18	0.00	31	0.00	1
-691	Max	0.00	1	0.00	1	0.00	13	0.00	9	0.00	33	0.00	1
-691	Min.	0.00	1	0.00	1	0.00	23	0.00	1	0.00	5	0.00	1
-690	Max	0.00	1	0.00	1	0.00	49	0.00	26	0.00	19	0.00	1
-690	Min.	0.00	1	0.00	1	0.00	1	0.00	13	0.00	5	0.00	1
-689	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-689	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-688	Max	0.00	1	0.00	1	0.00	26	0.00	28	0.00	23	0.00	1
-688	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1
-687	Max	0.00	1	0.00	1	0.00	19	0.00	23	0.00	23	0.00	1
-687	Min.	0.00	1	0.00	1	0.00	5	0.00	100	0.00	13	0.00	1
-686	Max	0.00	1	0.00	1	0.00	19	0.00	63	0.00	13	0.00	1
-686	Min.	0.00	1	0.00	1	0.00	13	0.00	32	0.00	31	0.00	1
-685	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-685	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-684	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-684	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-683	Max	0.00	1	0.00	1	0.00	21	0.00	27	0.00	9	0.00	1
-683	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	1	0.00	1
-682	Max	0.00	1	0.00	1	0.00	1	0.00	5	0.00	1	0.00	1
-682	Min.	0.00	1	0.00	1	0.00	23	0.00	20	0.00	1	0.00	1
-681	Max	0.00	1	0.00	1	0.00	5	0.00	19	0.00	28	0.00	1
-681	Min.	0.00	1	0.00	1	0.00	19	0.00	13	0.00	9	0.00	1
-680	Max	0.00	1	0.00	1	0.00	27	0.00	5	0.00	17	0.00	1
-680	Min.	0.00	1	0.00	1	0.00	9	0.00	18	0.00	13	0.00	1
-679	Max	0.00	1	0.00	1	0.00	13	0.00	20	0.00	28	0.00	1
-679	Min.	0.00	1	0.00	1	0.00	27	0.00	5	0.00	13	0.00	1
-678	Max	0.00	1	0.00	1	0.00	9	0.00	5	0.00	9	0.00	1
-678	Min.	0.00	1	0.00	1	0.00	1	0.00	13	0.00	19	0.00	1
-677	Max	0.00	1	0.00	1	0.00	18	0.00	5	0.00	9	0.00	1
-677	Min.	0.00	1	0.00	1	0.00	13	0.00	47	0.00	1	0.00	1
-676	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-676	Min.	0.00	1	0.00	1	0.00	18	0.00	9	0.00	9	0.00	1
-675	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	22	0.00	1
-675	Min.	0.00	1	0.00	1	0.00	5	0.00	43	0.00	9	0.00	1
-674	Max	0.00	1	0.00	1	0.00	18	0.00	9	0.00	1	0.00	1
-674	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	18	0.00	1
-673	Max	0.00	1	0.00	1	0.00	22	0.00	21	0.00	9	0.00	1
-673	Min.	0.00	1	0.00	1	0.00	13	0.00	5	0.00	1	0.00	1
-672	Max	3600.50	19	5662.03	19	0.00	33	0.00	17	0.00	1	107.43	13

-672	Min.	-925.36	13	-247.18	13	0.00	5	0.00	5	0.00	9	-804.41	19
-671	Max	3320.63	19	9008.17	19	0.00	1	0.00	9	0.00	1	132.91	13
-671	Min.	-933.97	13	-3059.27	5	0.00	9	0.00	1	0.00	9	-561.69	5
-670	Max	73.47	9	5309.17	23	0.00	1	0.00	1	0.00	5	176.09	13
-670	Min.	-733.00	1	-6743.50	13	0.00	20	0.00	9	0.00	25	-420.19	5
-669	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-669	Min.	0.00	1	0.00	1	0.00	9	0.00	17	0.00	21	0.00	1
-668	Max	0.00	1	0.00	1	0.00	19	0.00	9	0.00	13	0.00	1
-668	Min.	0.00	1	0.00	1	0.00	1	0.00	20	0.00	28	0.00	1
-667	Max	0.00	1	0.00	1	0.00	64	0.00	24	0.00	13	0.00	1
-667	Min.	0.00	1	0.00	1	0.00	31	0.00	13	0.00	5	0.00	1
-666	Max	0.00	1	0.00	1	0.00	25	0.00	1	0.00	5	0.00	1
-666	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	13	0.00	1
-665	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	13	0.00	1
-665	Min.	0.00	1	0.00	1	0.00	26	0.00	26	0.00	5	0.00	1
-664	Max	0.00	1	0.00	1	0.00	1	0.00	13	0.00	5	0.00	1
-664	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	33	0.00	1
-663	Max	0.00	1	0.00	1	0.00	1	0.00	19	0.00	17	0.00	1
-663	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	5	0.00	1
-662	Max	0.00	1	0.00	1	0.00	19	0.00	13	0.00	5	0.00	1
-662	Min.	0.00	1	0.00	1	0.00	5	0.00	45	0.00	19	0.00	1
-661	Max	0.00	1	0.00	1	0.00	1	0.00	13	0.00	5	0.00	1
-661	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	13	0.00	1
-660	Max	0.00	1	0.00	1	0.00	9	0.00	26	0.00	1	0.00	1
-660	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1
-659	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	13	0.00	1
-659	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	41	0.00	1
-658	Max	0.00	1	0.00	1	0.00	13	0.00	23	0.00	1	0.00	1
-658	Min.	0.00	1	0.00	1	0.00	28	0.00	9	0.00	18	0.00	1
-657	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	17	0.00	1
-657	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1
-656	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-656	Min.	0.00	1	0.00	1	0.00	17	0.00	9	0.00	9	0.00	1
-655	Max	0.00	1	0.00	1	0.00	20	0.00	9	0.00	17	0.00	1
-655	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	13	0.00	1
-654	Max	0.00	1	0.00	1	0.00	9	0.00	25	0.00	1	0.00	1
-654	Min.	0.00	1	0.00	1	0.00	41	0.00	9	0.00	9	0.00	1
-653	Max	0.00	1	0.00	1	0.00	31	0.00	5	0.00	13	0.00	1
-653	Min.	0.00	1	0.00	1	0.00	5	0.00	19	0.00	5	0.00	1
-652	Max	0.00	1	0.00	1	0.00	51	0.00	13	0.00	27	0.00	1
-652	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1
-651	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	5	0.00	1
-651	Min.	0.00	1	0.00	1	0.00	20	0.00	13	0.00	13	0.00	1
-650	Max	0.00	1	0.00	1	0.00	63	0.00	13	0.00	13	0.00	1
-650	Min.	0.00	1	0.00	1	0.00	32	0.00	5	0.00	20	0.00	1
-649	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	13	0.00	1
-649	Min.	0.00	1	0.00	1	0.00	24	0.00	5	0.00	19	0.00	1
-648	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1
-648	Min.	0.00	1	0.00	1	0.00	17	0.00	9	0.00	1	0.00	1
-647	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	20	0.00	1
-647	Min.	0.00	1	0.00	1	0.00	9	0.00	31	0.00	9	0.00	1
-646	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-646	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-645	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	9	0.00	1
-645	Min.	0.00	1	0.00	1	0.00	5	0.00	24	0.00	1	0.00	1
-644	Max	0.00	1	0.00	1	0.00	1	0.00	13	0.00	13	0.00	1
-644	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	31	0.00	1
-643	Max	0.00	1	0.00	1	0.00	40	0.00	13	0.00	5	0.00	1
-643	Min.	0.00	1	0.00	1	0.00	55	0.00	5	0.00	13	0.00	1
-642	Max	3189.17	19	4590.70	19	0.00	9	0.00	9	0.00	5	155.77	13
-642	Min.	-937.46	13	-278.66	13	0.00	33	0.00	1	0.00	13	-1076.12	19
-641	Max	2881.25	19	9481.34	19	0.00	1	0.00	1	0.00	13	160.40	13
-641	Min.	-1061.54	13	-3941.37	5	0.00	9	0.00	9	0.00	19	-637.50	5
-640	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	13	0.00	1
-640	Min.	0.00	1	0.00	1	0.00	18	0.00	5	0.00	30	0.00	1
-639	Max	544.72	9	5248.72	23	0.00	1	0.00	1	0.00	1	139.61	13
-639	Min.	-1211.44	1	-7988.23	13	0.00	9	0.00	19	0.00	19	-344.44	5
-638	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1	0.00	1
-638	Min.	0.00	1	0.00	1	0.00	27	0.00	1	0.00	9	0.00	1
-637	Max	0.00	1	0.00	1	0.00	51	0.00	25	0.00	5	0.00	1
-637	Min.	0.00	1	0.00	1	0.00	5	0.00	9	0.00	13	0.00	1
-636	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	13	0.00	1
-636	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	5	0.00	1

-635	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-635	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-634	Max	0.00	1	0.00	1	0.00	9	0.00	5	0.00	18	0.00	1
-634	Min.	0.00	1	0.00	1	0.00	1	0.00	32	0.00	5	0.00	1
-633	Max	0.00	1	0.00	1	0.00	42	0.00	9	0.00	5	0.00	1
-633	Min.	0.00	1	0.00	1	0.00	5	0.00	1	0.00	13	0.00	1
-632	Max	0.00	1	0.00	1	0.00	34	0.00	13	0.00	5	0.00	1
-632	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	33	0.00	1
-631	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	5	0.00	1
-631	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	21	0.00	1
-630	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	13	0.00	1
-630	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	41	0.00	1
-629	Max	0.00	1	0.00	1	0.00	32	0.00	35	0.00	5	0.00	1
-629	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	13	0.00	1
-628	Max	0.00	1	0.00	1	0.00	33	0.00	9	0.00	9	0.00	1
-628	Min.	0.00	1	0.00	1	0.00	13	0.00	30	0.00	17	0.00	1
-627	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1	0.00	1
-627	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1
-626	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1	0.00	1
-626	Min.	0.00	1	0.00	1	0.00	17	0.00	1	0.00	9	0.00	1
-625	Max	0.00	1	0.00	1	0.00	1	0.00	29	0.00	9	0.00	1
-625	Min.	0.00	1	0.00	1	0.00	17	0.00	9	0.00	1	0.00	1
-624	Max	0.00	1	0.00	1	0.00	1	0.00	13	0.00	60	0.00	1
-624	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	35	0.00	1
-623	Max	0.00	1	0.00	1	0.00	36	0.00	9	0.00	9	0.00	1
-623	Min.	0.00	1	0.00	1	0.00	9	0.00	36	0.00	1	0.00	1
-622	Max	0.00	1	0.00	1	0.00	43	0.00	35	0.00	5	0.00	1
-622	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	13	0.00	1
-621	Max	0.00	1	0.00	1	0.00	13	0.00	19	0.00	13	0.00	1
-621	Min.	0.00	1	0.00	1	0.00	34	0.00	5	0.00	19	0.00	1
-620	Max	0.00	1	0.00	1	0.00	35	0.00	19	0.00	5	0.00	1
-620	Min.	0.00	1	0.00	1	0.00	1	0.00	13	0.00	20	0.00	1
-619	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	1	0.00	1
-619	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	9	0.00	1
-618	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	39	0.00	1
-618	Min.	0.00	1	0.00	1	0.00	19	0.00	5	0.00	13	0.00	1
-617	Max	0.00	1	0.00	1	0.00	1	0.00	5	0.00	26	0.00	1
-617	Min.	0.00	1	0.00	1	0.00	22	0.00	45	0.00	9	0.00	1
-616	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-616	Min.	0.00	1	0.00	1	0.00	17	0.00	1	0.00	17	0.00	1
-615	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-615	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-614	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	29	0.00	1
-614	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1
-613	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	5	0.00	1
-613	Min.	0.00	1	0.00	1	0.00	30	0.00	9	0.00	21	0.00	1
-612	Max	0.00	1	0.00	1	0.00	34	0.00	1	0.00	5	0.00	1
-612	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	13	0.00	1
-611	Max	0.00	1	0.00	1	0.00	31	0.00	20	0.00	5	0.00	1
-611	Min.	0.00	1	0.00	1	0.00	13	0.00	5	0.00	24	0.00	1
-610	Max	2878.21	19	3559.16	19	0.00	9	0.00	1	0.00	1	131.44	9
-610	Min.	-1074.63	13	-213.36	13	0.00	1	0.00	9	0.00	9	-1137.72	19
-609	Max	2645.42	19	8895.48	19	0.00	1	0.00	13	0.00	13	148.87	13
-609	Min.	-1618.10	13	-4346.29	5	0.00	9	0.00	17	0.00	25	-528.02	5
-608	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	26	0.00	1
-608	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-607	Max	1480.16	23	4851.53	23	0.00	19	0.00	9	0.00	9	125.94	13
-607	Min.	-1670.79	9	-8399.28	13	0.00	1	0.00	1	0.00	46	-253.89	5
-606	Max	0.00	1	0.00	1	0.00	30	0.00	1	0.00	1	0.00	1
-606	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-605	Max	0.00	1	0.00	1	0.00	1	0.00	17	0.00	1	0.00	1
-605	Min.	0.00	1	0.00	1	0.00	23	0.00	13	0.00	9	0.00	1
-604	Max	0.00	1	0.00	1	0.00	43	0.00	28	0.00	48	0.00	1
-604	Min.	0.00	1	0.00	1	0.00	13	0.00	5	0.00	1	0.00	1
-603	Max	0.00	1	0.00	1	0.00	18	0.00	5	0.00	9	0.00	1
-603	Min.	0.00	1	0.00	1	0.00	9	0.00	31	0.00	1	0.00	1
-602	Max	0.00	1	0.00	1	0.00	5	0.00	31	0.00	5	0.00	1
-602	Min.	0.00	1	0.00	1	0.00	35	0.00	13	0.00	13	0.00	1
-601	Max	0.00	1	0.00	1	0.00	9	0.00	13	0.00	25	0.00	1
-601	Min.	0.00	1	0.00	1	0.00	38	0.00	32	0.00	13	0.00	1
-600	Max	0.00	1	0.00	1	0.00	1	0.00	36	0.00	32	0.00	1
-600	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	1	0.00	1
-599	Max	0.00	1	0.00	1	0.00	20	0.00	43	0.00	5	0.00	1

-599	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	13	0.00	1
-598	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-598	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-597	Max	0.00	1	0.00	1	0.00	40	0.00	24	0.00	9	0.00	1
-597	Min.	0.00	1	0.00	1	0.00	55	0.00	13	0.00	1	0.00	1
-596	Max	0.00	1	0.00	1	0.00	19	0.00	17	0.00	13	0.00	1
-596	Min.	0.00	1	0.00	1	0.00	5	0.00	1	0.00	19	0.00	1
-595	Max	0.00	1	0.00	1	0.00	9	0.00	34	0.00	19	0.00	1
-595	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	13	0.00	1
-594	Max	0.00	1	0.00	1	0.00	9	0.00	49	0.00	13	0.00	1
-594	Min.	0.00	1	0.00	1	0.00	1	0.00	42	0.00	42	0.00	1
-593	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	5	0.00	1
-593	Min.	0.00	1	0.00	1	0.00	5	0.00	23	0.00	13	0.00	1
-592	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	20	0.00	1
-592	Min.	0.00	1	0.00	1	0.00	20	0.00	19	0.00	13	0.00	1
-591	Max	0.00	1	0.00	1	0.00	44	0.00	19	0.00	19	0.00	1
-591	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	13	0.00	1
-590	Max	0.00	1	0.00	1	0.00	13	0.00	41	0.00	5	0.00	1
-590	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	13	0.00	1
-589	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	23	0.00	1
-589	Min.	0.00	1	0.00	1	0.00	43	0.00	27	0.00	5	0.00	1
-588	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	19	0.00	1
-588	Min.	0.00	1	0.00	1	0.00	55	0.00	26	0.00	13	0.00	1
-587	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-587	Min.	0.00	1	0.00	1	0.00	24	0.00	18	0.00	21	0.00	1
-586	Max	0.00	1	0.00	1	0.00	24	0.00	9	0.00	5	0.00	1
-586	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	18	0.00	1
-585	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1
-585	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	32	0.00	1
-584	Max	0.00	1	0.00	1	0.00	29	0.00	25	0.00	25	0.00	1
-584	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-583	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	41	0.00	1
-583	Min.	0.00	1	0.00	1	0.00	33	0.00	53	0.00	9	0.00	1
-582	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-582	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-581	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-581	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-580	Max	0.00	1	0.00	1	0.00	9	0.00	5	0.00	17	0.00	1
-580	Min.	0.00	1	0.00	1	0.00	1	0.00	18	0.00	13	0.00	1
-579	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-579	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-578	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-578	Min.	0.00	1	0.00	1	0.00	21	0.00	1	0.00	1	0.00	1
-577	Max	0.00	1	0.00	1	0.00	9	0.00	5	0.00	5	0.00	1
-577	Min.	0.00	1	0.00	1	0.00	23	0.00	30	0.00	13	0.00	1
-576	Max	0.00	1	0.00	1	0.00	13	0.00	9	0.00	9	0.00	1
-576	Min.	0.00	1	0.00	1	0.00	18	0.00	1	0.00	29	0.00	1
-575	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	21	0.00	1
-575	Min.	0.00	1	0.00	1	0.00	38	0.00	9	0.00	42	0.00	1
-574	Max	0.00	1	0.00	1	0.00	19	0.00	13	0.00	1	0.00	1
-574	Min.	0.00	1	0.00	1	0.00	13	0.00	5	0.00	17	0.00	1
-573	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	1	0.00	1
-573	Min.	0.00	1	0.00	1	0.00	20	0.00	5	0.00	18	0.00	1
-572	Max	0.00	1	0.00	1	0.00	43	0.00	5	0.00	13	0.00	1
-572	Min.	0.00	1	0.00	1	0.00	13	0.00	23	0.00	5	0.00	1
-571	Max	0.00	1	0.00	1	0.00	9	0.00	13	0.00	1	0.00	1
-571	Min.	0.00	1	0.00	1	0.00	1	0.00	5	0.00	9	0.00	1
-570	Max	0.00	1	0.00	1	0.00	13	0.00	1	0.00	5	0.00	1
-570	Min.	0.00	1	0.00	1	0.00	17	0.00	9	0.00	13	0.00	1
-569	Max	0.00	1	0.00	1	0.00	1	0.00	25	0.00	9	0.00	1
-569	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	1	0.00	1
-568	Max	0.00	1	0.00	1	0.00	5	0.00	47	0.00	13	0.00	1
-568	Min.	0.00	1	0.00	1	0.00	19	0.00	5	0.00	35	0.00	1
-567	Max	2710.62	19	2336.75	1	0.00	9	0.00	9	0.00	5	50.39	9
-567	Min.	-1259.40	13	-368.69	9	0.00	1	0.00	1	0.00	13	-1064.54	19
-566	Max	7374.17	19	11054.40	19	0.00	1	0.00	9	0.00	34	167.61	13
-566	Min.	-4492.36	13	-5773.23	13	0.00	9	0.00	1	0.00	13	-375.84	5
-565	Max	0.00	1	0.00	1	0.00	5	0.00	61	0.00	9	0.00	1
-565	Min.	0.00	1	0.00	1	0.00	25	0.00	30	0.00	1	0.00	1
-564	Max	2085.94	19	4237.25	23	0.00	9	0.00	1	0.00	1	200.34	13
-564	Min.	-950.15	9	-7938.20	13	0.00	1	0.00	9	0.00	9	-223.04	5
-563	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-563	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1

-562	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-562	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	37	0.00	1
-561	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1
-561	Min.	0.00	1	0.00	1	0.00	13	0.00	47	0.00	13	0.00	1
-560	Max	0.00	1	0.00	1	0.00	18	0.00	1	0.00	23	0.00	1
-560	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-559	Max	0.00	1	0.00	1	0.00	35	0.00	32	0.00	5	0.00	1
-559	Min.	0.00	1	0.00	1	0.00	5	0.00	1	0.00	23	0.00	1
-558	Max	0.00	1	0.00	1	0.00	30	0.00	5	0.00	25	0.00	1
-558	Min.	0.00	1	0.00	1	0.00	9	0.00	13	0.00	1	0.00	1
-557	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-557	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-556	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	13	0.00	1
-556	Min.	0.00	1	0.00	1	0.00	13	0.00	5	0.00	5	0.00	1
-555	Max	0.00	1	0.00	1	0.00	40	0.00	13	0.00	28	0.00	1
-555	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	13	0.00	1
-554	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	20	0.00	1
-554	Min.	0.00	1	0.00	1	0.00	19	0.00	27	0.00	5	0.00	1
-553	Max	0.00	1	0.00	1	0.00	1	0.00	54	0.00	5	0.00	1
-553	Min.	0.00	1	0.00	1	0.00	9	0.00	37	0.00	13	0.00	1
-552	Max	0.00	1	0.00	1	0.00	34	0.00	1	0.00	1	0.00	1
-552	Min.	0.00	1	0.00	1	0.00	13	0.00	9	0.00	9	0.00	1
-551	Max	0.00	1	0.00	1	0.00	18	0.00	1	0.00	9	0.00	1
-551	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1	0.00	1
-550	Max	0.00	1	0.00	1	0.00	34	0.00	1	0.00	9	0.00	1
-550	Min.	0.00	1	0.00	1	0.00	5	0.00	9	0.00	36	0.00	1
-549	Max	0.00	1	0.00	1	0.00	1	0.00	33	0.00	28	0.00	1
-549	Min.	0.00	1	0.00	1	0.00	42	0.00	1	0.00	13	0.00	1
-548	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-548	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-547	Max	0.00	1	0.00	1	0.00	1	0.00	13	0.00	13	0.00	1
-547	Min.	0.00	1	0.00	1	0.00	9	0.00	32	0.00	17	0.00	1
-546	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	24	0.00	1
-546	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	5	0.00	1
-545	Max	0.00	1	0.00	1	0.00	5	0.00	9	0.00	17	0.00	1
-545	Min.	0.00	1	0.00	1	0.00	13	0.00	1	0.00	13	0.00	1
-544	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-544	Min.	0.00	1	0.00	1	0.00	18	0.00	1	0.00	1	0.00	1
-543	Max	0.00	1	0.00	1	0.00	1	0.00	5	0.00	20	0.00	1
-543	Min.	0.00	1	0.00	1	0.00	9	0.00	42	0.00	13	0.00	1
-542	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	1	0.00	1
-542	Min.	0.00	1	0.00	1	0.00	35	0.00	20	0.00	9	0.00	1
-541	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-541	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-540	Max	0.00	1	0.00	1	0.00	1	0.00	17	0.00	9	0.00	1
-540	Min.	0.00	1	0.00	1	0.00	52	0.00	1	0.00	1	0.00	1
-539	Max	0.00	1	0.00	1	0.00	1	0.00	5	0.00	13	0.00	1
-539	Min.	0.00	1	0.00	1	0.00	9	0.00	33	0.00	5	0.00	1
-538	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-538	Min.	0.00	1	0.00	1	0.00	17	0.00	9	0.00	9	0.00	1
-537	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	34	0.00	1
-537	Min.	0.00	1	0.00	1	0.00	43	0.00	56	0.00	1	0.00	1
-536	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	5	0.00	1
-536	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	13	0.00	1
-535	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	25	0.00	1
-535	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-534	Max	0.00	1	0.00	1	0.00	35	0.00	5	0.00	5	0.00	1
-534	Min.	0.00	1	0.00	1	0.00	1	0.00	25	0.00	27	0.00	1
-533	Max	0.00	1	0.00	1	0.00	9	0.00	42	0.00	35	0.00	1
-533	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	5	0.00	1
-532	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	13	0.00	1
-532	Min.	0.00	1	0.00	1	0.00	26	0.00	13	0.00	5	0.00	1
-531	Max	3044.12	19	2762.70	9	0.00	1	0.00	1	0.00	9	-85.08	1
-531	Min.	-1488.71	13	-1539.56	1	0.00	18	0.00	9	0.00	1	-920.45	19
-530	Max	25144.00	19	15155.30	9	0.00	1	0.00	9	0.00	1	312.97	13
-530	Min.	-11830.80	13	-14342.80	1	0.00	9	0.00	1	0.00	9	-226.05	5
-529	Max	5621.85	9	5352.21	9	0.00	9	0.00	20	0.00	1	529.13	13
-529	Min.	-4789.15	1	-3718.77	1	0.00	1	0.00	9	0.00	9	-131.74	5
-528	Max	3696.29	9	1257.59	9	0.00	1	0.00	1	0.00	42	485.48	13
-528	Min.	-3168.68	1	106.55	1	0.00	9	0.00	9	0.00	1	-77.63	5
-527	Max	3268.22	9	772.03	9	0.00	9	0.00	13	0.00	9	388.25	13
-527	Min.	-3400.38	1	171.96	1	0.00	1	0.00	5	0.00	1	-5.33	5
-526	Max	2593.89	9	588.25	5	0.00	1	0.00	50	0.00	1	354.05	13

-526	Min.	-3144.58	1	163.99	13	0.00	41	0.00	41	0.00	9	-6.26	5
-525	Max	2189.66	9	526.45	5	0.00	17	0.00	5	0.00	9	334.03	13
-525	Min.	-2909.84	1	143.26	13	0.00	1	0.00	13	0.00	1	-29.15	5
-524	Max	2010.38	1	558.68	5	0.00	33	0.00	20	0.00	1	325.27	13
-524	Min.	-2736.81	19	136.66	13	0.00	9	0.00	5	0.00	9	-69.78	5
-523	Max	2147.56	1	685.68	5	0.00	37	0.00	5	0.00	21	322.98	13
-523	Min.	-2539.15	27	132.36	13	0.00	5	0.00	13	0.00	9	-128.23	5
-522	Max	2658.77	5	576.79	5	0.00	18	0.00	5	0.00	32	338.62	13
-522	Min.	-2068.25	13	21.09	13	0.00	9	0.00	13	0.00	5	-173.39	5
-521	Max	1556.70	13	700.88	5	0.00	13	0.00	5	0.00	13	295.62	13
-521	Min.	-5.33	5	174.40	13	0.00	39	0.00	22	0.00	5	-157.41	5
-520	Max	2059.31	13	838.13	5	0.00	5	0.00	5	0.00	13	242.49	13
-520	Min.	494.64	5	-34.11	13	0.00	43	0.00	24	0.00	5	-103.37	5
-519	Max	27041.90	13	726.41	5	0.00	5	0.00	43	0.00	27	180.55	13
-519	Min.	-27003.70	5	-158.68	13	0.00	13	0.00	13	0.00	5	-2.14	5
-518	Max	-1490.21	13	1416.75	13	0.00	18	0.00	38	0.00	25	-94.06	13
-518	Min.	-51777.40	5	-479.21	5	0.00	9	0.00	9	0.00	5	-506.65	5
-517	Max	3289.90	5	2265.33	13	0.00	5	0.00	1	0.00	42	-144.81	13
-517	Min.	-2008.40	13	-399.60	5	0.00	18	0.00	9	0.00	9	-731.17	5
-516	Max	1992.09	5	2739.55	1	0.00	1	0.00	17	0.00	22	-153.28	13
-516	Min.	-1245.31	13	-304.40	9	0.00	9	0.00	13	0.00	13	-666.24	5
-515	Max	5090.98	5	3891.89	1	0.00	9	0.00	27	0.00	9	-188.63	13
-515	Min.	-759.61	13	-384.63	9	0.00	1	0.00	13	0.00	1	-632.13	5
-514	Max	4877.40	5	6984.68	1	0.00	1	0.00	1	0.00	9	-126.72	13
-514	Min.	-1448.34	31	-280.26	9	0.00	9	0.00	9	0.00	1	-626.17	17
-513	Max	6631.35	1	12999.10	1	0.00	1	0.00	13	0.00	1	731.62	9
-513	Min.	175.37	9	611.69	9	0.00	9	0.00	26	0.00	18	-868.36	23
-512	Max	7210.10	1	5718.05	1	0.00	1	0.00	17	0.00	9	1471.60	9
-512	Min.	1554.61	9	-80.26	9	0.00	9	0.00	5	0.00	1	-1004.43	23
-511	Max	6595.86	18	1570.01	17	0.00	9	0.00	52	0.00	9	1568.31	1
-511	Min.	2092.28	9	378.35	13	0.00	1	0.00	43	0.00	33	-1013.61	23
-510	Max	4961.26	19	4748.23	19	0.00	1	0.00	1	0.00	5	1265.69	5
-510	Min.	-106.48	5	-2043.45	5	0.00	9	0.00	19	0.00	25	-500.48	31
-509	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	28	0.00	1
-509	Min.	0.00	1	0.00	1	0.00	9	0.00	18	0.00	5	0.00	1
-508	Max	0.00	1	0.00	1	0.00	21	0.00	26	0.00	22	0.00	1
-508	Min.	0.00	1	0.00	1	0.00	13	0.00	9	0.00	13	0.00	1
-507	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1	0.00	1
-507	Min.	0.00	1	0.00	1	0.00	38	0.00	25	0.00	9	0.00	1
-506	Max	0.00	1	0.00	1	0.00	9	0.00	13	0.00	9	0.00	1
-506	Min.	0.00	1	0.00	1	0.00	1	0.00	17	0.00	1	0.00	1
-505	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	18	0.00	1
-505	Min.	0.00	1	0.00	1	0.00	17	0.00	1	0.00	5	0.00	1
-504	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-504	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-503	Max	0.00	1	0.00	1	0.00	1	0.00	13	0.00	25	0.00	1
-503	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	5	0.00	1
-502	Max	0.00	1	0.00	1	0.00	5	0.00	9	0.00	9	0.00	1
-502	Min.	0.00	1	0.00	1	0.00	18	0.00	19	0.00	1	0.00	1
-501	Max	0.00	1	0.00	1	0.00	13	0.00	1	0.00	9	0.00	1
-501	Min.	0.00	1	0.00	1	0.00	26	0.00	43	0.00	20	0.00	1
-500	Max	0.00	1	0.00	1	0.00	26	0.00	1	0.00	9	0.00	1
-500	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-499	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	19	0.00	1
-499	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	13	0.00	1
-498	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	13	0.00	1
-498	Min.	0.00	1	0.00	1	0.00	43	0.00	5	0.00	20	0.00	1
-497	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	30	0.00	1
-497	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	13	0.00	1
-496	Max	0.00	1	0.00	1	0.00	1	0.00	13	0.00	29	0.00	1
-496	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	62	0.00	1
-495	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-495	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-494	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	41	0.00	1
-494	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	5	0.00	1
-493	Max	0.00	1	0.00	1	0.00	23	0.00	35	0.00	5	0.00	1
-493	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	23	0.00	1
-492	Max	0.00	1	0.00	1	0.00	30	0.00	18	0.00	21	0.00	1
-492	Min.	0.00	1	0.00	1	0.00	61	0.00	1	0.00	5	0.00	1
-491	Max	0.00	1	0.00	1	0.00	13	0.00	33	0.00	19	0.00	1
-491	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	9	0.00	1
-490	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	5	0.00	1
-490	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	34	0.00	1

-489	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-489	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-488	Max	0.00	1	0.00	1	0.00	17	0.00	9	0.00	22	0.00	1
-488	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	5	0.00	1
-487	Max	0.00	1	0.00	1	0.00	26	0.00	9	0.00	1	0.00	1
-487	Min.	0.00	1	0.00	1	0.00	9	0.00	34	0.00	9	0.00	1
-486	Max	0.00	1	0.00	1	0.00	9	0.00	33	0.00	1	0.00	1
-486	Min.	0.00	1	0.00	1	0.00	1	0.00	5	0.00	27	0.00	1
-485	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	13	0.00	1
-485	Min.	0.00	1	0.00	1	0.00	27	0.00	19	0.00	5	0.00	1
-484	Max	0.00	1	0.00	1	0.00	9	0.00	38	0.00	1	0.00	1
-484	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-483	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-483	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-482	Max	0.00	1	0.00	1	0.00	38	0.00	17	0.00	9	0.00	1
-482	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1	0.00	1
-481	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-481	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-480	Max	0.00	1	0.00	1	0.00	9	0.00	5	0.00	9	0.00	1
-480	Min.	0.00	1	0.00	1	0.00	1	0.00	17	0.00	1	0.00	1
-479	Max	0.00	1	0.00	1	0.00	18	0.00	13	0.00	9	0.00	1
-479	Min.	0.00	1	0.00	1	0.00	1	0.00	33	0.00	1	0.00	1
-478	Max	0.00	1	0.00	1	0.00	9	0.00	5	0.00	9	0.00	1
-478	Min.	0.00	1	0.00	1	0.00	25	0.00	13	0.00	1	0.00	1
-477	Max	0.00	1	0.00	1	0.00	9	0.00	34	0.00	9	0.00	1
-477	Min.	0.00	1	0.00	1	0.00	25	0.00	1	0.00	1	0.00	1
-476	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	21	0.00	1
-476	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-475	Max	0.00	1	0.00	1	0.00	42	0.00	13	0.00	9	0.00	1
-475	Min.	0.00	1	0.00	1	0.00	9	0.00	38	0.00	1	0.00	1
-474	Max	0.00	1	0.00	1	0.00	17	0.00	1	0.00	9	0.00	1
-474	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	40	0.00	1
-473	Max	2475.71	19	3448.75	9	0.00	1	0.00	1	0.00	9	-185.03	1
-473	Min.	-1162.98	13	-2642.39	1	0.00	9	0.00	9	0.00	1	-669.83	19
-472	Max	3409.56	9	7780.47	9	0.00	39	0.00	1	0.00	9	1104.15	5
-472	Min.	-2144.80	1	38.97	1	0.00	48	0.00	9	0.00	1	-18.27	13
-471	Max	0.00	1	0.00	1	0.00	5	0.00	9	0.00	9	0.00	1
-471	Min.	0.00	1	0.00	1	0.00	38	0.00	17	0.00	1	0.00	1
-470	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	5	0.00	1
-470	Min.	0.00	1	0.00	1	0.00	19	0.00	5	0.00	13	0.00	1
-469	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-469	Min.	0.00	1	0.00	1	0.00	36	0.00	9	0.00	18	0.00	1
-468	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	5	0.00	1
-468	Min.	0.00	1	0.00	1	0.00	26	0.00	13	0.00	13	0.00	1
-467	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	1	0.00	1
-467	Min.	0.00	1	0.00	1	0.00	13	0.00	36	0.00	9	0.00	1
-466	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1
-466	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1	0.00	1
-465	Max	0.00	1	0.00	1	0.00	9	0.00	28	0.00	13	0.00	1
-465	Min.	0.00	1	0.00	1	0.00	33	0.00	13	0.00	5	0.00	1
-464	Max	0.00	1	0.00	1	0.00	13	0.00	24	0.00	13	0.00	1
-464	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	5	0.00	1
-463	Max	0.00	1	0.00	1	0.00	37	0.00	13	0.00	18	0.00	1
-463	Min.	0.00	1	0.00	1	0.00	9	0.00	26	0.00	1	0.00	1
-462	Max	0.00	1	0.00	1	0.00	9	0.00	38	0.00	13	0.00	1
-462	Min.	0.00	1	0.00	1	0.00	1	0.00	53	0.00	25	0.00	1
-461	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-461	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-460	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-460	Min.	0.00	1	0.00	1	0.00	1	0.00	18	0.00	1	0.00	1
-459	Max	0.00	1	0.00	1	0.00	26	0.00	24	0.00	13	0.00	1
-459	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	33	0.00	1
-458	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1
-458	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	19	0.00	1
-457	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	34	0.00	1
-457	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-456	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	13	0.00	1
-456	Min.	0.00	1	0.00	1	0.00	32	0.00	13	0.00	28	0.00	1
-455	Max	0.00	1	0.00	1	0.00	61	0.00	9	0.00	1	0.00	1
-455	Min.	0.00	1	0.00	1	0.00	30	0.00	1	0.00	9	0.00	1
-454	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	1	0.00	1
-454	Min.	0.00	1	0.00	1	0.00	17	0.00	5	0.00	9	0.00	1
-453	Max	0.00	1	0.00	1	0.00	27	0.00	13	0.00	13	0.00	1

-453	Min.	0.00	1	0.00	1	0.00	13	0.00	5	0.00	5	0.00	1
-452	Max	0.00	1	0.00	1	0.00	13	0.00	25	0.00	13	0.00	1
-452	Min.	0.00	1	0.00	1	0.00	5	0.00	1	0.00	5	0.00	1
-451	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-451	Min.	0.00	1	0.00	1	0.00	18	0.00	33	0.00	1	0.00	1
-450	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	13	0.00	1
-450	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	21	0.00	1
-449	Max	0.00	1	0.00	1	0.00	9	0.00	17	0.00	22	0.00	1
-449	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-448	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	13	0.00	1
-448	Min.	0.00	1	0.00	1	0.00	18	0.00	9	0.00	42	0.00	1
-447	Max	0.00	1	0.00	1	0.00	9	0.00	5	0.00	1	0.00	1
-447	Min.	0.00	1	0.00	1	0.00	1	0.00	21	0.00	26	0.00	1
-446	Max	0.00	1	0.00	1	0.00	28	0.00	13	0.00	13	0.00	1
-446	Min.	0.00	1	0.00	1	0.00	5	0.00	17	0.00	5	0.00	1
-445	Max	0.00	1	0.00	1	0.00	1	0.00	13	0.00	13	0.00	1
-445	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	5	0.00	1
-444	Max	0.00	1	0.00	1	0.00	5	0.00	9	0.00	21	0.00	1
-444	Min.	0.00	1	0.00	1	0.00	17	0.00	1	0.00	9	0.00	1
-443	Max	0.00	1	0.00	1	0.00	13	0.00	9	0.00	9	0.00	1
-443	Min.	0.00	1	0.00	1	0.00	42	0.00	1	0.00	1	0.00	1
-442	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	26	0.00	1
-442	Min.	0.00	1	0.00	1	0.00	13	0.00	5	0.00	5	0.00	1
-441	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	13	0.00	1
-441	Min.	0.00	1	0.00	1	0.00	19	0.00	13	0.00	5	0.00	1
-440	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	18	0.00	1
-440	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-439	Max	0.00	1	0.00	1	0.00	1	0.00	21	0.00	1	0.00	1
-439	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-438	Max	0.00	1	0.00	1	0.00	13	0.00	47	0.00	1	0.00	1
-438	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	9	0.00	1
-437	Max	0.00	1	0.00	1	0.00	1	0.00	17	0.00	9	0.00	1
-437	Min.	0.00	1	0.00	1	0.00	9	0.00	13	0.00	1	0.00	1
-436	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1	0.00	1
-436	Min.	0.00	1	0.00	1	0.00	18	0.00	34	0.00	9	0.00	1
-435	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	22	0.00	1
-435	Min.	0.00	1	0.00	1	0.00	39	0.00	1	0.00	13	0.00	1
-434	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	13	0.00	1
-434	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	19	0.00	1
-433	Max	0.00	1	0.00	1	0.00	36	0.00	56	0.00	5	0.00	1
-433	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	13	0.00	1
-432	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	13	0.00	1
-432	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1
-431	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-431	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-430	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-430	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-429	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-429	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-428	Max	0.00	1	0.00	1	0.00	5	0.00	1	0.00	41	0.00	1
-428	Min.	0.00	1	0.00	1	0.00	33	0.00	25	0.00	13	0.00	1
-427	Max	0.00	1	0.00	1	0.00	41	0.00	9	0.00	1	0.00	1
-427	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1
-426	Max	0.00	1	0.00	1	0.00	9	0.00	26	0.00	1	0.00	1
-426	Min.	0.00	1	0.00	1	0.00	33	0.00	1	0.00	9	0.00	1
-425	Max	0.00	1	0.00	1	0.00	38	0.00	9	0.00	9	0.00	1
-425	Min.	0.00	1	0.00	1	0.00	53	0.00	34	0.00	1	0.00	1
-424	Max	0.00	1	0.00	1	0.00	41	0.00	9	0.00	9	0.00	1
-424	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-423	Max	1683.20	19	3618.77	9	0.00	9	0.00	1	0.00	9	-53.05	5
-423	Min.	-579.47	13	-3700.13	1	0.00	1	0.00	9	0.00	1	-520.34	13
-422	Max	2928.49	9	9026.00	9	0.00	5	0.00	9	0.00	1	1029.14	5
-422	Min.	-2350.19	23	-936.27	1	0.00	46	0.00	1	0.00	9	134.53	13
-421	Max	0.00	1	0.00	1	0.00	35	0.00	5	0.00	5	0.00	1
-421	Min.	0.00	1	0.00	1	0.00	13	0.00	43	0.00	13	0.00	1
-420	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	13	0.00	1
-420	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	5	0.00	1
-419	Max	0.00	1	0.00	1	0.00	9	0.00	34	0.00	43	0.00	1
-419	Min.	0.00	1	0.00	1	0.00	37	0.00	9	0.00	1	0.00	1
-418	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-418	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-417	Max	0.00	1	0.00	1	0.00	61	0.00	9	0.00	9	0.00	1
-417	Min.	0.00	1	0.00	1	0.00	30	0.00	1	0.00	1	0.00	1

-416	Max	0.00	1	0.00	1	0.00	13	0.00	19	0.00	13	0.00	1
-416	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1
-415	Max	0.00	1	0.00	1	0.00	13	0.00	26	0.00	13	0.00	1
-415	Min.	0.00	1	0.00	1	0.00	35	0.00	5	0.00	5	0.00	1
-414	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	5	0.00	1
-414	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	13	0.00	1
-413	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-413	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	17	0.00	1
-412	Max	0.00	1	0.00	1	0.00	33	0.00	1	0.00	9	0.00	1
-412	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1	0.00	1
-411	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	5	0.00	1
-411	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	13	0.00	1
-410	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	5	0.00	1
-410	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	40	0.00	1
-409	Max	0.00	1	0.00	1	0.00	41	0.00	1	0.00	9	0.00	1
-409	Min.	0.00	1	0.00	1	0.00	13	0.00	9	0.00	1	0.00	1
-408	Max	0.00	1	0.00	1	0.00	13	0.00	9	0.00	29	0.00	1
-408	Min.	0.00	1	0.00	1	0.00	33	0.00	1	0.00	1	0.00	1
-407	Max	0.00	1	0.00	1	0.00	38	0.00	1	0.00	42	0.00	1
-407	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-406	Max	0.00	1	0.00	1	0.00	44	0.00	13	0.00	5	0.00	1
-406	Min.	0.00	1	0.00	1	0.00	5	0.00	18	0.00	13	0.00	1
-405	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	13	0.00	1
-405	Min.	0.00	1	0.00	1	0.00	19	0.00	1	0.00	33	0.00	1
-404	Max	0.00	1	0.00	1	0.00	1	0.00	32	0.00	1	0.00	1
-404	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-403	Max	0.00	1	0.00	1	0.00	17	0.00	21	0.00	27	0.00	1
-403	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	5	0.00	1
-402	Max	0.00	1	0.00	1	0.00	26	0.00	5	0.00	13	0.00	1
-402	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	5	0.00	1
-401	Max	0.00	1	0.00	1	0.00	33	0.00	9	0.00	1	0.00	1
-401	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	21	0.00	1
-400	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	18	0.00	1
-400	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-399	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	5	0.00	1
-399	Min.	0.00	1	0.00	1	0.00	41	0.00	1	0.00	22	0.00	1
-398	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-398	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	37	0.00	1
-397	Max	0.00	1	0.00	1	0.00	17	0.00	5	0.00	37	0.00	1
-397	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	9	0.00	1
-396	Max	0.00	1	0.00	1	0.00	13	0.00	33	0.00	1	0.00	1
-396	Min.	0.00	1	0.00	1	0.00	41	0.00	1	0.00	17	0.00	1
-395	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	13	0.00	1
-395	Min.	0.00	1	0.00	1	0.00	22	0.00	19	0.00	5	0.00	1
-394	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-394	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-393	Max	0.00	1	0.00	1	0.00	18	0.00	1	0.00	9	0.00	1
-393	Min.	0.00	1	0.00	1	0.00	13	0.00	9	0.00	1	0.00	1
-392	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-392	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-391	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-391	Min.	0.00	1	0.00	1	0.00	33	0.00	9	0.00	9	0.00	1
-390	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-390	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-389	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1
-389	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1	0.00	1
-388	Max	1023.34	19	3357.36	9	0.00	1	0.00	9	0.00	9	136.64	5
-388	Min.	52.28	13	-4302.47	23	0.00	9	0.00	1	0.00	1	-524.21	13
-387	Max	1529.80	9	8682.94	9	0.00	9	0.00	9	0.00	1	926.05	5
-387	Min.	-2023.74	23	-1391.33	1	0.00	39	0.00	1	0.00	9	99.79	13
-386	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-386	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	42	0.00	1
-385	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	13	0.00	1
-385	Min.	0.00	1	0.00	1	0.00	5	0.00	35	0.00	5	0.00	1
-384	Max	0.00	1	0.00	1	0.00	1	0.00	38	0.00	13	0.00	1
-384	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	5	0.00	1
-383	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-383	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-382	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-382	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-381	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-381	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-380	Max	0.00	1	0.00	1	0.00	9	0.00	29	0.00	9	0.00	1

-380	Min.	0.00	1	0.00	1	0.00	1	0.00	62	0.00	1	0.00	1
-379	Max	0.00	1	0.00	1	0.00	33	0.00	9	0.00	18	0.00	1
-379	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1
-378	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-378	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-377	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	17	0.00	1
-377	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-376	Max	0.00	1	0.00	1	0.00	34	0.00	1	0.00	1	0.00	1
-376	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-375	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1
-375	Min.	0.00	1	0.00	1	0.00	35	0.00	40	0.00	1	0.00	1
-374	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	25	0.00	1
-374	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1	0.00	1
-373	Max	0.00	1	0.00	1	0.00	1	0.00	18	0.00	42	0.00	1
-373	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1	0.00	1
-372	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-372	Min.	0.00	1	0.00	1	0.00	1	0.00	33	0.00	38	0.00	1
-371	Max	0.00	1	0.00	1	0.00	30	0.00	35	0.00	5	0.00	1
-371	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	13	0.00	1
-370	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	13	0.00	1
-370	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	5	0.00	1
-369	Max	0.00	1	0.00	1	0.00	13	0.00	1	0.00	5	0.00	1
-369	Min.	0.00	1	0.00	1	0.00	5	0.00	9	0.00	13	0.00	1
-368	Max	0.00	1	0.00	1	0.00	43	0.00	48	0.00	17	0.00	1
-368	Min.	0.00	1	0.00	1	0.00	13	0.00	9	0.00	13	0.00	1
-367	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	13	0.00	1
-367	Min.	0.00	1	0.00	1	0.00	13	0.00	35	0.00	5	0.00	1
-366	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	1	0.00	1
-366	Min.	0.00	1	0.00	1	0.00	18	0.00	46	0.00	30	0.00	1
-365	Max	0.00	1	0.00	1	0.00	5	0.00	1	0.00	1	0.00	1
-365	Min.	0.00	1	0.00	1	0.00	37	0.00	9	0.00	9	0.00	1
-364	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-364	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-363	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-363	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-362	Max	0.00	1	0.00	1	0.00	9	0.00	20	0.00	9	0.00	1
-362	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-361	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-361	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-360	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-360	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-359	Max	0.00	1	0.00	1	0.00	21	0.00	34	0.00	1	0.00	1
-359	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-358	Max	0.00	1	0.00	1	0.00	30	0.00	1	0.00	1	0.00	1
-358	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-357	Max	877.67	1	2913.01	13	0.00	1	0.00	1	0.00	9	301.93	5
-357	Min.	172.80	9	-5039.03	19	0.00	29	0.00	9	0.00	1	-467.27	13
-356	Max	609.13	13	7698.96	9	0.00	1	0.00	1	0.00	1	858.06	5
-356	Min.	-1905.53	19	-1777.84	1	0.00	9	0.00	9	0.00	9	-83.54	13
-355	Max	0.00	1	0.00	1	0.00	26	0.00	42	0.00	34	0.00	1
-355	Min.	0.00	1	0.00	1	0.00	1	0.00	49	0.00	1	0.00	1
-354	Max	0.00	1	0.00	1	0.00	42	0.00	9	0.00	21	0.00	1
-354	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	70	0.00	1
-353	Max	0.00	1	0.00	1	0.00	25	0.00	9	0.00	1	0.00	1
-353	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-352	Max	0.00	1	0.00	1	0.00	41	0.00	1	0.00	21	0.00	1
-352	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1	0.00	1
-351	Max	0.00	1	0.00	1	0.00	1	0.00	42	0.00	9	0.00	1
-351	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-350	Max	0.00	1	0.00	1	0.00	29	0.00	13	0.00	1	0.00	1
-350	Min.	0.00	1	0.00	1	0.00	46	0.00	25	0.00	9	0.00	1
-349	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	18	0.00	1
-349	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-348	Max	0.00	1	0.00	1	0.00	13	0.00	9	0.00	1	0.00	1
-348	Min.	0.00	1	0.00	1	0.00	5	0.00	1	0.00	9	0.00	1
-347	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	34	0.00	1
-347	Min.	0.00	1	0.00	1	0.00	9	0.00	41	0.00	1	0.00	1
-346	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-346	Min.	0.00	1	0.00	1	0.00	9	0.00	25	0.00	1	0.00	1
-345	Max	0.00	1	0.00	1	0.00	5	0.00	34	0.00	17	0.00	1
-345	Min.	0.00	1	0.00	1	0.00	13	0.00	1	0.00	1	0.00	1
-344	Max	0.00	1	0.00	1	0.00	34	0.00	1	0.00	1	0.00	1
-344	Min.	0.00	1	0.00	1	0.00	9	0.00	21	0.00	9	0.00	1

-343	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	9	0.00	1
-343	Min.	0.00	1	0.00	1	0.00	13	0.00	25	0.00	36	0.00	1
-342	Max	0.00	1	0.00	1	0.00	37	0.00	13	0.00	13	0.00	1
-342	Min.	0.00	1	0.00	1	0.00	1	0.00	5	0.00	37	0.00	1
-341	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	5	0.00	1
-341	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	13	0.00	1
-340	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	5	0.00	1
-340	Min.	0.00	1	0.00	1	0.00	34	0.00	5	0.00	33	0.00	1
-339	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	38	0.00	1
-339	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	13	0.00	1
-338	Max	0.00	1	0.00	1	0.00	13	0.00	1	0.00	13	0.00	1
-338	Min.	0.00	1	0.00	1	0.00	37	0.00	34	0.00	5	0.00	1
-337	Max	1015.59	1	2410.81	13	0.00	1	0.00	1	0.00	1	465.97	5
-337	Min.	152.03	9	-5736.69	19	0.00	9	0.00	9	0.00	9	-381.85	13
-336	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-336	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-335	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-335	Min.	0.00	1	0.00	1	0.00	33	0.00	9	0.00	9	0.00	1
-334	Max	0.00	1	0.00	1	0.00	1	0.00	85	0.00	35	0.00	1
-334	Min.	0.00	1	0.00	1	0.00	9	0.00	34	0.00	9	0.00	1
-333	Max	0.00	1	0.00	1	0.00	9	0.00	25	0.00	13	0.00	1
-333	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	5	0.00	1
-332	Max	0.00	1	0.00	1	0.00	25	0.00	9	0.00	9	0.00	1
-332	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	26	0.00	1
-331	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	25	0.00	1
-331	Min.	0.00	1	0.00	1	0.00	5	0.00	41	0.00	13	0.00	1
-330	Max	-15.00	13	6641.07	9	0.00	9	0.00	1	0.00	1	748.82	5
-330	Min.	-1774.11	19	-2120.70	1	0.00	26	0.00	9	0.00	9	-301.18	13
-329	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	36	0.00	1
-329	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	5	0.00	1
-328	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-328	Min.	0.00	1	0.00	1	0.00	42	0.00	9	0.00	9	0.00	1
-327	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1	0.00	1
-327	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1
-326	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-326	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-325	Max	0.00	1	0.00	1	0.00	9	0.00	5	0.00	1	0.00	1
-325	Min.	0.00	1	0.00	1	0.00	1	0.00	13	0.00	9	0.00	1
-324	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-324	Min.	0.00	1	0.00	1	0.00	34	0.00	9	0.00	34	0.00	1
-323	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-323	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-322	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	78	0.00	1
-322	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	41	0.00	1
-321	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	36	0.00	1
-321	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-320	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	32	0.00	1
-320	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-319	Max	0.00	1	0.00	1	0.00	33	0.00	13	0.00	9	0.00	1
-319	Min.	0.00	1	0.00	1	0.00	9	0.00	30	0.00	1	0.00	1
-318	Max	0.00	1	0.00	1	0.00	9	0.00	5	0.00	13	0.00	1
-318	Min.	0.00	1	0.00	1	0.00	18	0.00	13	0.00	5	0.00	1
-317	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-317	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-316	Max	0.00	1	0.00	1	0.00	1	0.00	20	0.00	1	0.00	1
-316	Min.	0.00	1	0.00	1	0.00	55	0.00	5	0.00	41	0.00	1
-315	Max	0.00	1	0.00	1	0.00	13	0.00	9	0.00	1	0.00	1
-315	Min.	0.00	1	0.00	1	0.00	40	0.00	1	0.00	9	0.00	1
-314	Max	0.00	1	0.00	1	0.00	13	0.00	9	0.00	1	0.00	1
-314	Min.	0.00	1	0.00	1	0.00	29	0.00	1	0.00	18	0.00	1
-313	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	5	0.00	1
-313	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	13	0.00	1
-312	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	13	0.00	1
-312	Min.	0.00	1	0.00	1	0.00	13	0.00	5	0.00	34	0.00	1
-311	Max	0.00	1	0.00	1	0.00	13	0.00	9	0.00	29	0.00	1
-311	Min.	0.00	1	0.00	1	0.00	5	0.00	1	0.00	5	0.00	1
-310	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1
-310	Min.	0.00	1	0.00	1	0.00	36	0.00	13	0.00	21	0.00	1
-309	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	5	0.00	1
-309	Min.	0.00	1	0.00	1	0.00	5	0.00	29	0.00	13	0.00	1
-308	Max	0.00	1	0.00	1	0.00	17	0.00	30	0.00	36	0.00	1
-308	Min.	0.00	1	0.00	1	0.00	9	0.00	13	0.00	5	0.00	1
-307	Max	1072.31	1	1924.25	13	0.00	17	0.00	9	0.00	9	618.40	5

-307	Min.	155.15	9	-6396.07	19	0.00	9	0.00	1	0.00	1	-276.56	13
-306	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1	0.00	1
-306	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1
-305	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-305	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-304	Max	-433.02	13	5533.62	1	0.00	1	0.00	9	0.00	9	649.82	1
-304	Min.	-1606.65	19	-2450.65	9	0.00	9	0.00	1	0.00	1	-557.40	9
-303	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	36	0.00	1
-303	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1
-302	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	17	0.00	1
-302	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1
-301	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-301	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-300	Max	0.00	1	0.00	1	0.00	5	0.00	9	0.00	5	0.00	1
-300	Min.	0.00	1	0.00	1	0.00	13	0.00	1	0.00	13	0.00	1
-299	Max	0.00	1	0.00	1	0.00	37	0.00	1	0.00	9	0.00	1
-299	Min.	0.00	1	0.00	1	0.00	54	0.00	9	0.00	1	0.00	1
-298	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	69	0.00	1
-298	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	22	0.00	1
-297	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	1	0.00	1
-297	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	9	0.00	1
-296	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	5	0.00	1
-296	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	27	0.00	1
-295	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-295	Min.	0.00	1	0.00	1	0.00	25	0.00	9	0.00	17	0.00	1
-294	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	1	0.00	1
-294	Min.	0.00	1	0.00	1	0.00	25	0.00	13	0.00	9	0.00	1
-293	Max	0.00	1	0.00	1	0.00	44	0.00	9	0.00	9	0.00	1
-293	Min.	0.00	1	0.00	1	0.00	5	0.00	1	0.00	1	0.00	1
-292	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	42	0.00	1
-292	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-291	Max	0.00	1	0.00	1	0.00	1	0.00	5	0.00	1	0.00	1
-291	Min.	0.00	1	0.00	1	0.00	9	0.00	13	0.00	9	0.00	1
-290	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-290	Min.	0.00	1	0.00	1	0.00	1	0.00	36	0.00	9	0.00	1
-289	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	5	0.00	1
-289	Min.	0.00	1	0.00	1	0.00	17	0.00	22	0.00	13	0.00	1
-288	Max	0.00	1	0.00	1	0.00	34	0.00	9	0.00	1	0.00	1
-288	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	36	0.00	1
-287	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1
-287	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1	0.00	1
-286	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	1	0.00	1
-286	Min.	0.00	1	0.00	1	0.00	31	0.00	25	0.00	9	0.00	1
-285	Max	0.00	1	0.00	1	0.00	27	0.00	5	0.00	1	0.00	1
-285	Min.	0.00	1	0.00	1	0.00	1	0.00	40	0.00	9	0.00	1
-284	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	5	0.00	1
-284	Min.	0.00	1	0.00	1	0.00	13	0.00	5	0.00	30	0.00	1
-283	Max	0.00	1	0.00	1	0.00	19	0.00	5	0.00	33	0.00	1
-283	Min.	0.00	1	0.00	1	0.00	5	0.00	22	0.00	13	0.00	1
-282	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1
-282	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1	0.00	1
-281	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	13	0.00	1
-281	Min.	0.00	1	0.00	1	0.00	13	0.00	5	0.00	5	0.00	1
-280	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	21	0.00	1
-280	Min.	0.00	1	0.00	1	0.00	29	0.00	32	0.00	1	0.00	1
-279	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	13	0.00	1
-279	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	32	0.00	1
-278	Max	0.00	1	0.00	1	0.00	1	0.00	34	0.00	1	0.00	1
-278	Min.	0.00	1	0.00	1	0.00	38	0.00	1	0.00	9	0.00	1
-277	Max	1084.13	1	1462.61	13	0.00	9	0.00	30	0.00	9	746.86	5
-277	Min.	158.64	9	-6931.47	19	0.00	1	0.00	9	0.00	1	-163.85	13
-276	Max	0.00	1	0.00	1	0.00	1	0.00	17	0.00	1	0.00	1
-276	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	9	0.00	1
-275	Max	-645.79	5	4459.08	1	0.00	9	0.00	1	0.00	1	553.84	1
-275	Min.	-1437.83	19	-3324.38	23	0.00	1	0.00	9	0.00	9	-807.09	9
-274	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	13	0.00	1
-274	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	5	0.00	1
-273	Max	0.00	1	0.00	1	0.00	37	0.00	9	0.00	17	0.00	1
-273	Min.	0.00	1	0.00	1	0.00	54	0.00	1	0.00	1	0.00	1
-272	Max	0.00	1	0.00	1	0.00	9	0.00	26	0.00	13	0.00	1
-272	Min.	0.00	1	0.00	1	0.00	1	0.00	5	0.00	29	0.00	1
-271	Max	0.00	1	0.00	1	0.00	13	0.00	1	0.00	5	0.00	1
-271	Min.	0.00	1	0.00	1	0.00	23	0.00	9	0.00	35	0.00	1

-270	Max	0.00	1	0.00	1	0.00	29	0.00	9	0.00	1	0.00	1
-270	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1
-269	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-269	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-268	Max	0.00	1	0.00	1	0.00	43	0.00	17	0.00	5	0.00	1
-268	Min.	0.00	1	0.00	1	0.00	9	0.00	13	0.00	13	0.00	1
-267	Max	0.00	1	0.00	1	0.00	1	0.00	19	0.00	9	0.00	1
-267	Min.	0.00	1	0.00	1	0.00	18	0.00	1	0.00	1	0.00	1
-266	Max	0.00	1	0.00	1	0.00	9	0.00	18	0.00	9	0.00	1
-266	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	25	0.00	1
-265	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1
-265	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1	0.00	1
-264	Max	0.00	1	0.00	1	0.00	5	0.00	1	0.00	19	0.00	1
-264	Min.	0.00	1	0.00	1	0.00	13	0.00	9	0.00	9	0.00	1
-263	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-263	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-262	Max	0.00	1	0.00	1	0.00	1	0.00	49	0.00	33	0.00	1
-262	Min.	0.00	1	0.00	1	0.00	9	0.00	42	0.00	1	0.00	1
-261	Max	0.00	1	0.00	1	0.00	1	0.00	5	0.00	13	0.00	1
-261	Min.	0.00	1	0.00	1	0.00	9	0.00	13	0.00	5	0.00	1
-260	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-260	Min.	0.00	1	0.00	1	0.00	17	0.00	9	0.00	1	0.00	1
-259	Max	0.00	1	0.00	1	0.00	9	0.00	13	0.00	9	0.00	1
-259	Min.	0.00	1	0.00	1	0.00	1	0.00	21	0.00	1	0.00	1
-258	Max	0.00	1	0.00	1	0.00	1	0.00	23	0.00	1	0.00	1
-258	Min.	0.00	1	0.00	1	0.00	40	0.00	9	0.00	9	0.00	1
-257	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	13	0.00	1
-257	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	5	0.00	1
-256	Max	0.00	1	0.00	1	0.00	5	0.00	29	0.00	17	0.00	1
-256	Min.	0.00	1	0.00	1	0.00	27	0.00	1	0.00	1	0.00	1
-255	Max	0.00	1	0.00	1	0.00	35	0.00	51	0.00	35	0.00	1
-255	Min.	0.00	1	0.00	1	0.00	60	0.00	44	0.00	13	0.00	1
-254	Max	0.00	1	0.00	1	0.00	9	0.00	43	0.00	13	0.00	1
-254	Min.	0.00	1	0.00	1	0.00	1	0.00	13	0.00	5	0.00	1
-253	Max	0.00	1	0.00	1	0.00	1	0.00	5	0.00	9	0.00	1
-253	Min.	0.00	1	0.00	1	0.00	9	0.00	42	0.00	1	0.00	1
-252	Max	0.00	1	0.00	1	0.00	51	0.00	13	0.00	13	0.00	1
-252	Min.	0.00	1	0.00	1	0.00	44	0.00	5	0.00	5	0.00	1
-251	Max	0.00	1	0.00	1	0.00	13	0.00	1	0.00	1	0.00	1
-251	Min.	0.00	1	0.00	1	0.00	28	0.00	9	0.00	9	0.00	1
-250	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	1	0.00	1
-250	Min.	0.00	1	0.00	1	0.00	13	0.00	5	0.00	9	0.00	1
-249	Max	0.00	1	0.00	1	0.00	13	0.00	19	0.00	24	0.00	1
-249	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	13	0.00	1
-248	Max	0.00	1	0.00	1	0.00	33	0.00	1	0.00	1	0.00	1
-248	Min.	0.00	1	0.00	1	0.00	86	0.00	9	0.00	18	0.00	1
-247	Max	1081.97	1	1046.98	13	0.00	9	0.00	1	0.00	1	839.05	5
-247	Min.	157.50	9	-7298.14	19	0.00	17	0.00	9	0.00	9	-55.71	13
-246	Max	-573.95	1	3639.61	5	0.00	57	0.00	9	0.00	1	450.69	1
-246	Min.	-1304.03	18	-4156.48	23	0.00	34	0.00	27	0.00	9	-1006.52	9
-245	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-245	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-244	Max	0.00	1	0.00	1	0.00	50	0.00	13	0.00	1	0.00	1
-244	Min.	0.00	1	0.00	1	0.00	1	0.00	5	0.00	9	0.00	1
-243	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	23	0.00	1
-243	Min.	0.00	1	0.00	1	0.00	1	0.00	30	0.00	1	0.00	1
-242	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1	0.00	1
-242	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1
-241	Max	0.00	1	0.00	1	0.00	1	0.00	31	0.00	31	0.00	1
-241	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	13	0.00	1
-240	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-240	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-239	Max	0.00	1	0.00	1	0.00	5	0.00	1	0.00	5	0.00	1
-239	Min.	0.00	1	0.00	1	0.00	13	0.00	9	0.00	13	0.00	1
-238	Max	0.00	1	0.00	1	0.00	17	0.00	9	0.00	5	0.00	1
-238	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	13	0.00	1
-237	Max	0.00	1	0.00	1	0.00	13	0.00	50	0.00	59	0.00	1
-237	Min.	0.00	1	0.00	1	0.00	5	0.00	41	0.00	36	0.00	1
-236	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	1	0.00	1
-236	Min.	0.00	1	0.00	1	0.00	22	0.00	5	0.00	33	0.00	1
-235	Max	0.00	1	0.00	1	0.00	13	0.00	27	0.00	18	0.00	1
-235	Min.	0.00	1	0.00	1	0.00	43	0.00	5	0.00	9	0.00	1
-234	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1

-234	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1	0.00	1
-233	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-233	Min.	0.00	1	0.00	1	0.00	9	0.00	38	0.00	1	0.00	1
-232	Max	0.00	1	0.00	1	0.00	5	0.00	19	0.00	5	0.00	1
-232	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	50	0.00	1
-231	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	30	0.00	1
-231	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	45	0.00	1
-230	Max	0.00	1	0.00	1	0.00	41	0.00	1	0.00	18	0.00	1
-230	Min.	0.00	1	0.00	1	0.00	50	0.00	9	0.00	9	0.00	1
-229	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	13	0.00	1
-229	Min.	0.00	1	0.00	1	0.00	13	0.00	5	0.00	23	0.00	1
-228	Max	0.00	1	0.00	1	0.00	9	0.00	17	0.00	9	0.00	1
-228	Min.	0.00	1	0.00	1	0.00	31	0.00	1	0.00	1	0.00	1
-227	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	13	0.00	1
-227	Min.	0.00	1	0.00	1	0.00	55	0.00	28	0.00	33	0.00	1
-226	Max	0.00	1	0.00	1	0.00	13	0.00	59	0.00	20	0.00	1
-226	Min.	0.00	1	0.00	1	0.00	5	0.00	36	0.00	1	0.00	1
-225	Max	0.00	1	0.00	1	0.00	9	0.00	33	0.00	37	0.00	1
-225	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-224	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	5	0.00	1
-224	Min.	0.00	1	0.00	1	0.00	13	0.00	5	0.00	13	0.00	1
-223	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	30	0.00	1
-223	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-222	Max	0.00	1	0.00	1	0.00	13	0.00	17	0.00	5	0.00	1
-222	Min.	0.00	1	0.00	1	0.00	30	0.00	5	0.00	28	0.00	1
-221	Max	0.00	1	0.00	1	0.00	31	0.00	1	0.00	5	0.00	1
-221	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	26	0.00	1
-220	Max	0.00	1	0.00	1	0.00	18	0.00	5	0.00	23	0.00	1
-220	Min.	0.00	1	0.00	1	0.00	9	0.00	13	0.00	5	0.00	1
-219	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	28	0.00	1
-219	Min.	0.00	1	0.00	1	0.00	28	0.00	9	0.00	9	0.00	1
-218	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-218	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-217	Max	1090.38	1	702.58	13	0.00	19	0.00	18	0.00	1	904.03	1
-217	Min.	153.45	9	-7461.79	19	0.00	5	0.00	5	0.00	9	14.07	9
-216	Max	-429.44	1	2918.27	5	0.00	9	0.00	1	0.00	13	351.76	1
-216	Min.	-1236.46	34	-4792.53	19	0.00	1	0.00	9	0.00	5	-1135.25	9
-215	Max	0.00	1	0.00	1	0.00	1	0.00	13	0.00	13	0.00	1
-215	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	21	0.00	1
-214	Max	0.00	1	0.00	1	0.00	5	0.00	1	0.00	9	0.00	1
-214	Min.	0.00	1	0.00	1	0.00	27	0.00	9	0.00	1	0.00	1
-213	Max	0.00	1	0.00	1	0.00	5	0.00	9	0.00	27	0.00	1
-213	Min.	0.00	1	0.00	1	0.00	13	0.00	1	0.00	5	0.00	1
-212	Max	0.00	1	0.00	1	0.00	9	0.00	13	0.00	13	0.00	1
-212	Min.	0.00	1	0.00	1	0.00	1	0.00	5	0.00	5	0.00	1
-211	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-211	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-210	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	13	0.00	1
-210	Min.	0.00	1	0.00	1	0.00	30	0.00	1	0.00	5	0.00	1
-209	Max	0.00	1	0.00	1	0.00	25	0.00	9	0.00	9	0.00	1
-209	Min.	0.00	1	0.00	1	0.00	5	0.00	1	0.00	23	0.00	1
-208	Max	0.00	1	0.00	1	0.00	13	0.00	23	0.00	13	0.00	1
-208	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	5	0.00	1
-207	Max	0.00	1	0.00	1	0.00	31	0.00	31	0.00	9	0.00	1
-207	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-206	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1
-206	Min.	0.00	1	0.00	1	0.00	21	0.00	9	0.00	18	0.00	1
-205	Max	0.00	1	0.00	1	0.00	26	0.00	17	0.00	9	0.00	1
-205	Min.	0.00	1	0.00	1	0.00	1	0.00	13	0.00	1	0.00	1
-204	Max	0.00	1	0.00	1	0.00	18	0.00	18	0.00	5	0.00	1
-204	Min.	0.00	1	0.00	1	0.00	5	0.00	9	0.00	23	0.00	1
-203	Max	0.00	1	0.00	1	0.00	32	0.00	5	0.00	13	0.00	1
-203	Min.	0.00	1	0.00	1	0.00	13	0.00	30	0.00	5	0.00	1
-202	Max	0.00	1	0.00	1	0.00	52	0.00	42	0.00	1	0.00	1
-202	Min.	0.00	1	0.00	1	0.00	5	0.00	49	0.00	23	0.00	1
-201	Max	0.00	1	0.00	1	0.00	20	0.00	5	0.00	13	0.00	1
-201	Min.	0.00	1	0.00	1	0.00	5	0.00	34	0.00	5	0.00	1
-200	Max	0.00	1	0.00	1	0.00	1	0.00	13	0.00	9	0.00	1
-200	Min.	0.00	1	0.00	1	0.00	17	0.00	5	0.00	26	0.00	1
-199	Max	0.00	1	0.00	1	0.00	34	0.00	9	0.00	55	0.00	1
-199	Min.	0.00	1	0.00	1	0.00	57	0.00	1	0.00	40	0.00	1
-198	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	40	0.00	1
-198	Min.	0.00	1	0.00	1	0.00	13	0.00	5	0.00	5	0.00	1

-197	Max	0.00	1	0.00	1	0.00	20	0.00	24	0.00	1	0.00	1
-197	Min.	0.00	1	0.00	1	0.00	13	0.00	1	0.00	9	0.00	1
-196	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1
-196	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	13	0.00	1
-195	Max	0.00	1	0.00	1	0.00	1	0.00	13	0.00	1	0.00	1
-195	Min.	0.00	1	0.00	1	0.00	9	0.00	20	0.00	9	0.00	1
-194	Max	0.00	1	0.00	1	0.00	18	0.00	9	0.00	5	0.00	1
-194	Min.	0.00	1	0.00	1	0.00	13	0.00	55	0.00	13	0.00	1
-193	Max	0.00	1	0.00	1	0.00	13	0.00	20	0.00	13	0.00	1
-193	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	43	0.00	1
-192	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	5	0.00	1
-192	Min.	0.00	1	0.00	1	0.00	48	0.00	5	0.00	13	0.00	1
-191	Max	0.00	1	0.00	1	0.00	1	0.00	5	0.00	5	0.00	1
-191	Min.	0.00	1	0.00	1	0.00	9	0.00	36	0.00	36	0.00	1
-190	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1
-190	Min.	0.00	1	0.00	1	0.00	13	0.00	27	0.00	13	0.00	1
-189	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1
-189	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1	0.00	1
-188	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	5	0.00	1
-188	Min.	0.00	1	0.00	1	0.00	37	0.00	1	0.00	46	0.00	1
-187	Max	1134.03	1	474.59	13	0.00	9	0.00	1	0.00	9	916.51	1
-187	Min.	159.29	9	-7366.63	19	0.00	30	0.00	17	0.00	1	44.34	9
-186	Max	-298.10	1	2333.17	5	0.00	9	0.00	1	0.00	9	264.41	1
-186	Min.	-1374.86	9	-5148.61	19	0.00	24	0.00	9	0.00	1	-1167.64	9
-185	Max	0.00	1	0.00	1	0.00	1	0.00	20	0.00	5	0.00	1
-185	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	13	0.00	1
-184	Max	0.00	1	0.00	1	0.00	13	0.00	9	0.00	1	0.00	1
-184	Min.	0.00	1	0.00	1	0.00	5	0.00	1	0.00	24	0.00	1
-183	Max	0.00	1	0.00	1	0.00	1	0.00	13	0.00	13	0.00	1
-183	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	5	0.00	1
-182	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-182	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-181	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-181	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-180	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	1	0.00	1
-180	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	38	0.00	1
-179	Max	0.00	1	0.00	1	0.00	5	0.00	1	0.00	5	0.00	1
-179	Min.	0.00	1	0.00	1	0.00	13	0.00	9	0.00	31	0.00	1
-178	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	27	0.00	1
-178	Min.	0.00	1	0.00	1	0.00	28	0.00	32	0.00	1	0.00	1
-177	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	5	0.00	1
-177	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	13	0.00	1
-176	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	17	0.00	1
-176	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	1	0.00	1
-175	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	13	0.00	1
-175	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	5	0.00	1
-174	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	1	0.00	1
-174	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	27	0.00	1
-173	Max	0.00	1	0.00	1	0.00	24	0.00	5	0.00	55	0.00	1
-173	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	9	0.00	1
-172	Max	0.00	1	0.00	1	0.00	13	0.00	40	0.00	9	0.00	1
-172	Min.	0.00	1	0.00	1	0.00	5	0.00	55	0.00	1	0.00	1
-171	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	13	0.00	1
-171	Min.	0.00	1	0.00	1	0.00	43	0.00	13	0.00	28	0.00	1
-170	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	5	0.00	1
-170	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	28	0.00	1
-169	Max	0.00	1	0.00	1	0.00	27	0.00	5	0.00	20	0.00	1
-169	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	5	0.00	1
-168	Max	0.00	1	0.00	1	0.00	31	0.00	1	0.00	9	0.00	1
-168	Min.	0.00	1	0.00	1	0.00	1	0.00	29	0.00	1	0.00	1
-167	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	5	0.00	1
-167	Min.	0.00	1	0.00	1	0.00	20	0.00	24	0.00	13	0.00	1
-166	Max	0.00	1	0.00	1	0.00	27	0.00	9	0.00	18	0.00	1
-166	Min.	0.00	1	0.00	1	0.00	13	0.00	1	0.00	5	0.00	1
-165	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	1	0.00	1
-165	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	9	0.00	1
-164	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	13	0.00	1
-164	Min.	0.00	1	0.00	1	0.00	35	0.00	36	0.00	5	0.00	1
-163	Max	0.00	1	0.00	1	0.00	13	0.00	1	0.00	9	0.00	1
-163	Min.	0.00	1	0.00	1	0.00	5	0.00	9	0.00	1	0.00	1
-162	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	13	0.00	1
-162	Min.	0.00	1	0.00	1	0.00	5	0.00	31	0.00	5	0.00	1
-161	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	13	0.00	1

-161	Min.	0.00	1	0.00	1	0.00	13	0.00	5	0.00	17	0.00	1
-160	Max	0.00	1	0.00	1	0.00	1	0.00	5	0.00	5	0.00	1
-160	Min.	0.00	1	0.00	1	0.00	9	0.00	13	0.00	13	0.00	1
-159	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-159	Min.	0.00	1	0.00	1	0.00	49	0.00	9	0.00	9	0.00	1
-158	Max	0.00	1	0.00	1	0.00	13	0.00	9	0.00	13	0.00	1
-158	Min.	0.00	1	0.00	1	0.00	5	0.00	1	0.00	5	0.00	1
-157	Max	1303.76	1	406.36	13	0.00	5	0.00	5	0.00	1	819.24	1
-157	Min.	217.53	9	-6966.72	19	0.00	13	0.00	13	0.00	9	48.23	9
-156	Max	-235.10	1	1955.82	13	0.00	9	0.00	13	0.00	9	203.43	1
-156	Min.	-1632.51	9	-5175.71	19	0.00	27	0.00	55	0.00	1	-1064.28	9
-155	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	5	0.00	1
-155	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	13	0.00	1
-154	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-154	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-153	Max	0.00	1	0.00	1	0.00	13	0.00	9	0.00	9	0.00	1
-153	Min.	0.00	1	0.00	1	0.00	5	0.00	1	0.00	1	0.00	1
-152	Max	0.00	1	0.00	1	0.00	9	0.00	20	0.00	9	0.00	1
-152	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-151	Max	0.00	1	0.00	1	0.00	1	0.00	13	0.00	19	0.00	1
-151	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	5	0.00	1
-150	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	13	0.00	1
-150	Min.	0.00	1	0.00	1	0.00	5	0.00	18	0.00	24	0.00	1
-149	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	30	0.00	1
-149	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	1	0.00	1
-148	Max	0.00	1	0.00	1	0.00	9	0.00	5	0.00	1	0.00	1
-148	Min.	0.00	1	0.00	1	0.00	1	0.00	13	0.00	9	0.00	1
-147	Max	0.00	1	0.00	1	0.00	13	0.00	18	0.00	13	0.00	1
-147	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	5	0.00	1
-146	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	9	0.00	1
-146	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	1	0.00	1
-145	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	27	0.00	1
-145	Min.	0.00	1	0.00	1	0.00	1	0.00	19	0.00	13	0.00	1
-144	Max	0.00	1	0.00	1	0.00	27	0.00	5	0.00	27	0.00	1
-144	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	1	0.00	1
-143	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1
-143	Min.	0.00	1	0.00	1	0.00	19	0.00	13	0.00	13	0.00	1
-142	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1	0.00	1
-142	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	9	0.00	1
-141	Max	0.00	1	0.00	1	0.00	5	0.00	32	0.00	13	0.00	1
-141	Min.	0.00	1	0.00	1	0.00	33	0.00	5	0.00	5	0.00	1
-140	Max	0.00	1	0.00	1	0.00	1	0.00	5	0.00	5	0.00	1
-140	Min.	0.00	1	0.00	1	0.00	9	0.00	13	0.00	13	0.00	1
-139	Max	0.00	1	0.00	1	0.00	5	0.00	28	0.00	31	0.00	1
-139	Min.	0.00	1	0.00	1	0.00	31	0.00	5	0.00	13	0.00	1
-138	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	13	0.00	1
-138	Min.	0.00	1	0.00	1	0.00	1	0.00	19	0.00	17	0.00	1
-137	Max	0.00	1	0.00	1	0.00	22	0.00	47	0.00	5	0.00	1
-137	Min.	0.00	1	0.00	1	0.00	13	0.00	40	0.00	13	0.00	1
-136	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	9	0.00	1
-136	Min.	0.00	1	0.00	1	0.00	36	0.00	5	0.00	19	0.00	1
-135	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	28	0.00	1
-135	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	5	0.00	1
-134	Max	0.00	1	0.00	1	0.00	5	0.00	9	0.00	1	0.00	1
-134	Min.	0.00	1	0.00	1	0.00	13	0.00	1	0.00	9	0.00	1
-133	Max	0.00	1	0.00	1	0.00	27	0.00	5	0.00	13	0.00	1
-133	Min.	0.00	1	0.00	1	0.00	13	0.00	27	0.00	5	0.00	1
-132	Max	0.00	1	0.00	1	0.00	51	0.00	13	0.00	13	0.00	1
-132	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	28	0.00	1
-131	Max	0.00	1	0.00	1	0.00	24	0.00	27	0.00	23	0.00	1
-131	Min.	0.00	1	0.00	1	0.00	5	0.00	1	0.00	5	0.00	1
-130	Max	0.00	1	0.00	1	0.00	9	0.00	5	0.00	1	0.00	1
-130	Min.	0.00	1	0.00	1	0.00	18	0.00	13	0.00	9	0.00	1
-129	Max	0.00	1	0.00	1	0.00	26	0.00	9	0.00	9	0.00	1
-129	Min.	0.00	1	0.00	1	0.00	1	0.00	30	0.00	1	0.00	1
-128	Max	0.00	1	0.00	1	0.00	13	0.00	1	0.00	19	0.00	1
-128	Min.	0.00	1	0.00	1	0.00	27	0.00	9	0.00	5	0.00	1
-127	Max	1559.64	1	602.73	13	0.00	9	0.00	9	0.00	30	544.10	1
-127	Min.	215.81	9	-6099.58	19	0.00	1	0.00	1	0.00	1	12.27	9
-126	Max	36.02	1	1959.57	13	0.00	13	0.00	9	0.00	9	172.33	1
-126	Min.	-2149.47	9	-4739.00	19	0.00	28	0.00	1	0.00	1	-734.99	9
-125	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	1	0.00	1
-125	Min.	0.00	1	0.00	1	0.00	13	0.00	24	0.00	9	0.00	1

-124	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1	0.00	1
-124	Min.	0.00	1	0.00	1	0.00	9	0.00	9	0.00	9	0.00	1
-123	Max	0.00	1	0.00	1	0.00	13	0.00	9	0.00	13	0.00	1
-123	Min.	0.00	1	0.00	1	0.00	5	0.00	1	0.00	24	0.00	1
-122	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	1	0.00	1
-122	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	9	0.00	1
-121	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	13	0.00	1
-121	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	5	0.00	1
-120	Max	0.00	1	0.00	1	0.00	1	0.00	5	0.00	5	0.00	1
-120	Min.	0.00	1	0.00	1	0.00	9	0.00	13	0.00	13	0.00	1
-119	Max	0.00	1	0.00	1	0.00	13	0.00	23	0.00	20	0.00	1
-119	Min.	0.00	1	0.00	1	0.00	5	0.00	1	0.00	9	0.00	1
-118	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1
-118	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	13	0.00	1
-117	Max	0.00	1	0.00	1	0.00	5	0.00	23	0.00	1	0.00	1
-117	Min.	0.00	1	0.00	1	0.00	36	0.00	13	0.00	9	0.00	1
-116	Max	0.00	1	0.00	1	0.00	9	0.00	5	0.00	5	0.00	1
-116	Min.	0.00	1	0.00	1	0.00	1	0.00	13	0.00	13	0.00	1
-115	Max	0.00	1	0.00	1	0.00	9	0.00	35	0.00	1	0.00	1
-115	Min.	0.00	1	0.00	1	0.00	1	0.00	60	0.00	9	0.00	1
-114	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	5	0.00	1
-114	Min.	0.00	1	0.00	1	0.00	31	0.00	5	0.00	13	0.00	1
-113	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	13	0.00	1
-113	Min.	0.00	1	0.00	1	0.00	44	0.00	19	0.00	5	0.00	1
-112	Max	0.00	1	0.00	1	0.00	35	0.00	19	0.00	9	0.00	1
-112	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-111	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	5	0.00	1
-111	Min.	0.00	1	0.00	1	0.00	27	0.00	5	0.00	13	0.00	1
-110	Max	0.00	1	0.00	1	0.00	5	0.00	9	0.00	5	0.00	1
-110	Min.	0.00	1	0.00	1	0.00	13	0.00	37	0.00	13	0.00	1
-109	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	31	0.00	1
-109	Min.	0.00	1	0.00	1	0.00	32	0.00	5	0.00	13	0.00	1
-108	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	19	0.00	1
-108	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	5	0.00	1
-107	Max	0.00	1	0.00	1	0.00	32	0.00	5	0.00	5	0.00	1
-107	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	13	0.00	1
-106	Max	0.00	1	0.00	1	0.00	5	0.00	28	0.00	5	0.00	1
-106	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	28	0.00	1
-105	Max	0.00	1	0.00	1	0.00	13	0.00	27	0.00	5	0.00	1
-105	Min.	0.00	1	0.00	1	0.00	19	0.00	5	0.00	13	0.00	1
-104	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	1	0.00	1
-104	Min.	0.00	1	0.00	1	0.00	25	0.00	5	0.00	9	0.00	1
-103	Max	0.00	1	0.00	1	0.00	1	0.00	13	0.00	1	0.00	1
-103	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	19	0.00	1
-102	Max	0.00	1	0.00	1	0.00	1	0.00	13	0.00	27	0.00	1
-102	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	9	0.00	1
-101	Max	0.00	1	0.00	1	0.00	36	0.00	13	0.00	13	0.00	1
-101	Min.	0.00	1	0.00	1	0.00	59	0.00	5	0.00	5	0.00	1
-100	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-100	Min.	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-99	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	5	0.00	1
-99	Min.	0.00	1	0.00	1	0.00	31	0.00	9	0.00	55	0.00	1
-98	Max	0.00	1	0.00	1	0.00	5	0.00	1	0.00	22	0.00	1
-98	Min.	0.00	1	0.00	1	0.00	37	0.00	9	0.00	1	0.00	1
-97	Max	584.34	13	-724.71	13	0.00	5	0.00	31	0.00	1	19.01	5
-97	Min.	-2302.01	19	-5377.21	19	0.00	13	0.00	13	0.00	9	-146.84	13
-96	Max	277.41	13	-463.92	9	0.00	13	0.00	13	0.00	1	-198.41	9
-96	Min.	-5879.45	19	-2010.89	1	0.00	5	0.00	5	0.00	9	-635.49	1
-95	Max	730.57	13	-104.46	9	0.00	1	0.00	5	0.00	13	-253.69	9
-95	Min.	-4930.89	19	-1306.29	1	0.00	30	0.00	13	0.00	5	-899.33	1
-94	Max	956.90	13	-54.47	9	0.00	9	0.00	9	0.00	13	-266.16	9
-94	Min.	-4197.93	19	-1050.09	1	0.00	1	0.00	1	0.00	5	-1004.26	1
-93	Max	1104.44	13	-54.31	9	0.00	5	0.00	1	0.00	5	-260.81	9
-93	Min.	-3532.05	19	-921.30	1	0.00	13	0.00	28	0.00	24	-1025.96	1
-92	Max	1213.59	13	-56.51	9	0.00	13	0.00	59	0.00	5	-240.67	9
-92	Min.	-2942.82	19	-801.34	1	0.00	45	0.00	13	0.00	13	-992.08	1
-91	Max	1263.70	13	-56.50	9	0.00	13	0.00	5	0.00	5	-202.62	13
-91	Min.	-2421.23	19	-697.10	1	0.00	5	0.00	13	0.00	13	-931.56	5
-90	Max	1278.38	13	-55.20	9	0.00	5	0.00	5	0.00	13	-153.84	13
-90	Min.	-1938.89	19	-607.06	1	0.00	13	0.00	13	0.00	5	-853.63	5
-89	Max	1262.69	13	-44.03	13	0.00	1	0.00	13	0.00	5	-101.71	13
-89	Min.	-1485.43	19	-538.17	5	0.00	47	0.00	5	0.00	18	-762.23	5
-88	Max	1373.83	9	-5.92	13	0.00	5	0.00	13	0.00	5	-47.41	13

-88	Min.	-1153.89	1	-510.74	5	0.00	31	0.00	60	0.00	13	-663.39	5
-87	Max	1470.18	9	20.87	13	0.00	24	0.00	13	0.00	27	9.14	13
-87	Min.	-1080.25	1	-489.28	5	0.00	5	0.00	5	0.00	13	-561.00	5
-86	Max	1524.92	9	34.31	13	0.00	13	0.00	5	0.00	13	69.04	13
-86	Min.	-997.56	1	-473.11	5	0.00	27	0.00	23	0.00	5	-457.97	5
-85	Max	1539.10	9	33.86	13	0.00	13	0.00	13	0.00	13	134.28	13
-85	Min.	-905.47	1	-462.01	5	0.00	20	0.00	5	0.00	5	-356.78	5
-84	Max	1518.21	9	26.17	13	0.00	13	0.00	5	0.00	5	207.37	13
-84	Min.	-809.22	1	-462.51	5	0.00	5	0.00	13	0.00	27	-259.48	5
-83	Max	1489.86	9	15.04	13	0.00	5	0.00	28	0.00	5	296.24	9
-83	Min.	-735.56	1	-477.25	5	0.00	13	0.00	1	0.00	13	-173.44	1
-82	Max	1455.78	9	-7.89	13	0.00	5	0.00	19	0.00	19	398.43	9
-82	Min.	-684.73	1	-498.33	5	0.00	20	0.00	5	0.00	5	-95.77	1
-81	Max	1443.97	18	-36.29	5	0.00	9	0.00	52	0.00	9	511.66	9
-81	Min.	-633.17	9	-532.33	13	0.00	27	0.00	9	0.00	1	-24.20	1
-80	Max	1685.88	18	-70.67	5	0.00	13	0.00	27	0.00	5	634.45	9
-80	Min.	-568.28	9	-578.70	13	0.00	29	0.00	5	0.00	13	41.69	1
-79	Max	1940.47	19	-77.10	1	0.00	31	0.00	13	0.00	5	763.67	9
-79	Min.	-618.52	13	-670.62	9	0.00	13	0.00	5	0.00	13	102.39	1
-78	Max	2201.67	19	-66.29	1	0.00	20	0.00	13	0.00	5	894.07	9
-78	Min.	-761.07	13	-794.17	9	0.00	13	0.00	5	0.00	13	158.23	1
-77	Max	2473.25	19	-45.67	1	0.00	5	0.00	5	0.00	13	1016.87	9
-77	Min.	-901.88	13	-935.35	9	0.00	13	0.00	19	0.00	5	209.00	1
-76	Max	2774.07	19	-9.22	1	0.00	5	0.00	13	0.00	9	1118.55	9
-76	Min.	-1074.73	13	-1091.19	9	0.00	13	0.00	5	0.00	1	253.62	1
-75	Max	3133.52	19	46.09	1	0.00	1	0.00	31	0.00	5	1179.03	9
-75	Min.	-1283.14	13	-1256.31	9	0.00	9	0.00	1	0.00	31	290.04	1
-74	Max	3599.00	19	112.19	1	0.00	13	0.00	5	0.00	5	1169.89	9
-74	Min.	-1442.98	13	-1428.64	9	0.00	5	0.00	19	0.00	13	313.99	1
-73	Max	4197.76	19	150.88	1	0.00	60	0.00	21	0.00	13	1048.98	34
-73	Min.	-1470.95	13	-1695.30	9	0.00	13	0.00	5	0.00	5	323.97	1
-72	Max	5187.21	19	-233.31	1	0.00	9	0.00	23	0.00	13	771.95	34
-72	Min.	-1129.24	13	-2126.96	9	0.00	19	0.00	1	0.00	5	287.26	1
-71	Max	2098.04	1	5.24	5	0.00	13	0.00	9	0.00	13	219.85	1
-71	Min.	-1730.72	9	-4942.25	19	0.00	23	0.00	1	0.00	5	-21.75	9
-70	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	13	0.00	1
-70	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	5	0.00	1
-69	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	1	0.00	1
-69	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	9	0.00	1
-68	Max	0.00	1	0.00	1	0.00	13	0.00	9	0.00	13	0.00	1
-68	Min.	0.00	1	0.00	1	0.00	5	0.00	1	0.00	5	0.00	1
-67	Max	0.00	1	0.00	1	0.00	5	0.00	1	0.00	32	0.00	1
-67	Min.	0.00	1	0.00	1	0.00	23	0.00	17	0.00	13	0.00	1
-66	Max	0.00	1	0.00	1	0.00	24	0.00	5	0.00	1	0.00	1
-66	Min.	0.00	1	0.00	1	0.00	1	0.00	13	0.00	27	0.00	1
-65	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1
-65	Min.	0.00	1	0.00	1	0.00	13	0.00	28	0.00	13	0.00	1
-64	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	13	0.00	1
-64	Min.	0.00	1	0.00	1	0.00	13	0.00	5	0.00	5	0.00	1
-63	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	1	0.00	1
-63	Min.	0.00	1	0.00	1	0.00	13	0.00	30	0.00	9	0.00	1
-62	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	5	0.00	1
-62	Min.	0.00	1	0.00	1	0.00	20	0.00	5	0.00	13	0.00	1
-61	Max	0.00	1	0.00	1	0.00	23	0.00	1	0.00	5	0.00	1
-61	Min.	0.00	1	0.00	1	0.00	13	0.00	9	0.00	13	0.00	1
-60	Max	0.00	1	0.00	1	0.00	9	0.00	1	0.00	13	0.00	1
-60	Min.	0.00	1	0.00	1	0.00	30	0.00	18	0.00	5	0.00	1
-59	Max	0.00	1	0.00	1	0.00	1	0.00	13	0.00	32	0.00	1
-59	Min.	0.00	1	0.00	1	0.00	9	0.00	24	0.00	9	0.00	1
-58	Max	0.00	1	0.00	1	0.00	31	0.00	1	0.00	5	0.00	1
-58	Min.	0.00	1	0.00	1	0.00	5	0.00	20	0.00	13	0.00	1
-57	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	13	0.00	1
-57	Min.	0.00	1	0.00	1	0.00	28	0.00	18	0.00	5	0.00	1
-56	Max	0.00	1	0.00	1	0.00	13	0.00	31	0.00	5	0.00	1
-56	Min.	0.00	1	0.00	1	0.00	43	0.00	5	0.00	19	0.00	1
-55	Max	0.00	1	0.00	1	0.00	13	0.00	30	0.00	5	0.00	1
-55	Min.	0.00	1	0.00	1	0.00	5	0.00	9	0.00	24	0.00	1
-54	Max	0.00	1	0.00	1	0.00	5	0.00	35	0.00	13	0.00	1
-54	Min.	0.00	1	0.00	1	0.00	22	0.00	5	0.00	5	0.00	1
-53	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	5	0.00	1
-53	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	25	0.00	1
-52	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	5	0.00	1
-52	Min.	0.00	1	0.00	1	0.00	31	0.00	19	0.00	24	0.00	1

-51	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	13	0.00	1
-51	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1
-50	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1
-50	Min.	0.00	1	0.00	1	0.00	28	0.00	52	0.00	13	0.00	1
-49	Max	0.00	1	0.00	1	0.00	19	0.00	13	0.00	13	0.00	1
-49	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	24	0.00	1
-48	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	31	0.00	1
-48	Min.	0.00	1	0.00	1	0.00	5	0.00	19	0.00	1	0.00	1
-47	Max	0.00	1	0.00	1	0.00	1	0.00	9	0.00	5	0.00	1
-47	Min.	0.00	1	0.00	1	0.00	9	0.00	1	0.00	13	0.00	1
-46	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	5	0.00	1
-46	Min.	0.00	1	0.00	1	0.00	27	0.00	5	0.00	13	0.00	1
-45	Max	0.00	1	0.00	1	0.00	27	0.00	5	0.00	13	0.00	1
-45	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	5	0.00	1
-44	Max	0.00	1	0.00	1	0.00	28	0.00	5	0.00	13	0.00	1
-44	Min.	0.00	1	0.00	1	0.00	9	0.00	13	0.00	32	0.00	1
-43	Max	0.00	1	0.00	1	0.00	5	0.00	51	0.00	28	0.00	1
-43	Min.	0.00	1	0.00	1	0.00	58	0.00	13	0.00	5	0.00	1
-42	Max	0.00	1	0.00	1	0.00	9	0.00	5	0.00	5	0.00	1
-42	Min.	0.00	1	0.00	1	0.00	27	0.00	13	0.00	20	0.00	1
-41	Max	0.00	1	0.00	1	0.00	31	0.00	13	0.00	31	0.00	1
-41	Min.	0.00	1	0.00	1	0.00	1	0.00	31	0.00	1	0.00	1
-40	Max	0.00	1	0.00	1	0.00	13	0.00	9	0.00	21	0.00	1
-40	Min.	0.00	1	0.00	1	0.00	18	0.00	18	0.00	5	0.00	1
-39	Max	0.00	1	0.00	1	0.00	31	0.00	5	0.00	1	0.00	1
-39	Min.	0.00	1	0.00	1	0.00	13	0.00	28	0.00	9	0.00	1
-38	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	9	0.00	1
-38	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	1	0.00	1
-37	Max	0.00	1	0.00	1	0.00	29	0.00	1	0.00	1	0.00	1
-37	Min.	0.00	1	0.00	1	0.00	1	0.00	19	0.00	9	0.00	1
-36	Max	0.00	1	0.00	1	0.00	5	0.00	52	0.00	30	0.00	1
-36	Min.	0.00	1	0.00	1	0.00	13	0.00	1	0.00	5	0.00	1
-35	Max	0.00	1	0.00	1	0.00	31	0.00	9	0.00	1	0.00	1
-35	Min.	0.00	1	0.00	1	0.00	13	0.00	1	0.00	9	0.00	1
-34	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	22	0.00	1
-34	Min.	0.00	1	0.00	1	0.00	13	0.00	5	0.00	13	0.00	1
-33	Max	0.00	1	0.00	1	0.00	17	0.00	13	0.00	5	0.00	1
-33	Min.	0.00	1	0.00	1	0.00	5	0.00	31	0.00	13	0.00	1
-32	Max	0.00	1	0.00	1	0.00	25	0.00	5	0.00	5	0.00	1
-32	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	13	0.00	1
-31	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	5	0.00	1
-31	Min.	0.00	1	0.00	1	0.00	5	0.00	23	0.00	19	0.00	1
-30	Max	0.00	1	0.00	1	0.00	9	0.00	13	0.00	5	0.00	1
-30	Min.	0.00	1	0.00	1	0.00	23	0.00	5	0.00	23	0.00	1
-29	Max	0.00	1	0.00	1	0.00	9	0.00	13	0.00	5	0.00	1
-29	Min.	0.00	1	0.00	1	0.00	1	0.00	24	0.00	13	0.00	1
-28	Max	0.00	1	0.00	1	0.00	5	0.00	24	0.00	5	0.00	1
-28	Min.	0.00	1	0.00	1	0.00	13	0.00	9	0.00	13	0.00	1
-27	Max	0.00	1	0.00	1	0.00	1	0.00	5	0.00	1	0.00	1
-27	Min.	0.00	1	0.00	1	0.00	19	0.00	13	0.00	9	0.00	1
-26	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	13	0.00	1
-26	Min.	0.00	1	0.00	1	0.00	5	0.00	13	0.00	5	0.00	1
-25	Max	0.00	1	0.00	1	0.00	5	0.00	17	0.00	9	0.00	1
-25	Min.	0.00	1	0.00	1	0.00	13	0.00	5	0.00	1	0.00	1
-24	Max	0.00	1	0.00	1	0.00	56	0.00	31	0.00	1	0.00	1
-24	Min.	0.00	1	0.00	1	0.00	13	0.00	9	0.00	9	0.00	1
-23	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	13	0.00	1
-23	Min.	0.00	1	0.00	1	0.00	5	0.00	28	0.00	5	0.00	1
-22	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1
-22	Min.	0.00	1	0.00	1	0.00	20	0.00	25	0.00	13	0.00	1
-21	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	13	0.00	1
-21	Min.	0.00	1	0.00	1	0.00	24	0.00	55	0.00	5	0.00	1
-20	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	13	0.00	1
-20	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	5	0.00	1
-19	Max	0.00	1	0.00	1	0.00	23	0.00	13	0.00	20	0.00	1
-19	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1
-18	Max	0.00	1	0.00	1	0.00	13	0.00	5	0.00	23	0.00	1
-18	Min.	0.00	1	0.00	1	0.00	27	0.00	13	0.00	100	0.00	1
-17	Max	0.00	1	0.00	1	0.00	13	0.00	32	0.00	29	0.00	1
-17	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1
-16	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	13	0.00	1
-16	Min.	0.00	1	0.00	1	0.00	20	0.00	5	0.00	5	0.00	1
-15	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	13	0.00	1

-15	Min.	0.00	1	0.00	1	0.00	13	0.00	5	0.00	5	0.00	1
-14	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	5	0.00	1
-14	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	13	0.00	1
-13	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	13	0.00	1
-13	Min.	0.00	1	0.00	1	0.00	32	0.00	31	0.00	5	0.00	1
-12	Max	0.00	1	0.00	1	0.00	23	0.00	13	0.00	5	0.00	1
-12	Min.	0.00	1	0.00	1	0.00	13	0.00	5	0.00	32	0.00	1
-11	Max	0.00	1	0.00	1	0.00	24	0.00	13	0.00	5	0.00	1
-11	Min.	0.00	1	0.00	1	0.00	13	0.00	19	0.00	13	0.00	1
-10	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	13	0.00	1
-10	Min.	0.00	1	0.00	1	0.00	28	0.00	13	0.00	5	0.00	1
-9	Max	0.00	1	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1
-9	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	5	0.00	1
-8	Max	0.00	1	0.00	1	0.00	1	0.00	1	0.00	13	0.00	1
-8	Min.	0.00	1	0.00	1	0.00	20	0.00	9	0.00	31	0.00	1
-7	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	13	0.00	1
-7	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1
-6	Max	0.00	1	0.00	1	0.00	28	0.00	13	0.00	13	0.00	1
-6	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1
-5	Max	0.00	1	0.00	1	0.00	5	0.00	13	0.00	5	0.00	1
-5	Min.	0.00	1	0.00	1	0.00	13	0.00	5	0.00	13	0.00	1
-4	Max	0.00	1	0.00	1	0.00	13	0.00	13	0.00	13	0.00	1
-4	Min.	0.00	1	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1
-3	Max	0.00	1	0.00	1	0.00	32	0.00	5	0.00	1	0.00	1
-3	Min.	0.00	1	0.00	1	0.00	13	0.00	13	0.00	9	0.00	1
-2	Max	0.00	1	0.00	1	0.00	9	0.00	9	0.00	13	0.00	1
-2	Min.	0.00	1	0.00	1	0.00	1	0.00	1	0.00	5	0.00	1
-1	Max	0.00	1	0.00	1	0.00	1	0.00	13	0.00	1	0.00	1
-1	Min.	0.00	1	0.00	1	0.00	9	0.00	5	0.00	9	0.00	1
1	Max	2077.00	9	998.14	5	66893.60	20	17260.40	13	8681.41	9	392.81	13
1	Min.	-1297.50	1	-5312.09	13	35070.50	13	-7089.81	5	-5713.82	1	-1096.07	5
2	Max	1919.55	9	742.76	5	38935.90	20	18547.10	19	8421.45	9	395.42	13
2	Min.	-1484.84	1	-4326.68	19	23446.10	13	-4043.46	5	-6022.60	1	-1103.35	5
6	Max	1799.22	1	1661.38	5	36432.40	17	16025.40	19	8995.01	1	395.42	13
6	Min.	-681.63	9	-3166.00	19	22897.70	1	-8186.34	5	-3407.84	9	-1103.35	5
7	Max	1798.96	1	870.20	5	29981.80	17	16949.90	19	8994.57	1	395.42	13
7	Min.	-681.65	9	-3357.95	19	18420.50	1	-4254.97	5	-3407.87	9	-1103.35	5
8	Max	1799.20	1	190.54	5	24496.20	17	17893.10	19	8994.97	1	395.42	13
8	Min.	-681.73	9	-3553.01	19	15079.00	1	-876.22	5	-3408.00	9	-1103.35	5
9	Max	1799.22	1	-163.83	13	18712.90	17	18811.40	19	8995.00	1	395.42	13
9	Min.	-681.74	9	-3743.43	19	11559.80	1	875.07	13	-3408.02	9	-1103.35	5
10	Max	1799.20	1	-189.97	13	18652.60	17	19714.30	19	8994.98	1	395.42	13
10	Min.	-681.74	9	-3924.51	19	12930.90	1	1012.12	13	-3408.01	9	-1103.35	5
11	Max	294.23	1	-282.45	5	21886.00	19	4310.57	27	1469.01	1	1493.91	13
11	Min.	-79.12	9	-7976.08	19	10872.10	5	-1934.71	5	-395.72	9	-4168.49	5
12	Max	-2037.39	1	3433.52	5	0.00	9	0.00	13	0.00	5	269.16	13
12	Min.	-3980.08	17	-753.21	13	0.00	1	0.00	5	0.00	17	-950.09	5
13	Max	2593.06	1	2187.47	5	48716.70	17	14356.70	19	12223.30	1	395.42	13
13	Min.	-1382.45	9	-2915.12	13	25432.30	1	-6425.25	5	-4420.32	9	-1103.35	5
14	Max	2618.86	1	1646.01	5	39608.60	19	13045.10	27	12265.80	1	395.42	13
14	Min.	-865.82	9	-2153.85	13	23971.30	5	-3275.88	5	-3568.53	9	-1103.35	5
15	Max	2723.51	1	295.72	13	29653.40	19	16990.50	19	12438.40	1	395.42	13
15	Min.	-931.74	9	-3516.14	5	17994.70	13	117.52	13	-3677.23	9	-1103.35	5
16	Max	2547.47	1	545.89	13	31520.00	19	17435.90	5	12148.10	1	395.42	13
16	Min.	-985.98	9	-4279.86	5	19159.50	13	-199.29	13	-3766.64	9	-1103.35	5

TENSIONI SUL TERRENO

Simbologia

Nodo = Numero del nodo
σ_t = Tensione sul terreno
CC = Numero della combinazione delle condizioni di carico elementari

Nodo	σ_t	CC	Nodo	σ_t	CC	Nodo	σ_t	CC	Nodo	σ_t	CC
	<daN/cmq>			<daN/cmq>			<daN/cmq>			<daN/cmq>	
-1680	Max 1.54	19	-1680	Min. 0.96	1	-1679	Max 1.59	18	-1679	Min. 1.03	9
-1678	Max 1.65	18									

-1678 Min.	1.00 9	-1677 Max	1.70 34	-1677 Min.	0.97 9	-1676 Max	1.76 34
-1676 Min.	0.94 9						
-1675 Max	1.82 34	-1675 Min.	0.91 9	-1648 Max	2.30 19	-1648 Min.	1.00 5
-1644 Max	1.00 17						
-1644 Min.	0.69 1	-1643 Max	1.00 17	-1643 Min.	0.69 1	-1639 Max	2.10 19
-1639 Min.	1.16 5						
-1636 Max	1.00 17	-1636 Min.	0.69 1	-1632 Max	1.00 17	-1632 Min.	0.69 1
-1628 Max	1.93 36						
-1628 Min.	1.19 13	-1625 Max	1.00 17	-1625 Min.	0.69 1	-1621 Max	1.00 17
-1621 Min.	0.69 1						
-1620 Max	1.83 36	-1620 Min.	1.01 13	-1617 Max	1.00 17	-1617 Min.	0.69 1
-1613 Max	1.00 17						
-1613 Min.	0.69 1	-1591 Max	1.73 36	-1591 Min.	0.83 13	-1587 Max	1.00 17
-1587 Min.	0.69 1						
-850 Max	1.06 17	-850 Min.	0.20 9	-849 Max	1.07 17	-849 Min.	0.24 9
-848 Max	1.09 17						
-848 Min.	0.27 9	-847 Max	1.11 17	-847 Min.	0.30 9	-846 Max	1.13 17
-846 Min.	0.34 9						
-845 Max	1.15 17	-845 Min.	0.37 9	-844 Max	1.16 17	-844 Min.	0.40 13
-843 Max	1.18 19						
-843 Min.	0.41 13	-842 Max	1.19 19	-842 Min.	0.43 13	-841 Max	1.21 19
-841 Min.	0.45 13						
-840 Max	1.23 19	-840 Min.	0.47 13	-839 Max	1.24 19	-839 Min.	0.48 13
-838 Max	1.25 19						
-838 Min.	0.50 13	-837 Max	1.27 19	-837 Min.	0.51 13	-836 Max	1.28 19
-836 Min.	0.52 13						
-835 Max	1.30 19	-835 Min.	0.53 13	-834 Max	1.31 19	-834 Min.	0.52 13
-833 Max	1.32 19						
-833 Min.	0.52 13	-832 Max	1.33 19	-832 Min.	0.52 13	-831 Max	1.35 19
-831 Min.	0.52 13						
-830 Max	1.36 19	-830 Min.	0.51 5	-829 Max	1.37 19	-829 Min.	0.50 5
-828 Max	1.38 19						
-828 Min.	0.49 1	-827 Max	1.39 19	-827 Min.	0.47 1	-826 Max	1.40 19
-826 Min.	0.45 1						
-825 Max	1.41 19	-825 Min.	0.43 1	-824 Max	1.32 19	-824 Min.	0.52 13
-823 Max	1.13 17						
-823 Min.	0.38 9	-822 Max	1.31 19	-822 Min.	0.52 13	-821 Max	1.08 17
-821 Min.	0.28 9						
-820 Max	1.14 17	-820 Min.	0.40 13	-819 Max	1.30 19	-819 Min.	0.52 13
-818 Max	1.20 19						
-818 Min.	0.47 13	-817 Max	1.09 17	-817 Min.	0.30 9	-816 Max	1.15 19
-816 Min.	0.41 13						
-815 Max	1.06 17	-815 Min.	0.25 9	-814 Max	1.28 19	-814 Min.	0.52 13
-813 Max	1.27 19						
-813 Min.	0.52 13	-812 Max	1.21 19	-812 Min.	0.48 13	-811 Max	1.16 19
-811 Min.	0.43 13						
-810 Max	1.10 17	-810 Min.	0.33 9	-809 Max	1.04 17	-809 Min.	0.21 9
-808 Max	1.33 19						
-808 Min.	0.50 5	-807 Max	1.22 19	-807 Min.	0.49 13	-806 Max	1.32 19
-806 Min.	0.51 5						
-805 Max	1.17 19	-805 Min.	0.44 13	-804 Max	1.06 17	-804 Min.	0.26 9
-803 Max	1.23 19						
-803 Min.	0.51 13	-802 Max	1.11 17	-802 Min.	0.36 9	-801 Max	1.31 19
-801 Min.	0.51 13						
-800 Max	1.04 17	-800 Min.	0.23 9	-799 Max	1.18 19	-799 Min.	0.46 13
-798 Max	1.24 19						
-798 Min.	0.52 13	-797 Max	1.29 19	-797 Min.	0.52 13	-796 Max	1.07 17
-796 Min.	0.28 9						
-795 Max	1.11 17	-795 Min.	0.38 9	-794 Max	1.28 19	-794 Min.	0.52 13
-793 Max	1.12 17						
-793 Min.	0.40 9	-792 Max	1.18 19	-792 Min.	0.47 13	-791 Max	1.04 17
-791 Min.	0.24 9						
-790 Max	1.27 19	-790 Min.	0.52 13	-789 Max	1.07 17	-789 Min.	0.30 9
-788 Max	1.33 19						
-788 Min.	0.48 1	-787 Max	1.12 17	-787 Min.	0.41 13	-786 Max	1.32 19
-786 Min.	0.50 1						
-785 Max	1.23 19	-785 Min.	0.52 13	-784 Max	1.34 19	-784 Min.	0.46 1
-783 Max	1.25 19						
-783 Min.	0.52 13	-782 Max	1.02 17	-782 Min.	0.21 9	-781 Max	1.24 19
-781 Min.	0.52 13						
-780 Max	1.17 19	-780 Min.	0.48 13	-779 Max	1.07 17	-779 Min.	0.32 9
-778 Max	1.13 19						
-778 Min.	0.43 13	-777 Max	1.30 19	-777 Min.	0.50 5	-776 Max	1.04 17

-776 Min.	0.25 9						
-775 Max	1.18 19	-775 Min.	0.49 13	-774 Max	1.14 19	-774 Min.	0.44 13
-773 Max	1.29 19						
-773 Min.	0.51 5	-772 Max	1.02 17	-772 Min.	0.22 9	-771 Max	1.08 17
-771 Min.	0.34 9						
-770 Max	1.19 19	-770 Min.	0.50 13	-769 Max	1.28 19	-769 Min.	0.51 13
-768 Max	1.15 19						
-768 Min.	0.46 13	-767 Max	1.04 17	-767 Min.	0.27 9	-766 Max	1.20 19
-766 Min.	0.51 13						
-765 Max	1.27 19	-765 Min.	0.51 13	-764 Max	1.09 17	-764 Min.	0.37 9
-763 Max	1.02 17						
-763 Min.	0.23 9	-762 Max	1.15 19	-762 Min.	0.47 13	-761 Max	1.26 19
-761 Min.	0.52 13						
-760 Max	1.05 17	-760 Min.	0.29 9	-759 Max	1.09 17	-759 Min.	0.40 9
-758 Max	1.25 19						
-758 Min.	0.52 13	-757 Max	1.21 19	-757 Min.	0.52 13	-756 Max	1.10 17
-756 Min.	0.41 13						
-755 Max	1.35 19	-755 Min.	0.41 1	-754 Max	1.34 19	-754 Min.	0.44 1
-753 Max	1.00 17						
-753 Min.	0.19 9	-752 Max	1.00 17	-752 Min.	0.21 9	-751 Max	1.01 17
-751 Min.	0.24 9						
-750 Max	1.02 17	-750 Min.	0.27 9	-749 Max	1.03 17	-749 Min.	0.30 9
-748 Max	1.05 17						
-748 Min.	0.33 9	-747 Max	1.06 17	-747 Min.	0.36 9	-746 Max	1.07 17
-746 Min.	0.40 9						
-745 Max	1.08 19	-745 Min.	0.42 13	-744 Max	1.10 19	-744 Min.	0.44 13
-743 Max	1.11 19						
-743 Min.	0.46 13	-742 Max	1.13 19	-742 Min.	0.47 13	-741 Max	1.14 19
-741 Min.	0.49 13						
-740 Max	1.16 19	-740 Min.	0.50 13	-739 Max	1.17 19	-739 Min.	0.51 13
-738 Max	1.18 19						
-738 Min.	0.52 13	-737 Max	1.19 19	-737 Min.	0.52 13	-736 Max	1.20 19
-736 Min.	0.52 13						
-735 Max	1.21 19	-735 Min.	0.52 13	-734 Max	1.23 19	-734 Min.	0.51 13
-733 Max	1.24 19						
-733 Min.	0.51 13	-732 Max	1.25 19	-732 Min.	0.51 13	-731 Max	1.26 19
-731 Min.	0.51 5						
-730 Max	1.27 19	-730 Min.	0.50 5	-729 Max	1.28 19	-729 Min.	0.49 1
-728 Max	1.29 19						
-728 Min.	0.47 1	-727 Max	1.30 19	-727 Min.	0.45 1	-726 Max	1.32 19
-726 Min.	0.44 1						
-725 Max	1.21 19	-725 Min.	0.50 1	-724 Max	1.20 19	-724 Min.	0.51 13
-723 Max	1.22 19						
-723 Min.	0.49 1	-722 Max	1.11 19	-722 Min.	0.51 13	-721 Max	1.28 19
-721 Min.	0.40 1						
-720 Max	0.95 17	-720 Min.	0.18 9	-719 Max	1.27 19	-719 Min.	0.41 1
-718 Max	1.22 19						
-718 Min.	0.48 1	-717 Max	1.17 19	-717 Min.	0.51 13	-716 Max	1.12 19
-716 Min.	0.51 13						
-715 Max	1.23 19	-715 Min.	0.46 1	-714 Max	1.15 19	-714 Min.	0.51 13
-713 Max	1.24 19						
-713 Min.	0.44 1	-712 Max	1.13 19	-712 Min.	0.51 13	-711 Max	0.95 17
-711 Min.	0.20 9						
-710 Max	0.97 17	-710 Min.	0.28 9	-709 Max	1.11 19	-709 Min.	0.51 13
-708 Max	1.25 19						
-708 Min.	0.42 1	-707 Max	1.09 19	-707 Min.	0.50 13	-706 Max	1.07 19
-706 Min.	0.49 13						
-705 Max	0.98 17	-705 Min.	0.34 9	-704 Max	1.05 19	-704 Min.	0.48 13
-703 Max	0.98 17						
-703 Min.	0.37 9	-702 Max	0.97 17	-702 Min.	0.32 9	-701 Max	1.03 19
-701 Min.	0.47 13						
-700 Max	0.95 17	-700 Min.	0.23 9	-699 Max	0.95 17	-699 Min.	0.25 9
-698 Max	0.99 17						
-698 Min.	0.40 9	-697 Max	1.00 19	-697 Min.	0.43 9	-696 Max	1.02 19
-696 Min.	0.45 13						
-695 Max	1.08 19	-695 Min.	0.50 13	-694 Max	1.08 19	-694 Min.	0.50 13
-693 Max	1.07 19						
-693 Min.	0.50 13	-692 Max	1.15 19	-692 Min.	0.50 9	-691 Max	1.17 19
-691 Min.	0.48 1						
-690 Max	1.16 19	-690 Min.	0.49 9	-689 Max	0.94 17	-689 Min.	0.29 9
-688 Max	1.05 19						
-688 Min.	0.50 13	-687 Max	1.05 19	-687 Min.	0.50 13	-686 Max	1.04 19
-686 Min.	0.50 13						

-685 Max	0.92 17	-685 Min.	0.23 9	-684 Max	0.92 17	-684 Min.	0.24 9
-683 Max	1.11 19						
-683 Min.	0.50 9	-682 Max	1.15 19	-682 Min.	0.47 1	-681 Max	1.04 19
-681 Min.	0.50 13						
-680 Max	1.05 19	-680 Min.	0.50 13	-679 Max	1.02 19	-679 Min.	0.50 13
-678 Max	1.21 18						
-678 Min.	0.38 1	-677 Max	1.16 19	-677 Min.	0.45 1	-676 Max	1.20 18
-676 Min.	0.40 1						
-675 Max	1.07 19	-675 Min.	0.50 13	-674 Max	1.17 18	-674 Min.	0.43 1
-673 Max	1.05 19						
-673 Min.	0.50 13	-672 Max	0.90 17	-672 Min.	0.19 9	-671 Max	0.90 17
-671 Min.	0.26 9						
-670 Max	1.19 18	-670 Min.	0.41 1	-669 Max	0.90 17	-669 Min.	0.18 9
-668 Max	1.11 19						
-668 Min.	0.48 9	-667 Max	1.01 19	-667 Min.	0.49 13	-666 Max	0.90 17
-666 Min.	0.21 9						
-665 Max	0.89 17	-665 Min.	0.24 9	-664 Max	0.90 17	-664 Min.	0.30 9
-663 Max	0.90 17						
-663 Min.	0.28 9	-662 Max	0.98 19	-662 Min.	0.49 13	-661 Max	0.89 17
-661 Min.	0.22 9						
-660 Max	0.88 17	-660 Min.	0.23 9	-659 Max	0.89 17	-659 Min.	0.32 9
-658 Max	0.96 19						
-658 Min.	0.47 13	-657 Max	0.90 17	-657 Min.	0.35 9	-656 Max	0.90 17
-656 Min.	0.37 9						
-655 Max	0.91 17	-655 Min.	0.40 9	-654 Max	0.93 19	-654 Min.	0.43 9
-653 Max	0.94 19						
-653 Min.	0.46 13	-652 Max	0.99 19	-652 Min.	0.49 5	-651 Max	0.95 19
-651 Min.	0.48 5						
-650 Max	0.96 19	-650 Min.	0.48 5	-649 Max	0.95 19	-649 Min.	0.48 5
-648 Max	0.85 17						
-648 Min.	0.29 9	-647 Max	1.03 19	-647 Min.	0.48 9	-646 Max	0.84 17
-646 Min.	0.27 9						
-645 Max	1.07 18	-645 Min.	0.45 9	-644 Max	1.09 18	-644 Min.	0.44 1
-643 Max	1.00 19						
-643 Min.	0.48 9	-642 Max	0.86 17	-642 Min.	0.19 9	-641 Max	0.83 17
-641 Min.	0.25 9						
-640 Max	1.11 18	-640 Min.	0.42 1	-639 Max	1.13 18	-639 Min.	0.40 1
-638 Max	1.05 18						
-638 Min.	0.47 9	-637 Max	1.14 18	-637 Min.	0.38 1	-636 Max	0.85 17
-636 Min.	0.20 9						
-635 Max	0.83 17	-635 Min.	0.23 9	-634 Max	1.14 18	-634 Min.	0.37 1
-633 Max	0.84 17						
-633 Min.	0.21 9	-632 Max	0.83 17	-632 Min.	0.22 9	-631 Max	0.96 19
-631 Min.	0.48 5						
-630 Max	0.85 1	-630 Min.	0.17 9	-629 Max	0.90 19	-629 Min.	0.46 5
-628 Max	0.81 17						
-628 Min.	0.29 9	-627 Max	0.81 17	-627 Min.	0.32 9	-626 Max	0.82 17
-626 Min.	0.35 9						
-625 Max	0.83 17	-625 Min.	0.38 9	-624 Max	0.85 19	-624 Min.	0.43 1
-623 Max	0.84 19						
-623 Min.	0.41 9	-622 Max	0.86 19	-622 Min.	0.45 5	-621 Max	0.88 19
-621 Min.	0.45 5						
-620 Max	0.89 19	-620 Min.	0.45 5	-619 Max	0.78 17	-619 Min.	0.25 9
-618 Max	0.86 19						
-618 Min.	0.44 5	-617 Max	0.97 18	-617 Min.	0.46 9	-616 Max	0.79 17
-616 Min.	0.20 9						
-615 Max	0.78 17	-615 Min.	0.20 9	-614 Max	0.93 19	-614 Min.	0.46 9
-613 Max	0.80 17						
-613 Min.	0.19 9	-612 Max	0.77 17	-612 Min.	0.21 9	-611 Max	0.86 19
-611 Min.	0.44 5						
-610 Max	0.81 17	-610 Min.	0.18 9	-609 Max	0.77 17	-609 Min.	0.23 9
-608 Max	1.05 18						
-608 Min.	0.40 1	-607 Max	1.07 18	-607 Min.	0.38 1	-606 Max	1.04 18
-606 Min.	0.42 9						
-605 Max	1.02 18	-605 Min.	0.44 9	-604 Max	0.84 19	-604 Min.	0.43 5
-603 Max	1.07 18						
-603 Min.	0.37 1	-602 Max	0.85 19	-602 Min.	0.43 5	-601 Max	0.86 19
-601 Min.	0.43 5						
-600 Max	0.98 18	-600 Min.	0.45 9	-599 Max	0.86 19	-599 Min.	0.44 5
-598 Max	1.07 18						
-598 Min.	0.35 1	-597 Max	0.84 19	-597 Min.	0.43 5	-596 Max	0.88 19
-596 Min.	0.46 1						
-595 Max	0.81 1	-595 Min.	0.16 9	-594 Max	0.86 19	-594 Min.	0.45 5

-593 Max	0.83 19						
-593 Min.	0.42 5	-592 Max	0.83 19	-592 Min.	0.42 5	-591 Max	0.81 19
-591 Min.	0.42 5						
-590 Max	0.83 19	-590 Min.	0.42 5	-589 Max	0.81 19	-589 Min.	0.41 5
-588 Max	0.83 19						
-588 Min.	0.42 5	-587 Max	0.92 18	-587 Min.	0.45 9	-586 Max	0.89 18
-586 Min.	0.45 9						
-585 Max	0.81 19	-585 Min.	0.41 5	-584 Max	0.94 18	-584 Min.	0.45 9
-583 Max	0.86 18						
-583 Min.	0.45 1	-582 Max	0.75 1	-582 Min.	0.19 9	-581 Max	0.74 1
-581 Min.	0.19 9						
-580 Max	0.72 17	-580 Min.	0.27 9	-579 Max	0.73 17	-579 Min.	0.30 9
-578 Max	0.74 17						
-578 Min.	0.33 9	-577 Max	0.79 19	-577 Min.	0.41 5	-576 Max	0.75 17
-576 Min.	0.35 1						
-575 Max	0.76 17	-575 Min.	0.38 1	-574 Max	0.77 19	-574 Min.	0.40 1
-573 Max	0.81 19						
-573 Min.	0.41 5	-572 Max	0.81 19	-572 Min.	0.40 5	-571 Max	0.75 1
-571 Min.	0.18 9						
-570 Max	0.73 1	-570 Min.	0.19 9	-569 Max	0.71 17	-569 Min.	0.23 9
-568 Max	0.80 19						
-568 Min.	0.40 5	-567 Max	0.77 1	-567 Min.	0.17 9	-566 Max	0.71 1
-566 Min.	0.21 9						
-565 Max	0.99 18	-565 Min.	0.39 1	-564 Max	1.01 18	-564 Min.	0.37 1
-563 Max	0.98 18						
-563 Min.	0.41 9	-562 Max	0.96 18	-562 Min.	0.43 9	-561 Max	0.79 19
-561 Min.	0.39 5						
-560 Max	0.81 19	-560 Min.	0.43 1	-559 Max	0.79 19	-559 Min.	0.40 5
-558 Max	0.94 18						
-558 Min.	0.44 9	-557 Max	1.01 18	-557 Min.	0.35 1	-556 Max	0.77 19
-556 Min.	0.39 5						
-555 Max	0.82 19	-555 Min.	0.43 1	-554 Max	0.78 19	-554 Min.	0.38 5
-553 Max	0.91 18						
-553 Min.	0.44 9	-552 Max	0.82 18	-552 Min.	0.43 1	-551 Max	1.00 18
-551 Min.	0.33 1						
-550 Max	1.01 18	-550 Min.	0.31 1	-549 Max	1.02 18	-549 Min.	0.29 1
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-288 Max	0.33 34						
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-165 Max	0.47	1	-165 Min.	0.14	9	-164 Max	0.20	13	-164 Min.	0.10	5
-163 Max	0.24	13									
-163 Min.	0.12	5	-162 Max	0.21	13	-162 Min.	0.10	5	-161 Max	0.23	13
-161 Min.	0.11	5									
-160 Max	0.22	13	-160 Min.	0.11	5	-159 Max	0.48	1	-159 Min.	0.13	9
-158 Max	0.31	9									
-158 Min.	0.03	1	-157 Max	0.28	9	-157 Min.	0.03	1	-156 Max	0.42	1
-156 Min.	0.12	9									
-155 Max	0.27	9	-155 Min.	0.04	1	-154 Max	0.26	9	-154 Min.	0.04	1
-153 Max	0.24	9									
-153 Min.	0.05	1	-152 Max	0.40	1	-152 Min.	0.13	9	-151 Max	0.23	13
-151 Min.	0.06	5									
-150 Max	0.22	13	-150 Min.	0.06	5	-149 Max	0.22	13	-149 Min.	0.06	5
-148 Max	0.37	1									
-148 Min.	0.13	9	-147 Max	0.21	13	-147 Min.	0.07	5	-146 Max	0.21	13
-146 Min.	0.07	5									
-145 Max	0.35	1	-145 Min.	0.12	9	-144 Max	0.21	13	-144 Min.	0.07	5
-143 Max	0.21	13									
-143 Min.	0.08	5	-142 Max	0.32	1	-142 Min.	0.12	9	-141 Max	0.21	13
-141 Min.	0.08	5									
-140 Max	0.30	1	-140 Min.	0.12	9	-139 Max	0.21	13	-139 Min.	0.09	5
-138 Max	0.28	1									

-138 Min.	0.12 9	-137 Max	0.21 13	-137 Min.	0.09 5	-136 Max	0.26 13
-136 Min.	0.12 5						
-135 Max	0.22 13	-135 Min.	0.09 5	-134 Max	0.25 13	-134 Min.	0.11 5
-133 Max	0.22 13						
-133 Min.	0.10 5	-132 Max	0.23 13	-132 Min.	0.10 5	-131 Max	0.24 13
-131 Min.	0.11 5						
-130 Max	0.43 1	-130 Min.	0.12 9	-129 Max	0.44 1	-129 Min.	0.12 9
-128 Max	0.28 9						
-128 Min.	0.01 1	-127 Max	0.25 9	-127 Min.	0.01 1	-126 Max	0.39 1
-126 Min.	0.11 9						
-125 Max	0.24 13	-125 Min.	0.02 5	-124 Max	0.24 13	-124 Min.	0.02 5
-123 Max	0.37 1						
-123 Min.	0.11 9	-122 Max	0.23 13	-122 Min.	0.03 5	-121 Max	0.23 13
-121 Min.	0.03 5						
-120 Max	0.23 13	-120 Min.	0.04 5	-119 Max	0.23 13	-119 Min.	0.05 5
-118 Max	0.35 1						
-118 Min.	0.11 9	-117 Max	0.22 13	-117 Min.	0.05 5	-116 Max	0.22 13
-116 Min.	0.06 5						
-115 Max	0.33 1	-115 Min.	0.11 9	-114 Max	0.22 13	-114 Min.	0.06 5
-113 Max	0.22 13						
-113 Min.	0.07 5	-112 Max	0.31 1	-112 Min.	0.11 9	-111 Max	0.22 13
-111 Min.	0.08 5						
-110 Max	0.30 1	-110 Min.	0.11 9	-109 Max	0.22 13	-109 Min.	0.08 5
-108 Max	0.28 5						
-108 Min.	0.11 13	-107 Max	0.23 13	-107 Min.	0.08 5	-106 Max	0.27 13
-106 Min.	0.11 5						
-105 Max	0.23 13	-105 Min.	0.09 5	-104 Max	0.26 13	-104 Min.	0.10 5
-103 Max	0.24 13						
-103 Min.	0.09 5	-102 Max	0.25 13	-102 Min.	0.09 5	-101 Max	0.26 13
-101 Min.	0.10 5						
-100 Max	0.39 1	-100 Min.	0.10 9	-99 Max	0.40 1	-99 Min.	0.10 9
-98 Max	0.24 9						
-98 Min.	-0.01 1	-97 Max	0.23 13	-97 Min.	-0.03 5	-96 Max	0.23 13
-96 Min.	-0.02 5						
-95 Max	0.23 13	-95 Min.	-0.01 5	-94 Max	0.23 13	-94 Min.	-0.00 5
-93 Max	0.23 13						
-93 Min.	0.01 5	-92 Max	0.23 13	-92 Min.	0.02 5	-91 Max	0.23 13
-91 Min.	0.03 5						
-90 Max	0.23 13	-90 Min.	0.03 5	-89 Max	0.23 13	-89 Min.	0.04 5
-88 Max	0.23 13						
-88 Min.	0.05 5	-87 Max	0.23 13	-87 Min.	0.06 5	-86 Max	0.23 13
-86 Min.	0.07 5						
-85 Max	0.24 13	-85 Min.	0.07 5	-84 Max	0.24 13	-84 Min.	0.08 5
-83 Max	0.25 13						
-83 Min.	0.08 5	-82 Max	0.25 13	-82 Min.	0.08 5	-81 Max	0.26 13
-81 Min.	0.08 5						
-80 Max	0.27 13	-80 Min.	0.09 5	-79 Max	0.27 13	-79 Min.	0.09 5
-78 Max	0.28 5						
-78 Min.	0.09 13	-77 Max	0.29 5	-77 Min.	0.09 13	-76 Max	0.29 5
-76 Min.	0.09 13						
-75 Max	0.30 5	-75 Min.	0.10 13	-74 Max	0.31 5	-74 Min.	0.10 13
-73 Max	0.32 1						
-73 Min.	0.09 9	-72 Max	0.34 1	-72 Min.	0.09 9	-71 Max	0.35 1
-71 Min.	0.09 9						
-70 Max	0.35 1	-70 Min.	0.08 9	-69 Max	0.36 1	-69 Min.	0.08 9
-68 Max	0.23 13						
-68 Min.	-0.04 5	-67 Max	0.23 13	-67 Min.	-0.03 5	-66 Max	0.23 13
-66 Min.	-0.03 5						
-65 Max	0.23 13	-65 Min.	-0.04 5	-64 Max	0.23 13	-64 Min.	-0.03 5
-63 Max	0.23 13						
-63 Min.	-0.02 5	-62 Max	0.22 13	-62 Min.	-0.05 5	-61 Max	0.23 13
-61 Min.	-0.02 5						
-60 Max	0.23 13	-60 Min.	-0.01 5	-59 Max	0.22 13	-59 Min.	-0.04 5
-58 Max	0.23 13						
-58 Min.	-0.00 5	-57 Max	0.23 13	-57 Min.	0.01 5	-56 Max	0.23 13
-56 Min.	0.02 5						
-55 Max	0.23 13	-55 Min.	0.03 5	-54 Max	0.24 13	-54 Min.	0.04 5
-53 Max	0.24 13						
-53 Min.	0.05 5	-52 Max	0.24 13	-52 Min.	0.06 5	-51 Max	0.24 13
-51 Min.	0.06 5						
-50 Max	0.25 13	-50 Min.	0.07 5	-49 Max	0.25 13	-49 Min.	0.07 5
-48 Max	0.26 13						
-48 Min.	0.07 5	-47 Max	0.27 13	-47 Min.	0.08 5	-46 Max	0.27 13

-46 Min. 0.08 5
  -45 Max 0.28 13 -45 Min. 0.08 5 -44 Max 0.28 5 -44 Min. 0.08 13
-43 Max 0.29 5
  -43 Min. 0.08 13 -42 Max 0.29 5 -42 Min. 0.08 13 -41 Max 0.30 5
-41 Min. 0.08 13
  -40 Max 0.30 5 -40 Min. 0.08 13 -39 Max 0.31 5 -39 Min. 0.08 13
-38 Max 0.32 5
  -38 Min. 0.08 13 -37 Max 0.32 1 -37 Min. 0.08 9 -36 Max 0.22 13
-36 Min. -0.03 5
  -35 Max 0.22 13 -35 Min. -0.05 5 -34 Max 0.22 13 -34 Min. -0.04 5
-33 Max 0.22 13
  -33 Min. -0.06 5 -32 Max 0.22 13 -32 Min. -0.03 5 -31 Max 0.22 13
-31 Min. -0.03 5
  -30 Max 0.22 13 -30 Min. -0.05 5 -29 Max 0.22 13 -29 Min. -0.04 5
-28 Max 0.21 13
  -28 Min. -0.08 5 -27 Max 0.22 13 -27 Min. -0.07 5 -26 Max 0.22 13
-26 Min. -0.06 5
  -25 Max 0.22 13 -25 Min. -0.05 5 -24 Max 0.22 13 -24 Min. -0.03 5
-23 Max 0.23 13
  -23 Min. -0.02 5 -22 Max 0.23 13 -22 Min. -0.01 5 -21 Max 0.23 13
-21 Min. 0.00 5
  -20 Max 0.24 13 -20 Min. 0.02 5 -19 Max 0.24 13 -19 Min. 0.03 5
-18 Max 0.24 13
  -18 Min. 0.04 5 -17 Max 0.25 13 -17 Min. 0.05 5 -16 Max 0.25 13
-16 Min. 0.05 5
  -15 Max 0.26 13 -15 Min. 0.06 5 -14 Max 0.26 13 -14 Min. 0.06 5
-13 Max 0.27 13
  -13 Min. 0.06 5 -12 Max 0.27 13 -12 Min. 0.07 5 -11 Max 0.27 13
-11 Min. 0.07 5
  -10 Max 0.28 13 -10 Min. 0.07 5 -9 Max 0.28 5 -9 Min. 0.07 13
-8 Max 0.29 5
  -8 Min. 0.07 13 -7 Max 0.29 5 -7 Min. 0.07 13 -6 Max 0.29 5
-6 Min. 0.07 13
  -5 Max 0.30 5 -5 Min. 0.06 13 -4 Max 0.30 5 -4 Min. 0.06 13
-3 Max 0.31 5
  -3 Min. 0.06 13 -2 Max 0.31 5 -2 Min. 0.06 13 -1 Max 0.32 5
-1 Min. 0.06 13
  12 Max 1.88 34 12 Min. 0.88 9

Elenco unità geotecniche

1 :
Classificazione: Coesivo

Pesi:
- Peso specifico del terreno naturale: γ = 1800.00 daN/mc
- Peso specifico del terreno saturo: γ_{sat} = 2000.00 daN/mc
Parametri plastici:
- Angolo di attrito efficace: ϕ' = 30.37 grad
  correlata alla stratigrafia 1
  valutata come valore medio risultante dalle seguenti correlazioni:

Correlazione	ϕ' <grad>
Terzaghi e Peck (1948)	30.37

- Coesione efficace: c' = 500.00 daN/mq
- Coesione non drenata: c_u = 5500.00 daN/mq
Caratteristiche litostatiche:
- Grado di sovraconsolidazione: OCR = 8.33
  correlata alla stratigrafia 1
  valutata come valore medio risultante dalle seguenti correlazioni:

Correlazione	OCR
SPT Mayne e Kemper (1988)	8.33

- Coeff. di spinta a riposo: κ_0 = 1.30
  calcolato utilizzando le seguenti opzioni:
  -Calcolo di k0 Brooker e Ireland (1965)
  -Calcolo di α Kulhawy (1989)

Parametri elastici:
- Modulo elastico normale: E = 450000.00 daN/mq
- Modulo elastico tangenziale: G = 173077.00 daN/mq
- Esponente del parametro tensionale: k_j = 0.00
- Coeff. di Poisson: ν = 0.30
- Modulo edometrico: E_{ed} = 605769.00 daN/mq
- Modulo elastico non drenato: E_u = 519231.00 daN/mq
  correlati alla stratigrafia 1
  Tipo di prova SPT, Stroud 1989
  Fattore elastico riduzione modulo secante: 1.00

2 :
Classificazione: Incoerente

Pesi:
- Peso specifico del terreno naturale: γ = 1800.00 daN/mc
- Peso specifico del terreno saturo: γ_{sat} = 2000.00 daN/mc
Parametri plastici:
- Angolo di attrito efficace: ϕ' = 31.99 grad
  correlata alla stratigrafia 1
  valutata come valore medio risultante dalle seguenti correlazioni:

Correlazione	ϕ' <grad>
Terzaghi e Peck (1948)	31.99

- Coesione efficace: c' = 500.00 daN/mq
Caratteristiche litostatiche:
- Grado di sovraconsolidazione: OCR = 5.69
  correlata alla stratigrafia 1
  valutata come valore medio risultante dalle seguenti correlazioni:

Correlazione	OCR
SPT Mayne e Kemper (1988)	5.69

- Coeff. di spinta a riposo: κ_0 = 1.06
  calcolato utilizzando le seguenti opzioni:
  -Calcolo di k0 Brooker e Ireland (1965)
  -Calcolo di α Kulhawy (1989)

Parametri elastici:
- Modulo elastico normale: E = 600000.00 daN/mq
- Modulo elastico tangenziale: G = 230769.00 daN/mq
- Esponente del parametro tensionale: k_j = 0.00
- Coeff. di Poisson: ν = 0.30
- Modulo edometrico: E_{ed} = 807692.00 daN/mq
- Modulo elastico non drenato: E_u = 0.00 daN/mq

Elenco colonne stratigrafiche

Prove in sito

Report grafico complessivo
Le verifiche degli elementi di fondazione sono state effettuate utilizzando l'approccio 2.

Coefficienti parziali per le azioni, per verifiche in condizioni statiche:
Permanenti strutturali, sicurezza a favore γ_A = 1.00;
Permanenti strutturali, sicurezza a sfavore γ_A = 1.30;
Permanenti non strutturali, sicurezza a favore γ_A = 0.00;
Permanenti non strutturali, sicurezza a sfavore γ_A = 1.50;
Variabili, sicurezza a favore γ_A = 0.00;
Variabili, sicurezza a sfavore γ_A = 1.50.

I coefficienti parziali per le azioni sono posti pari all'unità per le verifiche in condizioni sismiche.

Tali coefficienti sono comunque desumibili dalla tabella delle combinazioni delle CCE (Parametri di calcolo).

Coefficienti parziali per i parametri geotecnici:

Tangente dell'angolo di attrito γ_M = 1.00;
Coesione efficace γ_M = 1.00;
Coesione non drenata γ_M = 1.00;

Coefficienti parziali per la resistenza delle fondazioni superficiali:
Capacità portante γ_R = 2.30;
Scorrimento γ_R = 1.10;

Coefficienti parziali per la resistenza delle fondazioni profonde:
Per pali infissi:
Resistenza alla base γ_R,b = 1.15;
Resistenza laterale in compressione γ_R,s = 1.15;
Resistenza laterale in trazione γ_R,t = 1.25;
Per pali trivellati:
Resistenza alla base γ_R,b = 1.35;
Resistenza laterale in compressione γ_R,s = 1.15;
Resistenza laterale in trazione γ_R,t = 1.25;
Per pali ad elica continua:
Resistenza alla base γ_R,b = 1.30;
Resistenza laterale in compressione γ_R,s = 1.15;
Resistenza laterale in trazione γ_R,t = 1.25;

Fattore di correlazione per la determinazione della resistenza caratteristica desumibile dai criteri di progetto.
Fondazioni superficiali

Simbologia

B = Base della fondazione
L = Lunghezza della fondazione (L>B)
D = Profondità del piano di posa della fondazione
β = Inclinazione del piano di campagna
η = Inclinazione del piano di posa della fondazione
γ_r = Peso specifico rappresentativo del terreno di fondazione
$\sigma_{v0,f}$ = Pressione verticale alla profondità del piano di posa della fondazione
φ'_r = Angolo di attrito rappresentativo del terreno di fondazione
c'_r = Coesione efficace rappresentativa del terreno di fondazione
N_q = Coefficiente di capacità portante relativo al sovraccarico laterale
N_c = Coefficiente di capacità portante relativo alla coesione del terreno di fondazione
N_g = Coefficiente di capacità portante relativo al peso del terreno di fondazione
s_c = Fattore di forma relativo alla coesione
s_g = Fattore di forma relativo al peso del terreno
CC = Numero della combinazione delle condizioni di carico elementari
N = Sforzo normale
Mx = Momento intorno all'asse X
My = Momento intorno all'asse Y
B' = Base della fondazione reagente
L' = Lunghezza della fondazione reagente
q_{lim} = Pressione limite
R_d = Resistenza di progetto (Carico limite)
Sic. = Sicurezza a rottura

Verifiche capacità portante
Verifiche di capacità portante per rottura generale in condizioni statiche
Metodo utilizzato: Terzaghi

Platea n. 502

B=10.03 <m> L=13.31 <m> D=3.40 <m> β=0.00 <grad> η=0.00 <grad> γ_r=1799.98 <daN/mc>
$\sigma_{v0,f}$=6120.00 <daN/mq>

Verifiche in condizioni drenate

φ'_r=31.99 <grad> c'_r=499.99 <daN/mq>
N_q=28.48 N_c=43.99 N_g=26.82 s_c=1.30 s_g=0.80

CC	N <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	q_{lim} <daN/mq>	R_d <daN>	Sic.
17	699616.00	1320180.00	102674.00	6.25	13.02	323613.00	11452600.00	16.37

18 699562.00 1325120.00 196734.00 6.24 12.75 323335.00 11180600.00 15.98
19 699459.00 1351380.00 148697.00 6.16 12.89 321874.00 11113500.00 15.89
20 699719.00 1293930.00 150711.00 6.33 12.88 325073.00 11520700.00 16.46
21 671746.00 1277470.00 83663.50 6.22 13.07 323045.00 11417600.00 17.00
22 671693.00 1282410.00 177724.00 6.21 12.79 322755.00 11135900.00 16.58
23 671590.00 1308660.00 129686.00 6.13 12.93 321234.00 11065100.00 16.48
24 671849.00 1251210.00 131701.00 6.30 12.92 324566.00 11489400.00 17.10
25 687411.00 1297790.00 101763.00 6.25 13.02 323577.00 11445700.00 16.65
26 687358.00 1302730.00 195823.00 6.23 12.74 323294.00 11169000.00 16.25
27 687255.00 1328990.00 147786.00 6.16 12.88 321807.00 11100800.00 16.15
28 687514.00 1271530.00 149800.00 6.33 12.88 325063.00 11515000.00 16.75
29 659541.00 1255080.00 82752.10 6.22 13.06 322997.00 11409800.00 17.30
30 659488.00 1260010.00 176812.00 6.20 12.78 322702.00 11123000.00 16.87
31 659385.00 1286270.00 128775.00 6.12 12.92 321152.00 11050900.00 16.76
32 659644.00 1228820.00 130789.00 6.30 12.92 324546.00 11482900.00 17.41
33 696062.00 1190530.00 113056.00 6.60 12.99 330435.00 12325300.00 17.71
34 696009.00 1195460.00 207116.00 6.59 12.72 330156.00 12032200.00 17.29
35 695906.00 1221720.00 159078.00 6.51 12.86 328689.00 11969100.00 17.20
36 696165.00 1164270.00 161093.00 6.68 12.85 331902.00 12389300.00 17.80
37 668192.00 1147810.00 94044.90 6.59 13.03 330149.00 12327900.00 18.45
38 668139.00 1152750.00 188105.00 6.57 12.75 329858.00 12023400.00 18.00
39 668036.00 1179010.00 140068.00 6.50 12.90 328330.00 11956900.00 17.90
40 668295.00 1121550.00 142082.00 6.67 12.89 331677.00 12395500.00 18.55
41 683858.00 1168130.00 112144.00 6.61 12.99 330521.00 12333800.00 18.04
42 683805.00 1173070.00 206204.00 6.59 12.71 330237.00 12035200.00 17.60
43 683702.00 1199330.00 158167.00 6.52 12.85 328744.00 11971100.00 17.51
44 683961.00 1141880.00 160181.00 6.69 12.85 332014.00 12398800.00 18.13

Verifiche di capacità portante per rottura generale in condizioni statiche
Metodo utilizzato: Terzaghi

Plinto n. 11

B=1.60 <m> L=2.00 <m> D=1.00 <m> β=0.00 <grad> η=0.00 <grad> γ_r=1800.00 <daN/mc>
$\sigma_{v0,f}$=1800.00 <daN/mq>

Verifiche in condizioni drenate

φ'_r=31.87 <grad> c'$_r$=500.00 <daN/mq>
N_q=28.08 N_c=43.55 N_g=26.29 s_c=1.30 s_g=0.80

CC	N <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	q_{lim} <daN/mq>	R_d <daN>	Sic.
17	24582.80	777.56	-11573.10	0.66	1.94	91316.80	50630.00	2.06
18	24635.00	897.31	-11715.30	0.65	1.93	91136.10	49550.60	2.01
19	24846.00	804.28	-12286.20	0.61	1.94	90419.00	46486.00	1.87
20	24371.70	870.59	-11002.20	0.70	1.93	92049.40	53807.30	2.21
21	22970.20	730.37	-10823.90	0.66	1.94	91300.50	50545.90	2.20
22	23022.30	850.12	-10966.00	0.65	1.93	91107.10	49392.40	2.15
23	23233.40	757.09	-11536.90	0.61	1.93	90340.60	46120.30	1.99
24	22759.10	823.40	-10252.90	0.70	1.93	92084.80	53946.80	2.37
25	24571.80	753.71	-11569.40	0.66	1.94	91314.60	50669.70	2.06
26	24624.00	873.45	-11711.60	0.65	1.93	91133.80	49589.10	2.01
27	24835.00	780.42	-12282.50	0.61	1.94	90416.40	46519.60	1.87
28	24360.80	846.74	-10998.50	0.70	1.93	92047.50	53852.00	2.21
29	22959.20	706.52	-10820.10	0.66	1.94	91298.10	50588.30	2.20
30	23011.40	826.26	-10962.30	0.65	1.93	91104.60	49433.30	2.15
31	23222.40	733.23	-11533.20	0.61	1.94	90337.80	46155.70	1.99
32	22748.10	799.54	-10249.20	0.70	1.93	92082.80	53995.00	2.37
33	23776.20	842.81	-9475.92	0.80	1.93	94051.80	63337.30	2.66
34	23828.30	962.56	-9618.07	0.79	1.92	93858.90	62085.40	2.61
35	24039.40	869.53	-10189.00	0.75	1.93	93093.90	58697.60	2.44
36	23565.10	935.84	-8905.02	0.84	1.92	94833.90	66853.20	2.84
37	22163.50	795.62	-8726.64	0.81	1.93	94233.80	64190.00	2.90
38	22215.70	915.37	-8868.79	0.80	1.92	94026.60	62838.10	2.83
39	22426.80	822.34	-9439.70	0.76	1.93	93205.00	59195.30	2.64
40	21952.50	888.65	-8155.74	0.86	1.92	95075.20	67980.70	3.10
41	23765.20	818.96	-9472.20	0.80	1.93	94050.70	63397.10	2.67
42	23817.30	938.70	-9614.35	0.79	1.92	93857.80	62143.60	2.61
43	24028.40	845.67	-10185.30	0.75	1.93	93092.50	58750.00	2.45
44	23554.10	911.98	-8901.30	0.84	1.92	94833.20	66919.10	2.84

Verifiche di capacità portante per rottura generale in condizioni statiche
Metodo utilizzato: Terzaghi

Travata 512

B=1.30 <m> L=2.78 <m> D=1.00 <m> β=0.00 <grad> η=0.00 <grad> γ_r=1800.00 <daN/mc>
$\sigma_{v0,f}$=1800.00 <daN/mq>

Verifiche in condizioni drenate

φ'_r=31.85 <grad> c'_r=500.00 <daN/mq>
N_q=27.99 N_c=43.45 N_g=26.17 s_c=1.30 s_g=0.80

CC	N <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	q_{lim} <daN/mq>	R_d <daN>	Sic.
17	60879.10	-1209.25	2390.09	1.26	2.70	102371.00	151537.00	2.49
18	61525.90	-1235.19	2760.89	1.26	2.69	102363.00	150844.00	2.45
19	61087.30	-1350.35	2472.85	1.26	2.70	102287.00	150736.00	2.47
20	61317.70	-1094.09	2678.14	1.26	2.69	102447.00	151638.00	2.47
21	58634.10	-1184.99	2244.84	1.26	2.70	102358.00	151543.00	2.58
22	59280.90	-1210.94	2615.64	1.26	2.69	102350.00	150825.00	2.54
23	58842.30	-1326.09	2327.59	1.25	2.70	102271.00	150712.00	2.56
24	59072.70	-1069.84	2532.88	1.26	2.69	102437.00	151649.00	2.57
25	59845.20	-1211.25	2316.70	1.26	2.70	102357.00	151486.00	2.53
26	60492.00	-1237.19	2687.50	1.26	2.69	102349.00	150783.00	2.49
27	60053.30	-1352.35	2399.46	1.25	2.70	102271.00	150673.00	2.51
28	60283.80	-1096.09	2604.74	1.26	2.69	102435.00	151590.00	2.51
29	57600.20	-1186.99	2171.45	1.26	2.70	102343.00	151491.00	2.63
30	58247.00	-1212.94	2542.25	1.26	2.69	102335.00	150761.00	2.59
31	57808.30	-1328.09	2254.20	1.25	2.70	102254.00	150645.00	2.61
32	58038.80	-1071.84	2459.49	1.26	2.70	102424.00	151600.00	2.61
33	60892.70	-842.66	2592.17	1.27	2.69	102598.00	152949.00	2.51
34	61539.50	-868.60	2962.97	1.27	2.68	102588.00	152234.00	2.47
35	61100.80	-983.76	2674.92	1.27	2.69	102513.00	152142.00	2.49
36	61331.30	-727.50	2880.21	1.28	2.69	102673.00	153035.00	2.50
37	58647.70	-818.41	2446.91	1.27	2.70	102594.00	153011.00	2.61
38	59294.50	-844.35	2817.71	1.27	2.68	102583.00	152268.00	2.57
39	58855.80	-959.51	2529.67	1.27	2.69	102506.00	152172.00	2.59
40	59086.30	-703.25	2734.96	1.28	2.69	102671.00	153100.00	2.59
41	59858.70	-844.66	2518.78	1.27	2.70	102588.00	152924.00	2.55
42	60505.50	-870.60	2889.58	1.27	2.68	102578.00	152198.00	2.52
43	60066.90	-985.76	2601.53	1.27	2.69	102501.00	152103.00	2.53
44	60297.40	-729.50	2806.82	1.28	2.69	102664.00	153012.00	2.54

Verifiche di capacità portante per rottura generale in condizioni statiche
Metodo utilizzato: Terzaghi

Travata 513

B=1.30 <m> L=2.70 <m> D=1.00 <m> β=0.00 <grad> η=0.00 <grad> γ_r=1800.00 <daN/mc>
$\sigma_{v0,f}$=1800.00 <daN/mq>

Verifiche in condizioni drenate

φ'_r=31.85 <grad> c'_r=500.00 <daN/mq>
N_q=27.99 N_c=43.45 N_g=26.17 s_c=1.30 s_g=0.80

CC	N <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	q_{lim} <daN/mq>	R_d <daN>	Sic.
17	34996.10	0.00	1.41E-03	1.30	2.70	103120.00	157370.00	4.50
18	34996.10	0.00	1.41E-03	1.30	2.70	103120.00	157370.00	4.50
19	34996.10	0.00	1.41E-03	1.30	2.70	103120.00	157370.00	4.50
20	34996.10	0.00	1.41E-03	1.30	2.70	103120.00	157370.00	4.50
21	33465.20	0.00	1.42E-03	1.30	2.70	103120.00	157370.00	4.70
22	33465.20	0.00	1.42E-03	1.30	2.70	103120.00	157370.00	4.70
23	33465.20	0.00	1.42E-03	1.30	2.70	103120.00	157370.00	4.70
24	33465.20	0.00	1.42E-03	1.30	2.70	103120.00	157370.00	4.70
25	34485.80	0.00	1.40E-03	1.30	2.70	103120.00	157370.00	4.56
26	34485.80	0.00	1.40E-03	1.30	2.70	103120.00	157370.00	4.56
27	34485.80	0.00	1.40E-03	1.30	2.70	103120.00	157370.00	4.56
28	34485.80	0.00	1.40E-03	1.30	2.70	103120.00	157370.00	4.56
29	32954.90	0.00	1.40E-03	1.30	2.70	103120.00	157370.00	4.78

30	32954.90	0.00	1.40E-03	1.30	2.70	103120.00	157370.00	4.78
31	32954.90	0.00	1.40E-03	1.30	2.70	103120.00	157370.00	4.78
32	32954.90	0.00	1.40E-03	1.30	2.70	103120.00	157370.00	4.78
33	34996.10	0.00	1.41E-03	1.30	2.70	103120.00	157370.00	4.50
34	34996.10	0.00	1.41E-03	1.30	2.70	103120.00	157370.00	4.50
35	34996.10	0.00	1.41E-03	1.30	2.70	103120.00	157370.00	4.50
36	34996.10	0.00	1.41E-03	1.30	2.70	103120.00	157370.00	4.50
37	33465.20	0.00	1.42E-03	1.30	2.70	103120.00	157370.00	4.70
38	33465.20	0.00	1.42E-03	1.30	2.70	103120.00	157370.00	4.70
39	33465.20	0.00	1.42E-03	1.30	2.70	103120.00	157370.00	4.70
40	33465.20	0.00	1.42E-03	1.30	2.70	103120.00	157370.00	4.70
41	34485.80	0.00	1.40E-03	1.30	2.70	103120.00	157370.00	4.56
42	34485.80	0.00	1.40E-03	1.30	2.70	103120.00	157370.00	4.56
43	34485.80	0.00	1.40E-03	1.30	2.70	103120.00	157370.00	4.56
44	34485.80	0.00	1.40E-03	1.30	2.70	103120.00	157370.00	4.56

Verifiche di capacità portante per rottura generale in condizioni statiche
Metodo utilizzato: Terzaghi

Travata 515

B=1.30 <m> L=2.70 <m> D=1.00 <m> β=0.00 <grad> η=0.00 <grad> γ_r=1800.00 <daN/mc>
$\sigma_{v0,f}$=1800.00 <daN/mq>

Verifiche in condizioni drenate

φ'_r=31.85 <grad> c'_r=500.00 <daN/mq>
N_q=27.99 N_c=43.45 N_g=26.17 s_c=1.30 s_g=0.80

CC	N <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	q_{lim} <daN/mq>	R_d <daN>	Sic.
17	66750.50	251.08	-5788.09	1.29	2.53	102978.00	146209.00	2.19
18	66698.40	345.36	-5923.70	1.29	2.52	102925.00	145570.00	2.18
19	66487.30	321.30	-6471.29	1.29	2.51	102938.00	144683.00	2.18
20	66961.60	275.14	-5240.51	1.29	2.54	102965.00	147089.00	2.20
21	60583.80	231.36	-5697.69	1.29	2.51	102976.00	145344.00	2.40
22	60531.70	325.64	-5833.30	1.29	2.51	102917.00	144642.00	2.39
23	60320.60	301.58	-6380.89	1.29	2.49	102932.00	143660.00	2.38
24	60794.90	255.42	-5150.11	1.29	2.53	102962.00	146317.00	2.41
25	66224.50	252.14	-5791.33	1.29	2.53	102976.00	146110.00	2.21
26	66172.30	346.41	-5926.94	1.29	2.52	102923.00	145467.00	2.20
27	65961.30	322.36	-6474.53	1.29	2.50	102936.00	144572.00	2.19
28	66435.60	276.19	-5243.75	1.29	2.54	102963.00	146998.00	2.21
29	60057.80	232.42	-5700.93	1.29	2.51	102974.00	145228.00	2.42
30	60005.60	326.69	-5836.55	1.29	2.51	102915.00	144520.00	2.41
31	59794.60	302.64	-6384.13	1.29	2.49	102929.00	143530.00	2.40
32	60268.80	256.48	-5153.35	1.29	2.53	102960.00	146210.00	2.43
33	67557.20	187.94	-3720.39	1.29	2.59	103015.00	150152.00	2.22
34	67505.00	282.22	-3856.00	1.29	2.59	102962.00	149513.00	2.21
35	67294.00	258.16	-4403.58	1.29	2.57	102975.00	148649.00	2.21
36	67768.30	212.00	-3172.80	1.29	2.61	103002.00	151008.00	2.23
37	61390.50	168.23	-3629.99	1.29	2.58	103017.00	149693.00	2.44
38	61338.30	262.50	-3765.60	1.29	2.58	102959.00	148991.00	2.43
39	61127.30	238.44	-4313.18	1.29	2.56	102973.00	148038.00	2.42
40	61601.50	192.28	-3082.40	1.29	2.60	103002.00	150637.00	2.45
41	67031.10	189.00	-3723.63	1.29	2.59	103014.00	150085.00	2.24
42	66979.00	283.27	-3859.24	1.29	2.58	102961.00	149442.00	2.23
43	66767.90	259.22	-4406.82	1.29	2.57	102974.00	148571.00	2.23
44	67242.20	213.06	-3176.04	1.29	2.61	103001.00	150949.00	2.24

Verifiche di capacità portante per rottura generale in condizioni sismiche
Metodo utilizzato: Condizioni statiche

Platea n. 502

B=10.03 <m> L=13.31 <m> D=3.40 <m> β=0.00 <grad> η=0.00 <grad> γ_r=1799.98 <daN/mc>
$\sigma_{v0,f}$=6120.00 <daN/mq>

Verifiche in condizioni drenate

φ'_r=31.99 <grad> c'_r=499.99 <daN/mq>
N_q=28.48 N_c=43.99 N_g=26.82 s_c=1.30 s_g=0.80

CC	N <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	q_{lim} <daN/mq>	R_d <daN>	Sic.
1	518658.00	829790.00	779869.00	6.83	10.31	334703.00	10237800.00	19.74
3	518029.00	682675.00	715025.00	7.39	10.55	345597.00	11718600.00	22.62
5	519234.00	988390.00	405885.00	6.22	11.75	322974.00	10260700.00	19.76
7	519098.00	977218.00	20483.40	6.26	13.24	323786.00	11664300.00	22.47
9	518720.00	805510.00	797748.00	6.92	10.24	336519.00	10365700.00	19.98
11	518091.00	658395.00	732904.00	7.48	10.49	347413.00	11852500.00	22.88
13	519296.00	964110.00	423764.00	6.31	11.68	324788.00	10413100.00	20.05
15	519161.00	952938.00	38361.90	6.35	13.17	325601.00	11843900.00	22.81

Verifiche di capacità portante per rottura generale in condizioni sismiche
Metodo utilizzato: Condizioni statiche

Plinto n. 11

B=1.60 <m> L=2.00 <m> D=1.00 <m> β=0.00 <grad> η=0.00 <grad> γ_r=1800.00 <daN/mc>
$\sigma_{v0,f}$=1800.00 <daN/mq>

Verifiche in condizioni drenate

φ'_r=31.87 <grad> c'_r=500.00 <daN/mq>
N_q=28.08 N_c=43.55 N_g=26.29 s_c=1.30 s_g=0.80

CC	N <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	q_{lim} <daN/mq>	R_d <daN>	Sic.
1	18114.90	1939.56	-3600.11	1.20	1.79	101617.00	94881.40	5.24
1	18114.90	1939.56	-6066.92	0.93	1.79	96461.10	69668.50	3.85
1	16318.60	54.57	-3600.11	1.16	1.99	100789.00	101218.00	6.20
1	16318.60	54.57	-6066.92	0.86	1.99	95065.20	70561.10	4.32
1	18114.90	1562.26	-3600.11	1.20	1.83	101617.00	97094.50	5.36
1	18114.90	1562.26	-6066.92	0.93	1.83	96461.10	71293.60	3.94
1	16318.60	-322.73	-3600.11	1.16	1.96	100789.00	99549.00	6.10
1	16318.60	-322.73	-6066.92	0.86	1.96	95065.20	69397.70	4.25
3	16973.00	1605.36	-3633.99	1.17	1.81	101035.00	93212.30	5.49
3	16973.00	1605.36	-2960.76	1.25	1.81	102537.00	101002.00	5.95
3	17460.50	276.95	-3633.99	1.18	1.97	101262.00	102580.00	5.87
3	17460.50	276.95	-2960.76	1.26	1.97	102721.00	110838.00	6.35
3	16973.00	1339.88	-3633.99	1.17	1.84	101035.00	94822.60	5.59
3	16973.00	1339.88	-2960.76	1.25	1.84	102537.00	102747.00	6.05
3	17460.50	11.47	-3633.99	1.18	2.00	101262.00	104165.00	5.97
3	17460.50	11.47	-2960.76	1.26	2.00	102721.00	112550.00	6.45
5	19218.20	1654.63	-3566.73	1.23	1.83	102115.00	99719.10	5.19
5	19218.20	1654.63	-9069.19	0.66	1.83	91274.30	47596.90	2.48
5	15215.30	244.98	-3566.73	1.13	1.97	100266.00	97035.90	6.38
5	15215.30	244.98	-9069.19	0.41	1.97	86573.60	30211.70	1.99
5	19218.20	1371.85	-3566.73	1.23	1.86	102115.00	101325.00	5.27
5	19218.20	1371.85	-9069.19	0.66	1.86	91274.30	48363.30	2.52
5	15215.30	-37.80	-3566.73	1.13	2.00	100266.00	98378.80	6.47
5	15215.30	-37.80	-9069.19	0.41	2.00	86573.60	30629.80	2.01
7	19021.90	1076.20	-3572.01	1.22	1.89	102032.00	102489.00	5.39
7	19021.90	1076.20	-8536.39	0.70	1.89	92150.40	53104.50	2.79
7	15411.60	630.57	-3572.01	1.14	1.92	100366.00	95125.60	6.17
7	15411.60	630.57	-8536.39	0.49	1.92	88170.00	36193.70	2.35
7	19021.90	986.26	-3572.01	1.22	1.90	102032.00	103003.00	5.41
7	19021.90	986.26	-8536.39	0.70	1.90	92150.40	53370.60	2.81
7	15411.60	540.63	-3572.01	1.14	1.93	100366.00	95704.50	6.21
7	15411.60	540.63	-8536.39	0.49	1.93	88170.00	36413.90	2.36
9	18633.40	1739.97	-5017.92	1.06	1.81	98945.50	82795.20	4.44
9	18633.40	1739.97	-7484.74	0.80	1.81	93933.00	58993.50	3.17
9	16837.00	-145.02	-5017.92	1.00	1.98	97857.60	84693.10	5.03
9	16837.00	-145.02	-7484.74	0.71	1.98	92310.40	56573.80	3.36
9	18633.40	1362.67	-5017.92	1.06	1.85	98945.50	84644.40	4.54
9	18633.40	1362.67	-7484.74	0.80	1.85	93933.00	60311.00	3.24
9	16837.00	-522.32	-5017.92	1.00	1.94	97857.60	82778.80	4.92
9	16837.00	-522.32	-7484.74	0.71	1.94	92310.40	55295.00	3.28
11	17491.40	1405.77	-5051.81	1.02	1.84	98206.40	80290.20	4.59
11	17491.40	1405.77	-4378.58	1.10	1.84	99663.70	87616.80	5.01
11	17979.00	77.36	-5051.81	1.04	1.99	98503.00	88529.80	4.92
11	17979.00	77.36	-4378.58	1.11	1.99	99920.80	96283.20	5.36
11	17491.40	1140.28	-5051.81	1.02	1.87	98206.40	81615.40	4.67

11	17491.40	1140.28	-4378.58	1.10	1.87	99663.70	89062.80	5.09
11	17979.00	-188.12	-5051.81	1.04	1.98	98503.00	87982.10	4.89
11	17979.00	-188.12	-4378.58	1.11	1.98	99920.80	95687.40	5.32
13	19736.70	1455.04	-4984.55	1.09	1.85	99579.40	87818.30	4.45
13	19736.70	1455.04	-10487.00	0.54	1.85	89023.70	38527.60	1.95
13	15733.70	45.39	-4984.55	0.97	1.99	97146.70	81400.40	5.17
13	15733.70	45.39	-10487.00	0.27	1.99	83905.40	19420.20	1.23
13	19736.70	1172.26	-4984.55	1.09	1.88	99579.40	89176.70	4.52
13	19736.70	1172.26	-10487.00	0.54	1.88	89023.70	39123.60	1.98
13	15733.70	-237.39	-4984.55	0.97	1.97	97146.70	80404.20	5.11
13	15733.70	-237.39	-10487.00	0.27	1.97	83905.40	19182.50	1.22
15	19540.40	876.61	-4989.83	1.09	1.91	99473.10	89994.00	4.61
15	19540.40	876.61	-9954.21	0.58	1.91	89854.00	43371.50	2.22
15	15930.10	430.98	-4989.83	0.97	1.95	97281.90	80126.00	5.03
15	15930.10	430.98	-9954.21	0.35	1.95	85482.70	25331.50	1.59
15	19540.40	786.66	-4989.83	1.09	1.92	99473.10	90427.70	4.63
15	19540.40	786.66	-9954.21	0.58	1.92	89854.00	43580.50	2.23
15	15930.10	341.03	-4989.83	0.97	1.96	97281.90	80591.00	5.06
15	15930.10	341.03	-9954.21	0.35	1.96	85482.70	25478.50	1.60

Verifiche di capacità portante per rottura generale in condizioni sismiche
Metodo utilizzato: Condizioni statiche

Travata 512

B=1.30 <m> L=2.78 <m> D=1.00 <m> β=0.00 <grad> η=0.00 <grad> γ_r=1800.00 <daN/mc>
$\sigma_{v0,f}$=1800.00 <daN/mq>

Verifiche in condizioni drenate

φ'_r=31.85 <grad> c'_r=500.00 <daN/mq>
N_q=27.99 N_c=43.45 N_g=26.17 s_c=1.30 s_g=0.80

CC	N <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	q_{lim} <daN/mq>	R_d <daN>	Sic.
1	51155.00	-564.70	5993.54	1.28	2.55	102704.00	145267.00	2.84
3	49589.30	2.78	4959.24	1.30	2.58	103118.00	150359.00	3.03
5	49438.30	-1112.46	5110.44	1.25	2.57	102272.00	143600.00	2.90
7	46401.10	-1014.50	3319.18	1.26	2.64	102296.00	147338.00	3.18
9	50221.90	-788.34	5375.78	1.27	2.57	102528.00	145106.00	2.89
11	48656.30	-220.87	4341.47	1.29	2.60	102949.00	150323.00	3.09
13	48505.20	-1336.11	4492.68	1.24	2.59	102082.00	143369.00	2.96
15	45468.10	-1238.15	2701.42	1.25	2.66	102094.00	147130.00	3.24

Verifiche di capacità portante per rottura generale in condizioni sismiche
Metodo utilizzato: Condizioni statiche

Travata 513

B=1.30 <m> L=2.70 <m> D=1.00 <m> β=0.00 <grad> η=0.00 <grad> γ_r=1800.00 <daN/mc>
$\sigma_{v0,f}$=1800.00 <daN/mq>

Verifiche in condizioni drenate

φ'_r=31.85 <grad> c'_r=500.00 <daN/mq>
N_q=27.99 N_c=43.45 N_g=26.17 s_c=1.30 s_g=0.80

CC	N <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	q_{lim} <daN/mq>	R_d <daN>	Sic.
1	26560.70	0.00	1.18E-03	1.30	2.70	103120.00	157370.00	5.92
3	26560.70	0.00	1.18E-03	1.30	2.70	103120.00	157370.00	5.92
5	26560.70	0.00	1.18E-03	1.30	2.70	103120.00	157370.00	5.92
7	26560.70	0.00	1.18E-03	1.30	2.70	103120.00	157370.00	5.92
9	26560.70	0.00	1.18E-03	1.30	2.70	103120.00	157370.00	5.92
11	26560.70	0.00	1.18E-03	1.30	2.70	103120.00	157370.00	5.92
13	26560.70	0.00	1.18E-03	1.30	2.70	103120.00	157370.00	5.92
15	26560.70	0.00	1.18E-03	1.30	2.70	103120.00	157370.00	5.92

Verifiche di capacità portante per rottura generale in condizioni sismiche
Metodo utilizzato: Condizioni statiche

Travata 515

B=1.30 <m> L=2.70 <m> D=1.00 <m> β=0.00 <grad> η=0.00 <grad> γ_r=1800.00 <daN/mc>
$\sigma_{v0,f}$=1800.00 <daN/mq>

Verifiche in condizioni drenate

φ'_r=31.85 <grad> c'_r=500.00 <daN/mq>
N_q=27.99 N_c=43.45 N_g=26.17 s_c=1.30 s_g=0.80

CC	N <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	q_{lim} <daN/mq>	R_d <daN>	Sic.
1	49547.50	742.58	2535.54	1.27	2.60	102555.00	147104.00	2.97
3	48405.50	556.51	-432.27	1.28	2.68	102687.00	152919.00	3.16
5	50650.70	536.18	5403.16	1.28	2.49	102721.00	142023.00	2.80
7	50454.40	173.20	4893.30	1.29	2.51	102991.00	145111.00	2.88
9	49029.00	832.33	-3481.43	1.27	2.56	102480.00	144298.00	2.94
11	47887.00	646.26	-513.62	1.27	2.68	102611.00	152124.00	3.18
13	50132.30	625.93	-6349.05	1.28	2.45	102649.00	139229.00	2.78
15	49936.00	262.96	-5839.20	1.29	2.47	102921.00	142300.00	2.85

Cedimenti
Metodo utilizzato: Terzaghi (1955)

Simbologia

B = Base della fondazione
L = Lunghezza della fondazione (L>B)
k_1 = Costante di sottofondo standardizzata
kw = Costante di sottofondo
CC = Numero della combinazione delle condizioni di carico elementari
N = Sforzo normale
q_{es} = Pressione di esercizio
Ced = Cedimento calcolato

Platea n. 502
B=10.03 <m> L=13.31 <m> k_1=2000000.00 <daN/mc> kw=530372.00 <daN/mc>

CC	N <daN>	q_{es} <daN/mq>	Ced <cm>
1	518658.00	3885.63	0.73
2	518575.00	3885.01	0.73
3	518029.00	3880.92	0.73
4	518048.00	3881.07	0.73
5	519234.00	3889.95	0.73
6	519057.00	3888.62	0.73
7	519098.00	3888.93	0.73
8	518944.00	3887.78	0.73
9	518720.00	3886.10	0.73
10	518627.00	3885.40	0.73
11	518091.00	3881.39	0.73
12	518100.00	3881.46	0.73
13	519296.00	3890.41	0.73
14	519109.00	3889.02	0.73
15	519161.00	3889.40	0.73
16	518996.00	3888.17	0.73
17	699616.00	5241.32	0.99
18	699562.00	5240.92	0.99
19	699459.00	5240.15	0.99
20	699719.00	5242.09	0.99
21	671746.00	5032.52	0.95
22	671693.00	5032.12	0.95
23	671590.00	5031.35	0.95
24	671849.00	5033.29	0.95
25	687411.00	5149.88	0.97
26	687358.00	5149.49	0.97
27	687255.00	5148.71	0.97
28	687514.00	5150.66	0.97
29	659541.00	4941.09	0.93
30	659488.00	4940.69	0.93
31	659385.00	4939.92	0.93
32	659644.00	4941.86	0.93

33	696062.00	5214.69	0.98
34	696009.00	5214.30	0.98
35	695906.00	5213.52	0.98
36	696165.00	5215.47	0.98
37	668192.00	5005.90	0.94
38	668139.00	5005.50	0.94
39	668036.00	5004.73	0.94
40	668295.00	5006.67	0.94
41	683858.00	5123.26	0.97
42	683805.00	5122.87	0.97
43	683702.00	5122.09	0.97
44	683961.00	5124.04	0.97
45	518039.00	3880.99	0.73
46	517986.00	3880.60	0.73
47	517883.00	3879.82	0.73
48	518142.00	3881.77	0.73
49	499459.00	3741.80	0.71
50	499406.00	3741.40	0.71
51	499303.00	3740.63	0.71
52	499562.00	3742.57	0.71
53	509903.00	3820.04	0.72
54	509849.00	3819.64	0.72
55	509746.00	3818.87	0.72
56	510006.00	3820.81	0.72
57	491323.00	3680.84	0.69
58	491269.00	3680.45	0.69
59	491166.00	3679.68	0.69
60	491426.00	3681.62	0.69
61	515670.00	3863.25	0.73
62	515617.00	3862.85	0.73
63	515514.00	3862.08	0.73
64	515773.00	3864.02	0.73
65	497090.00	3724.05	0.70
66	497037.00	3723.65	0.70
67	496934.00	3722.88	0.70
68	497193.00	3724.82	0.70
69	507534.00	3802.29	0.72
70	507481.00	3801.90	0.72
71	507378.00	3801.12	0.72
72	507637.00	3803.07	0.72
73	481703.00	3608.78	0.68
74	481650.00	3608.38	0.68
75	481547.00	3607.61	0.68
76	481806.00	3609.55	0.68
77	475510.00	3562.38	0.67
78	475457.00	3561.98	0.67
79	475354.00	3561.21	0.67
80	475613.00	3563.15	0.67
81	478449.00	3584.40	0.68
82	478395.00	3584.00	0.68
83	478292.00	3583.23	0.68
84	478552.00	3585.17	0.68
85	472255.00	3538.00	0.67
86	472202.00	3537.60	0.67
87	472099.00	3536.83	0.67
88	472358.00	3538.77	0.67
89	480519.00	3599.90	0.68
90	480466.00	3599.51	0.68
91	480362.00	3598.74	0.68
92	480622.00	3600.68	0.68
93	474325.00	3553.51	0.67
94	474272.00	3553.11	0.67
95	474169.00	3552.34	0.67
96	474428.00	3554.28	0.67
97	477264.00	3575.52	0.67
98	477211.00	3575.13	0.67
99	477108.00	3574.35	0.67
100	477367.00	3576.29	0.67
101	471071.00	3529.12	0.67
102	471018.00	3528.73	0.67
103	470915.00	3527.96	0.67
104	471174.00	3529.90	0.67

Plinto n. 11
B=1.60 <m> L=2.00 <m> k_1=2000000.00 <daN/mc> kw=705078.00 <daN/mc>

CC	N <daN>	q_{es} <daN/mq>	Ced <cm>
1	18114.90	5660.92	0.80
2	18011.00	5628.45	0.80
3	16973.00	5304.05	0.75
4	17054.80	5329.61	0.76
5	19218.20	6005.69	0.85
6	18934.90	5917.16	0.84
7	19021.90	5944.34	0.84
8	18770.50	5865.79	0.83
9	18633.40	5822.94	0.83
10	18445.20	5764.12	0.82
11	17491.40	5466.07	0.78
12	17488.90	5465.28	0.78
13	19736.70	6167.71	0.87
14	19369.10	6052.84	0.86
15	19540.40	6106.36	0.87
16	19204.70	6001.46	0.85
17	24582.80	7682.13	1.09
18	24635.00	7698.42	1.09
19	24846.00	7764.38	1.10
20	24371.70	7616.17	1.08
21	22970.20	7178.18	1.02
22	23022.30	7194.48	1.02
23	23233.40	7260.44	1.03
24	22759.10	7112.22	1.01
25	24571.80	7678.70	1.09
26	24624.00	7694.99	1.09
27	24835.00	7760.95	1.10
28	24360.80	7612.74	1.08
29	22959.20	7174.75	1.02
30	23011.40	7191.05	1.02
31	23222.40	7257.01	1.03
32	22748.10	7108.79	1.01
33	23776.20	7430.05	1.05
34	23828.30	7446.35	1.06
35	24039.40	7512.30	1.07
36	23565.10	7364.09	1.04
37	22163.50	6926.11	0.98
38	22215.70	6942.40	0.98
39	22426.80	7008.36	0.99
40	21952.50	6860.15	0.97
41	23765.20	7426.62	1.05
42	23817.30	7442.92	1.06
43	24028.40	7508.88	1.06
44	23554.10	7360.66	1.04
45	18653.70	5829.27	0.83
46	18705.80	5845.56	0.83
47	18916.90	5911.52	0.84
48	18442.60	5763.31	0.82
49	17578.60	5493.31	0.78
50	17630.70	5509.60	0.78
51	17841.80	5575.56	0.79
52	17367.50	5427.35	0.77
53	18646.30	5826.98	0.83
54	18698.50	5843.28	0.83
55	18909.60	5909.24	0.84
56	18435.30	5761.02	0.82
57	17571.30	5491.02	0.78
58	17623.40	5507.32	0.78
59	17834.50	5573.27	0.79
60	17360.20	5425.06	0.77
61	18115.90	5661.22	0.80
62	18168.00	5677.51	0.81
63	18379.10	5743.47	0.81
64	17904.80	5595.26	0.79
65	17040.80	5325.25	0.76
66	17093.00	5341.55	0.76
67	17304.00	5407.51	0.77
68	16829.80	5259.30	0.75

69	18108.60	5658.93	0.80
70	18160.70	5675.23	0.80
71	18371.80	5741.19	0.81
72	17897.50	5592.97	0.79
73	16491.30	5153.55	0.73
74	16543.50	5169.84	0.73
75	16754.60	5235.80	0.74
76	16280.30	5087.59	0.72
77	16133.00	5041.56	0.72
78	16185.10	5057.85	0.72
79	16396.20	5123.81	0.73
80	15921.90	4975.60	0.71
81	16488.40	5152.63	0.73
82	16540.60	5168.93	0.73
83	16751.60	5234.89	0.74
84	16277.40	5086.67	0.72
85	16130.10	5040.64	0.71
86	16182.20	5056.94	0.72
87	16393.30	5122.90	0.73
88	15919.00	4974.69	0.71
89	16222.50	5069.52	0.72
90	16274.60	5085.82	0.72
91	16485.70	5151.77	0.73
92	16011.40	5003.56	0.71
93	15864.10	4957.53	0.70
94	15916.30	4973.83	0.71
95	16127.30	5039.79	0.71
96	15653.00	4891.58	0.69
97	16219.50	5068.61	0.72
98	16271.70	5084.90	0.72
99	16482.80	5150.86	0.73
100	16008.50	5002.65	0.71
101	15861.20	4956.62	0.70
102	15913.30	4972.91	0.71
103	16124.40	5038.87	0.71
104	15650.10	4890.66	0.69

Travata 512

B=1.30 <m> L=2.78 <m> k_1=2000000.00 <daN/mc> kw=757396.00 <daN/mc>

CC	N <daN>	q_{es} <daN/mq>	Ced <cm>
1	51155.00	14154.70	1.87
2	50128.80	13870.70	1.83
3	49589.30	13721.40	1.81
4	48817.70	13507.90	1.78
5	49438.30	13679.70	1.81
6	48691.20	13472.90	1.78
7	46401.10	12839.30	1.70
8	46147.90	12769.20	1.69
9	50221.90	13896.50	1.83
10	49347.40	13654.50	1.80
11	48656.30	13463.30	1.78
12	48036.30	13291.70	1.75
13	48505.20	13421.50	1.77
14	47909.90	13256.70	1.75
15	45468.10	12581.10	1.66
16	45366.60	12553.00	1.66
17	60879.10	16845.30	2.22
18	61525.90	17024.30	2.25
19	61087.30	16902.90	2.23
20	61317.70	16966.70	2.24
21	58634.10	16224.20	2.14
22	59280.90	16403.10	2.17
23	58842.30	16281.80	2.15
24	59072.70	16345.50	2.16
25	59845.20	16559.30	2.19
26	60492.00	16738.20	2.21
27	60053.30	16616.90	2.19
28	60283.80	16680.60	2.20
29	57600.20	15938.10	2.10
30	58247.00	16117.00	2.13
31	57808.30	15995.70	2.11

32	58038.80	16059.40	2.12
33	60892.70	16849.10	2.22
34	61539.50	17028.10	2.25
35	61100.80	16906.70	2.23
36	61331.30	16970.50	2.24
37	58647.70	16227.90	2.14
38	59294.50	16406.90	2.17
39	58855.80	16285.50	2.15
40	59086.30	16349.30	2.16
41	59858.70	16563.00	2.19
42	60505.50	16742.00	2.21
43	60066.90	16620.60	2.19
44	60297.40	16684.40	2.20
45	43795.10	12118.20	1.60
46	44441.90	12297.10	1.62
47	44003.20	12175.80	1.61
48	44233.70	12239.50	1.62
49	42298.40	11704.00	1.55
50	42945.20	11883.00	1.57
51	42506.60	11761.60	1.55
52	42737.10	11825.40	1.56
53	43105.80	11927.40	1.57
54	43752.60	12106.40	1.60
55	43314.00	11985.00	1.58
56	43544.40	12048.80	1.59
57	41609.10	11513.30	1.52
58	42255.90	11692.30	1.54
59	41817.30	11570.90	1.53
60	42047.80	11634.70	1.54
61	43804.10	12120.70	1.60
62	44450.90	12299.60	1.62
63	44012.30	12178.30	1.61
64	44242.80	12242.00	1.62
65	42307.50	11706.50	1.55
66	42954.30	11885.50	1.57
67	42515.60	11764.10	1.55
68	42746.10	11827.90	1.56
69	43114.80	11930.00	1.58
70	43761.70	12108.90	1.60
71	43323.00	11987.50	1.58
72	43553.50	12051.30	1.59
73	41213.70	11403.90	1.51
74	41860.50	11582.90	1.53
75	41421.80	11461.50	1.51
76	41652.30	11525.30	1.52
77	40714.80	11265.80	1.49
78	41361.60	11444.80	1.51
79	40922.90	11323.40	1.50
80	41153.40	11387.20	1.50
81	40938.00	11327.60	1.50
82	41584.80	11506.60	1.52
83	41146.10	11385.20	1.50
84	41376.60	11449.00	1.51
85	40439.10	11189.60	1.48
86	41085.90	11368.50	1.50
87	40647.20	11247.20	1.48
88	40877.70	11310.90	1.49
89	41218.20	11405.10	1.51
90	41865.00	11584.10	1.53
91	41426.40	11462.70	1.51
92	41656.80	11526.50	1.52
93	40719.30	11267.10	1.49
94	41366.10	11446.10	1.51
95	40927.50	11324.70	1.50
96	41158.00	11388.50	1.50
97	40942.50	11328.90	1.50
98	41589.30	11507.80	1.52
99	41150.60	11386.50	1.50
100	41381.10	11450.20	1.51
101	40443.60	11190.80	1.48
102	41090.40	11369.80	1.50
103	40651.80	11248.40	1.49
104	40882.20	11312.20	1.49

Travata 513

B=1.30 <m> L=2.70 <m> k_1=2000000.00 <daN/mc> kw=757396.00 <daN/mc>

CC	N <daN>	q_{es} <daN/mq>	Ced <cm>
1	26560.70	7567.16	1.00
2	26560.70	7567.16	1.00
3	26560.70	7567.16	1.00
4	26560.70	7567.16	1.00
5	26560.70	7567.16	1.00
6	26560.70	7567.16	1.00
7	26560.70	7567.16	1.00
8	26560.70	7567.16	1.00
9	26560.70	7567.16	1.00
10	26560.70	7567.16	1.00
11	26560.70	7567.16	1.00
12	26560.70	7567.16	1.00
13	26560.70	7567.16	1.00
14	26560.70	7567.16	1.00
15	26560.70	7567.16	1.00
16	26560.70	7567.16	1.00
17	34996.10	9970.39	1.32
18	34996.10	9970.39	1.32
19	34996.10	9970.39	1.32
20	34996.10	9970.39	1.32
21	33465.20	9534.24	1.26
22	33465.20	9534.24	1.26
23	33465.20	9534.24	1.26
24	33465.20	9534.24	1.26
25	34485.80	9825.01	1.30
26	34485.80	9825.01	1.30
27	34485.80	9825.01	1.30
28	34485.80	9825.01	1.30
29	32954.90	9388.85	1.24
30	32954.90	9388.85	1.24
31	32954.90	9388.85	1.24
32	32954.90	9388.85	1.24
33	34996.10	9970.39	1.32
34	34996.10	9970.39	1.32
35	34996.10	9970.39	1.32
36	34996.10	9970.39	1.32
37	33465.20	9534.24	1.26
38	33465.20	9534.24	1.26
39	33465.20	9534.24	1.26
40	33465.20	9534.24	1.26
41	34485.80	9825.01	1.30
42	34485.80	9825.01	1.30
43	34485.80	9825.01	1.30
44	34485.80	9825.01	1.30
45	26187.30	7460.77	0.99
46	26187.30	7460.77	0.99
47	26187.30	7460.77	0.99
48	26187.30	7460.77	0.99
49	25166.70	7170.00	0.95
50	25166.70	7170.00	0.95
51	25166.70	7170.00	0.95
52	25166.70	7170.00	0.95
53	25847.10	7363.85	0.97
54	25847.10	7363.85	0.97
55	25847.10	7363.85	0.97
56	25847.10	7363.85	0.97
57	24826.50	7073.08	0.93
58	24826.50	7073.08	0.93
59	24826.50	7073.08	0.93
60	24826.50	7073.08	0.93
61	26187.30	7460.77	0.99
62	26187.30	7460.77	0.99
63	26187.30	7460.77	0.99
64	26187.30	7460.77	0.99
65	25166.70	7170.00	0.95
66	25166.70	7170.00	0.95
67	25166.70	7170.00	0.95

68	25166.70	7170.00	0.95
69	25847.10	7363.85	0.97
70	25847.10	7363.85	0.97
71	25847.10	7363.85	0.97
72	25847.10	7363.85	0.97
73	24622.40	7014.93	0.93
74	24622.40	7014.93	0.93
75	24622.40	7014.93	0.93
76	24622.40	7014.93	0.93
77	24282.20	6918.00	0.91
78	24282.20	6918.00	0.91
79	24282.20	6918.00	0.91
80	24282.20	6918.00	0.91
81	24486.30	6976.16	0.92
82	24486.30	6976.16	0.92
83	24486.30	6976.16	0.92
84	24486.30	6976.16	0.92
85	24146.10	6879.23	0.91
86	24146.10	6879.23	0.91
87	24146.10	6879.23	0.91
88	24146.10	6879.23	0.91
89	24622.40	7014.93	0.93
90	24622.40	7014.93	0.93
91	24622.40	7014.93	0.93
92	24622.40	7014.93	0.93
93	24282.20	6918.00	0.91
94	24282.20	6918.00	0.91
95	24282.20	6918.00	0.91
96	24282.20	6918.00	0.91
97	24486.30	6976.16	0.92
98	24486.30	6976.16	0.92
99	24486.30	6976.16	0.92
100	24486.30	6976.16	0.92
101	24146.10	6879.23	0.91
102	24146.10	6879.23	0.91
103	24146.10	6879.23	0.91
104	24146.10	6879.23	0.91

Travata 515

B=1.30 <m> L=2.70 <m> k_1=2000000.00 <daN/mc> kw=757396.00 <daN/mc>

CC	N <daN>	q_{es} <daN/mq>	Ced <cm>
1	49547.50	14116.10	1.86
2	49359.30	14062.50	1.86
3	48405.50	13790.70	1.82
4	48403.00	13790.00	1.82
5	50650.70	14430.40	1.91
6	50283.10	14325.70	1.89
7	50454.40	14374.50	1.90
8	50118.70	14278.80	1.89
9	49029.00	13968.40	1.84
10	48925.10	13938.80	1.84
11	47887.00	13643.00	1.80
12	47968.80	13666.30	1.80
13	50132.30	14282.70	1.89
14	49849.00	14202.00	1.88
15	49936.00	14226.80	1.88
16	49684.60	14155.10	1.87
17	66750.50	19017.20	2.51
18	66698.40	19002.40	2.51
19	66487.30	18942.30	2.50
20	66961.60	19077.40	2.52
21	60583.80	17260.30	2.28
22	60531.70	17245.50	2.28
23	60320.60	17185.40	2.27
24	60794.90	17320.50	2.29
25	66224.50	18867.40	2.49
26	66172.30	18852.50	2.49
27	65961.30	18792.40	2.48
28	66435.60	18927.50	2.50
29	60057.80	17110.50	2.26
30	60005.60	17095.60	2.26

31	59794.60	17035.50	2.25
32	60268.80	17170.60	2.27
33	67557.20	19247.10	2.54
34	67505.00	19232.20	2.54
35	67294.00	19172.10	2.53
36	67768.30	19307.20	2.55
37	61390.50	17490.20	2.31
38	61338.30	17475.30	2.31
39	61127.30	17415.20	2.30
40	61601.50	17550.30	2.32
41	67031.10	19097.20	2.52
42	66979.00	19082.30	2.52
43	66767.90	19022.20	2.51
44	67242.20	19157.30	2.53
45	48855.60	13919.00	1.84
46	48803.40	13904.10	1.84
47	48592.40	13844.00	1.83
48	49066.60	13979.10	1.85
49	44744.40	12747.70	1.68
50	44692.30	12732.80	1.68
51	44481.20	12672.70	1.67
52	44955.50	12807.80	1.69
53	48504.90	13819.00	1.82
54	48452.70	13804.20	1.82
55	48241.60	13744.10	1.81
56	48715.90	13879.20	1.83
57	44393.70	12647.80	1.67
58	44341.60	12632.90	1.67
59	44130.50	12572.80	1.66
60	44604.80	12707.90	1.68
61	49393.30	14072.20	1.86
62	49341.20	14057.30	1.86
63	49130.10	13997.20	1.85
64	49604.40	14132.30	1.87
65	45282.20	12900.90	1.70
66	45230.00	12886.00	1.70
67	45019.00	12825.90	1.69
68	45493.20	12961.00	1.71
69	49042.60	13972.30	1.84
70	48990.50	13957.40	1.84
71	48779.40	13897.30	1.83
72	49253.70	14032.40	1.85
73	45258.80	12894.20	1.70
74	45206.70	12879.40	1.70
75	44995.60	12819.30	1.69
76	45469.90	12954.40	1.71
77	43888.40	12503.80	1.65
78	43836.30	12489.00	1.65
79	43625.20	12428.80	1.64
80	44099.50	12564.00	1.66
81	45118.50	12854.30	1.70
82	45066.40	12839.40	1.70
83	44855.30	12779.30	1.69
84	45329.60	12914.40	1.71
85	43748.10	12463.90	1.65
86	43696.00	12449.00	1.64
87	43484.90	12388.90	1.64
88	43959.20	12524.00	1.65
89	45527.70	12970.80	1.71
90	45475.50	12956.00	1.71
91	45264.50	12895.90	1.70
92	45738.70	13031.00	1.72
93	44157.30	12580.40	1.66
94	44105.20	12565.60	1.66
95	43894.10	12505.40	1.65
96	44368.40	12640.60	1.67
97	45387.40	12930.90	1.71
98	45335.30	12916.00	1.71
99	45124.20	12855.90	1.70
100	45598.50	12991.00	1.72
101	44017.00	12540.50	1.66
102	43964.90	12525.60	1.65
103	43753.80	12465.50	1.65

104 44228.10 12600.60 1.66

Criteri di analisi geotecnica e progetto delle fondazioni

Fondazioni superficiali

Generali

Generali
Condizioni di calcolo per terreni coesivi Sia drenate che non drenate
Calcolo di a' dal rapporto con c'
1
Calcolo di a_u dal rapporto con c_u
1
Calcolo di σ'dal rapporto con ϕ'
1
Considera l'angolo di attrito in deformazione piana per fondazioni nastriformi
No
Calcolo dei parametri rappresentativi per terreni stratificati
Media pesata
-Calcola i valori medi dell'angolo di attrito secondo la sua tangente
No
Capacità portante in condizioni statiche
Calcolo della capacità portante per rottura generale
Terzaghi (1943)
-Combinazione dei fattori di forma e di inclinazione del carico Considera solo i fattori di forma
-Considera il fattore di riduzione per platee
No
-Considera gli effetti dell'eccentricità del carico con un unico fattore riduttivo
No
Considera eccentricità e inclinazione dei carichi attraverso domini di interazione
No
-Parametro correttivo del momento
0
-Parametro correttivo del carico orizzontale
0
Calcolo della capacità portante per rottura locale
No

Vesic (1975)
Calcolo della capacità portante per rottura per punzonamento
No
Calcolo della capacità portante per scorrimento
No
-Percentuale di carico orizzontale assorbito dai cordoli <%>
0
-Percentuale di spinta passiva mobilitata <%>
0
Calcolo della capacità portante per sollevamento
No
Capacità portante in condizioni sismiche
Calcolo della capacità portante per rottura generale Metodo scelto per le condizioni statiche
Riduzione dell'angolo d'attrito per terreni incoerenti ben addensati
No
Calcolo della capacità portante per scorrimento
No
-Percentuale di carico orizzontale assorbito dai cordoli <%>
0
-Percentuale di spinta passiva mobilitata <%>
0
Cedimenti
Cedimenti
Terzaghi (1955)
-Costante di sottofondo standardizzata k_1
****
Considera pressioni di esercizio al netto delle tensioni litostatiche
No
Calcola costante di sottofondo per pressioni di esercizio
No

Limita costante di sottofondo ad un valore
No

Fondazioni profonde

Generali

Generali
Calcolo capacità portante per carichi verticali Secondo formule statiche
Considera capacità portante
Entrambe
Condizioni di calcolo per terreni coesivi Sia drenate che non drenate
Calcolo della profondità critica
No
Effettua calcolo elasto-plastico per cedimenti
Si
Effettua calcolo elasto-plastico per spostamenti orizzontali
Si
Rapporto di elasticità trazione/compressione pari a
1
Fattori di correlazione
1.7
Considera fattori di correlazione anche per carichi orizzontali
No
Considera peso del palo
No
Attrito laterale limite da prove in sito
Correlato con prove CPT
No
Correlato con prove SPT
No
Fattore di riduzione attrito laterale per pali trivellati
No
Pressione limite alla base da prove in sito
Correlata con prove CPT
No
Correlata con prove SPT
No
Fattore di riduzione pressione limite alla base per pali trivellati
No
Spostamenti orizzontali
Spostamenti orizzontali Risposta elastica in funzione della stratigrafia
Specifici
1 2 3 4 5 6 7 8 9 10

Attrito laterale limite
Calcolo dell'attrito laterale limite
Si Si Si Si Si Si Si Si Si Si
-Condizioni non drenate
-Calcolo di α
-Pari a
-A.G.I. (1984)
x x x x x x x x x x
-A.P.I. (1984)
-Viggiani (1999)
-Olson e Dennis (1982)
-Stas e Kulhavy (1984)
-Skempton (1986)
-Reese e O'Neill (1989)
-Metodo di Bustamente e Doix (1985) per micropali
No No No No No No No No No No
-Iniezioni ripetute
x x x x x x x x x x
-Unica iniezione
-Condizioni drenate
-Calcolo di β
-Pari a
0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3

-Reese e O'Neill (1989)
-Calcolato
-Calcolo di k
-Pari a
-Dal rapporto con k_0 pari a
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
-Fleming (1985)
-Calcolo di δ
-Pari a <grad>
-Dal rapporto con ϕ' pari a
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
-Calcolo di a' dal rapporto con c'
1 1 1 1 1 1 1 1 1 1
Calcolo dell'attrito laterale limite per trazione
-Considera i risultati del calcolo per l'attrito laterale limite percompressione con un fattore di riduzione pari a 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7
-Sowa (1970)
No No No No No No No No No No
-Bowles (1991)
No No No No No No No No No No
Considera l'effetto dell'attrito negativo
No No No No No No No No No
-Coefficiente di Lambe
Pressione limite alla base
Calcolo della pressione limite alla base del palo
Si Si Si Si Si Si Si Si Si Si
-Terzaghi (1943)
x x x x x x x x x x
-Meyerhof (1963)
-Hansen (1970)
-Vesic (1975)
-Berezantzev (1961)
-Berezantzev (1965)
-Stagg e Zienkiewicz (1968)
-Relazione generale, coefficienti di capacità portante
-In condizioni drenate
-N_q
-N_c
-In condizioni non drenate
-N_c
-Fattore di riduzione per terreni coesivi sovraconsolidati
No No No No No No No No No No
Cedimenti
Risposta elastica laterale
-Calcolata dalla rigidezza dello strato
x x x x x x x x x x
-Coefficiente di influenza
4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0
-Pari a <daN/mq>
Risposta elastica alla base
-Calcolata dalla rigidezza dello strato
x x x x x x x x x x
-Pari a <daN/mq>
Spostamenti orizzontali
Risposta elastica
-Vesic (1961)
-Broms (1964)
-Glick (1948)
-Chen (1978)
-Pari a <daN/mq>
-Dal modulo elastico
x x x x x x x x x x
-Coefficiente effetto tridimensionale
2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0
Resistenza limite
-Calcolata dai parametri plastici
x x x x x x x x x x
-Coefficiente effetto tridimensionale resistenza per attrito
3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0
-Coefficiente effetto tridimensionale resistenza per coesione
4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0
-Pari a <daN/mq>

Caratterizzazione

Specifici	1	2	3	4	5	6	7	8	9	10
Informazioni preliminari										
Coefficiente di uniformità	No	No	No	No	No	No	No	No	No	No
-Pari a	0	0	0	0	0	0	0	0	0	0
Definizione della composizione granulometrica, per terreni incoerenti	No	No	No	No	No	No	No	No	No	No
-Sabbia fine uniforme	x	x	x	x	x	x	x	x	x	x
-Sabbia fine ben gradata - sabbia media uniforme										
-Sabbia media ben gradata - sabbia grossa uniforme										
-Sabbia e ghiaia - ghiaia media										
Definizione indici compressibilità edometrica, per terreni coesivi	No	No	No	No	No	No	No	No	No	No
-Indice di compressione (Cc)	0	0	0	0	0	0	0	0	0	0
-Indice di ricompressione (Cr)	0	0	0	0	0	0	0	0	0	0
-Considera incremento preconsolidazione costante	No	No	No	No	No	No	No	No	No	No
-Pari a	0	0	0	0	0	0	0	0	0	0
Correggi NSPT se la misura è sottofalda	No	No	No	No	No	No	No	No	No	No
Densità relativa										
Correlata con prove SPT										
-Terzaghi e Peck (1948)	Si	Si	Si	Si	Si	Si	Si	Si	Si	Si
-Gibbs e Holtz (1957)	No	No	No	No	No	No	No	No	No	No
-Meyerhof (1957)	No	No	No	No	No	No	No	No	No	No
-Schultze e Menzenbach (1961)	No	No	No	No	No	No	No	No	No	No
-Bazaara (1967)	No	No	No	No	No	No	No	No	No	No
-Marcuson e Bieganousky (1977)	No	No	No	No	No	No	No	No	No	No
-Skempton (1986)	No	No	No	No	No	No	No	No	No	No
Correlata con prove CPT										
-Schmertmann (1976)	Si	Si	Si	Si	Si	Si	Si	Si	Si	Si
-Jamiolkowski et al. (1985)	No	No	No	No	No	No	No	No	No	No
-Baldi et al. (1986)	No	No	No	No	No	No	No	No	No	No
Elaborazione dei risultati										
-Valore medio	x	x	x	x	x	x	x	x	x	x
-Valore minore										
Angolo d'attrito										
Correlato con prove SPT										
-Terzaghi e Peck (1948)	Si	Si	Si	Si	Si	Si	Si	Si	Si	Si
-Schmertmann (1975)	No	No	No	No	No	No	No	No	No	No
-Wolff (1989)	No	No	No	No	No	No	No	No	No	No
-Hatanaka e Uchida (1996)	No	No	No	No	No	No	No	No	No	No
-Road Bridge Specification	No	No	No	No	No	No	No	No	No	No
-Owasaki e Iwasaki	No	No	No	No	No	No	No	No	No	No

-Japanese National Railway	No	No	No	No	No	No	No	No	No	No
-Peck-Hanson e Thornburn	No	No	No	No	No	No	No	No	No	No
-De Mello	No	No	No	No	No	No	No	No	No	No
Correlato con prove CPT										
-Robertson e Campanella (1983)	Si	Si	Si	Si	Si	Si	Si	Si	Si	Si
-Durgunoglu e Mitchell	No	No	No	No	No	No	No	No	No	No
-Caquot	No	No	No	No	No	No	No	No	No	No
Correlata con proprietà indice										
-In funzione della densità relativa, per terreni incoerenti	No	No	No	No	No	No	No	No	No	No
-In funzione dell'indice di plasticità, per terreni coesivi	No	No	No	No	No	No	No	No	No	No
Elaborazione dei risultati										
-Valore medio	x	x	x	x	x	x	x	x	x	x
-Valore minore										
Coesione non drenata										
Correlata con prove SPT										
-Hara et al. (1971)	No	Si	Si	Si	Si	Si	Si	Si	Si	Si
-Stroud (1974)	No	No	No	No	No	No	No	No	No	No
Correlata con prove CPT										
-Mayne e Kemper (1988)	Si	Si	Si	Si	Si	Si	Si	Si	Si	Si
-Lunne e Eide	No	No	No	No	No	No	No	No	No	No
Correlata con proprietà indice										
-Bjerrum e Simons (1960)	No	No	No	No	No	No	No	No	No	No
-Skempton (1953)	No	No	No	No	No	No	No	No	No	No
-Calcolata da $\sigma'v_0$ con moltiplicatore pari a	No	No	No	No	No	No	No	No	No	No
Pari a	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Elaborazione dei risultati										
-Valore medio	x	x	x	x	x	x	x	x	x	x
-Valore minore										
Caratteristiche litostatiche										
Grado di sovraconsolidazione										
-Correlato con prove SPT										
-Mayne e Kemper (1988)	Si	No	No	No	No	No	No	No	No	No
-Correlato con prove CPT										
-Mayne e Kemper (1988)	No	No	No	No	No	No	No	No	No	No
-Elaborazione dei risultati										
-Valore medio	x	x	x	x	x	x	x	x	x	x
-Valore minore										
Coefficiente di spinta a riposo										
-Calcolo di k_0 (NC)										
-Jaky (1936)		x	x	x	x	x	x	x	x	x
-Brooker e Ireland (1965)	x									
-Alpan (1967)										
-Massarsch (1979)										
-Correlato con Dr										
-Calcolato dal coefficiente di Poisson										
-Calcolo di α										
-Pari a										
-Kulhawy (1989)	x	x	x	x	x	x	x	x	x	x
-Alpan (1967) per terreni coesivi										
-Alpan (1967) per terreni incoerenti										

-Correlato con Dr
Parametri elastici
Correlati con prove GFS
Correlati con prove SPT
-Stroud e Butler (1975)
-Stroud (1989) x x x x x x x x x x
-Schmertmann (1978)
-Farrent
-Menzenbach e Malcev
-D'Appolonia
-Schulze e Menzenbach
-Crespellani e Vannucchi
-Ohsaki e Iwasaki, per sabbie
-Ohsaki e Iwasaki, per sabbie con fini
Correlati con prove CPT
-Schmertmann (1977)
-Robertson e Campanella (1983)
-Kulhawy e Mayne (1990)
-Rix e Stokoe (1992)
-Mayne e Rix (1993)
Fattore correttivo 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0

PIU – PROGETTO INNOVAZIONE URBANA

OPERAZIONE COWORKING, MEDIALIBRARY

A6 – RELAZIONE GEOTECNICA

NUOVO SOPPALCO IN ACCIAIO

(OTTOBRE 2017)

Introduzione

Sistemi di riferimento
Le coordinate, i carichi concentrati, i cedimenti, le reazioni vincolari e gli spostamenti dei NODI sono riferiti ad una terna destra cartesiana globale con l'asse Z verticale rivolto verso l'alto.
I carichi in coordinate locali e le sollecitazioni delle ASTE sono riferite ad una terna destra cartesiana locale così definita:
- origine nel nodo iniziale dell'asta;
- asse X coincidente con l'asse dell'asta e con verso dal nodo iniziale al nodo finale;
- immaginando la trave a sezione rettangolare l'asse Y è parallelo alla base e l'asse Z è parallelo all'altezza. La rotazione dell'asta comporta quindi una rotazione di tutta la terna locale.

Si può immaginare la terna locale di un'asta comunque disposta nello spazio come derivante da quella globale dopo una serie di trasformazioni:
- una rotazione intorno all'asse Z che porti l'asse X a coincidere con la proiezione dell'asse dell'asta sul piano orizzontale;
- una traslazione lungo il nuovo asse X così definito in modo da portare l'origine a coincidere con la proiezione del nodo iniziale dell'asta sul piano orizzontale;
- una traslazione lungo l'asse Z che porti l'origine a coincidere con il nodo iniziale dell'asta;
- una rotazione intorno all'asse Y così definito che porti l'asse X a coincidere con l'asse dell'asta;
- una rotazione intorno all'asse X così definito pari alla rotazione dell'asta.

In pratica le travi prive di rotazione avranno sempre l'asse Z rivolto verso l'alto e l'asse Y nel piano del solaio, mentre i pilastri privi di rotazione avranno l'asse Y parallelo all'asse Y globale e l'asse Z parallelo ma controverso all'asse X globale. Da notare quindi che per i pilastri la "base" è il lato parallelo a Y.

Le sollecitazioni ed i carichi in coordinate locali negli ELEMENTI BIDIMENSIONALI e nei MURI sono riferiti ad una terna destra cartesiana locale così definita:
- origine nel primo nodo dell'elemento;
- asse X coincidente con la congiungente il primo ed il secondo nodo dell'elemento;
- asse Y definito come prodotto vettoriale fra il versore dell'asse X e il versore della congiungente il primo e il quarto nodo. Asse Z a formare con gli altri due una terna destrorsa.

Praticamente un elemento verticale con l'asse X locale coincidente con l'asse X globale ha anche gli altri assi locali coincidenti con quelli globali.

Rotazioni e momenti
Seguendo il principio adottato per tutti i carichi che sono positivi se CONTROVERSI agli assi, anche i momenti concentrati e le rotazioni impresse in coordinate globali risultano positivi se CONTROVERSI al segno positivo delle rotazioni. Il segno positivo dei momenti e delle rotazioni è quello orario per l'osservatore posto nell'origine: X ruota su Y, Y ruota su Z, Z ruota su X. In pratica è sufficiente adottare la regola della mano destra: col pollice rivolto nella direzione dell'asse, la rotazione che porta a chiudere il palmo della mano corrisponde al segno positivo.

Normativa di riferimento
La normativa di riferimento è la seguente:
- Legge n. 64 del 2/2/1974 - Provvedimenti per le costruzioni con particolari prescrizioni per le zone sismiche.

- D.M. del 24/1/1986 - Norme tecniche relative alle costruzioni sismiche.

- Legge n. 1086 del 5/11/1971 - Norme per la disciplina delle opere di conglomerato cementizio armato, normale e precompresso ed a struttura metallica.

- D.M. del 14/2/1992 - Norme tecniche per l'esecuzione delle opere in c.a. normale e precompresso e per le strutture metalliche.

- D.M. del 9/1/1996 - Norme tecniche per l'esecuzione delle opere in c.a. normale e precompresso e per le strutture metalliche.

- D.M. del 16/1/1996 - Norme tecniche per le costruzioni in zone sismiche.

- Circolare n. 21745 del 30/7/1981 - Legge n. 219 del 14/5/1981 - Art. 10 - Istruzioni relative al

rafforzamento degli edifici in muratura danneggiati dal sisma.

- Regione Autonoma Friuli Venezia Giulia - Legge Regionale n. 30 del 20/6/1977 - Documentazione tecnica per la progettazione e direzione delle opere di riparazione degli edifici - Documento Tecnico n. 2 - Raccomandazioni per la riparazione strutturale degli edifici in muratura.

- D.M. del 20/11/1987 - Norme Tecniche per la progettazione, esecuzione e collaudo degli edifici in muratura e per il loro consolidamento.

- Norme Tecniche C.N.R. n. 10011-85 del 18/4/1985 - Costruzioni di acciaio - Istruzioni per il calcolo, l'esecuzione, il collaudo e la manutenzione.

- Norme Tecniche C.N.R. n. 10025-84 del 14/12/1984 - Istruzioni per il progetto, l'esecuzione ed il controllo delle strutture prefabbricate in conglomerato cementizio e per le strutture costruite con sistemi industrializzati di acciaio - Istruzioni per il calcolo, l'esecuzione, il collaudo e la manutenzione.

- Circolare n. 65 del 10/4/1997 - Istruzioni per l'applicazione delle "Norme tecniche per le costruzioni in zone sismiche" di cui al D.M. del 16/1/1996.

- Eurocodice 5 - Progettazione delle strutture di legno.

- DIN 1052 - Metodi di verifica per il legno.

- D.M. del 14/1/2008 - Norme tecniche per le costruzioni. Le verifiche degli elementi di fondazione sono eseguite utilizzando l'Approccio 2.

- Circolare n. 617 del 2/2/2009 - Istruzioni per l'applicazione delle "Nuove norme tecniche per le costruzioni" di cui al D.M. del 14/1/2008.

- Documento Tecnico CNR-DT 200 R1/2012 - Istruzioni per la Progettazione, l'Esecuzione ed il Controllo di Interventi di Consolidamento Statico mediante l'utilizzo di Compositi Fibrorinforzati.

- Eurocodice 3 - Progettazione delle strutture in acciaio.

Unità di misura
Le unità di misura adottate sono le seguenti:
- lunghezze : m
- forze : daN
- masse : kg
- temperature : gradi centigradi
- angoli : gradi sessadecimali o radianti

ELENCO VINCOLI NODI

Simbologia

Vn = Numero del vincolo nodo
Comm. = Commento
TV = Tipo vincolo se valutato da stratigrafia
SP = Plinto senza pali
CP = Palo o plinto con pali
Sx = Spostamento in dir. X (L=libero, B=bloccato, E=elastico)
Sy = Spostamento in dir. Y (L=libero, B=bloccato, E=elastico)
Sz = Spostamento in dir. Z (L=libero, B=bloccato, E=elastico)
Rx = Rotazione intorno all'asse X (L=libera, B=bloccata, E=elastica)
Ry = Rotazione intorno all'asse Y (L=libera, B=bloccata, E=elastica)
Rz = Rotazione intorno all'asse Z (L=libera, B=bloccata, E=elastica)
RL = Rotazione libera
Ly = Lunghezza (dir. Y locale)
Lz = Larghezza (dir. Z locale)
Kt = Coeff. di sottofondo su suolo elastico alla Winkler

Vn	Comm.	TV	Sx	Sy	Sz	Rx	Ry	Rz	RL	Ly <m>	Lz <m>	Kt <daN/cmc>
1	Libero		L	L	L	L	L	L				
4		SP	B	B	E	E	E	B				f(strat.)

Vn	Comm.	TV	Sx	Sy	Sz	Rx	Ry	Rz	RL	Ly <m>	Lz <m>	Kt <daN/cmc>
4		CP	E	E	E	E	E	B				f(strat.)

ELENCO COSTANTI ELASTICHE NODALI

Simbologia

Nodo = Numero del nodo
Kx = Costante elastica in dir. X
Ky = Costante elastica in dir. Y
Kz = Costante elastica in dir. Z
KRx = Costante elastica intorno all'asse X
KRy = Costante elastica intorno all'asse Y

Nodo	Kx	Ky	Kz	KRx	KRy	Nodo	Kx	Ky	Kz	KRx	KRy
	<daN/cm>	<daN/cm>	<daN/cm>	<daNm/rad>	<daNm/rad>		<daN/cm>	<daN/cm>	<daN/cm>	<daNm/rad>	<daNm/rad>
1	--	--	6634.84	44785.20	44785.20	2	--	--	8446.54	101359.00	101359.00
3	--	--	6634.84	44785.20	44785.20	4	--	--	6634.84	44785.20	44785.20
5	--	--	8446.54	101359.00	101359.00	6	--	--	6634.84	44785.20	44785.20
7	--	--	6634.84	44785.20	44785.20	8	--	--	6634.84	44785.20	44785.20
9	--	--	6634.84	44785.20	44785.20						

ELENCO NODI

Simbologia

Nodo = Numero del nodo
X = Coordinata X del nodo
Y = Coordinata Y del nodo
Z = Coordinata Z del nodo
Imp. = Numero dell'impalcato
Vn = Numero del vincolo nodo

Nodo	X	Y	Z	Imp.	Vn	Nodo	X	Y	Z	Imp.	Vn	Nodo	X	Y	Z	Imp.	Vn	Nodo	X	Y	Z	Imp.	Vn
	<m>	<m>	<m>				<m>	<m>	<m>				<m>	<m>	<m>				<m>	<m>	<m>		
-3	10.00	3.32	3.95	1	1	-2	5.00	3.32	3.95	1	1	-1	0.00	3.32	3.95	1	1	1	0.00	0.00	0.00	0	4
2	5.00	0.00	0.00	0	4	3	10.00	0.00	0.00	0	4	4	0.00	6.64	0.00	0	4	5	5.00	6.64	0.00	0	4
6	10.00	6.64	0.00	0	4	7	0.00	10.50	0.00	0	4	8	5.00	10.50	0.00	0	4	9	10.00	10.50	0.00	0	4
101	0.00	0.00	3.95	1	1	102	5.00	0.00	3.95	1	1	103	10.00	0.00	3.95	1	1	104	0.00	6.64	3.95	1	1
105	5.00	6.64	3.95	1	1	106	10.00	6.64	3.95	1	1	107	0.00	10.50	3.95	1	1	108	5.00	10.50	3.95	1	1
109	10.00	10.50	3.95	1	1																		

ELENCO MATERIALI

Simbologia

Mat. = Numero del materiale
Comm. = Commento
P = Peso specifico
E = Modulo elastico
G = Modulo elastico tangenziale
ν = Coeff. di Poisson
α = Coeff. di dilatazione termica

Mat.	Comm.	P <daN/mc>	E <daN/cmq>	G <daN/cmq>	ν	α
2	Acciaio	7850	2100000.00	800000.00	0.3	1.000000E-05

ELENCO SEZIONI ASTE

Simbologia

Sez. = Numero della sezione
Comm. = Commento
Tipo = Tipologia
- 2C = Doppia C lato labbri
- 2Cdx = Doppia C lato costola
- 2I = Doppia I
- 2L = Doppia L lato labbri
- 2Ldx = Doppia L lato costole
- C = Sezione a C
- Cdx = C destra
- Cir. = Circolare
- Cir.c = Circolare cava
- I = Sezione a I
- L = Sezione a L
- Ldx = L destra
- Om. = Omega
- Pg = Pi greco
- Pr = Poligono regolare
- Prc = Poligono regolare cavo
- Pc = Per coordinate
- Ia = Inerzie assegnate
- R = Rettangolare
- Rc = Rettangolare cava
- T = Sezione a T
- U = Sezione a U
- Ur = U rovescia
- V = Sezione a V
- Vr = V rovescia
- Z = Sezione a Z
- Zdx = Z destra
- Ts = T stondata
- Ls = L stondata
- Cs = C stondata
- Is = I stondata
- Dis. = Disegnata

Mem. = Membratura
- G = Generica
- T = Trave
- P = Pilastro

Ver. = Verifica prevista
- N = Nessuna
- C = Cemento armato
- A = Acciaio
- L = Legno

B = Base
H = Altezza
s = Spessore ala
a = Spessore anima
r = Raggio raccordo anima-ala
r1 = Raggio in testa ala
Ma = Numero del materiale
C = Numero del criterio di progetto
Crit. C.I. = Criterio di progetto collegamento iniziale
Crit. C.F. = Criterio di progetto collegamento finale

Sez.	Comm.	Tipo	Mem.	Ver.	B <cm>	H <cm>	s <cm>	a <cm>	r <cm>	r1 <cm>	Ma	C	Crit. C.I.	Crit. C.F.
3	HEB220	Is	P	A	22.00	22.00	1.60	0.95	1.80	0.00	2	2	1	10
6	IPE240	Is	T	A	12.00	24.00	0.98	0.62	1.50	0.00	2	1	10	10
7	HEA220	Is	T	A	22.00	21.00	1.10	0.70	1.80	0.00	2	1	10	10

ELENCO VINCOLI ASTE

Simbologia

Va = Numero del vincolo asta
Comm. = Commento
Tipo = Tipologia
SVI = Definizione di vincolamenti interni
ELA = Vincolo su suolo elastico alla Winkler
BIE-RTC = Biella resistente a trazione e a compressione
BIE-RC = Biella resistente solo a compressione
BIE-RT = Biella resistente solo a trazione
Ni = Sforzo normale nodo iniziale (0=sbloccato, 1=bloccato)
Tyi = Taglio in dir. Y locale nodo iniziale (0=sbloccato, 1=bloccato)
Tzi = Taglio in dir. Z locale nodo iniziale (0=sbloccato, 1=bloccato)
Mxi = Momento intorno all'asse X locale nodo iniziale (0=sbloccato, 1=bloccato)
Myi = Momento intorno all'asse Y locale nodo iniziale (0=sbloccato, 1=bloccato)
Mzi = Momento intorno all'asse Z locale nodo iniziale (0=sbloccato, 1=bloccato)
Nf = Sforzo normale nodo finale (0=sbloccato, 1=bloccato)
Tyf = Taglio in dir. Y locale nodo finale (0=sbloccato, 1=bloccato)
Tzf = Taglio in dir. Z locale nodo finale (0=sbloccato, 1=bloccato)
Mxf = Momento intorno all'asse X locale nodo finale (0=sbloccato, 1=bloccato)
Myf = Momento intorno all'asse Y locale nodo finale (0=sbloccato, 1=bloccato)
Mzf = Momento intorno all'asse Z locale nodo finale (0=sbloccato, 1=bloccato)
Kt = Coeff. di sottofondo su suolo elastico alla Winkler

Va	Comm.	Tipo	Ni	Tyi	Tzi	Mxi	Myi	Mzi	Nf	Tyf	Tzf	Mxf	Myf	Mzf	Kt <daN/cmc>
1	Inc+Inc	SVI	1	1	1	1	1	1	1	1	1	1	1	1	
3	Cer+Inc	SVI	1	1	1	0	0	0	1	1	1	1	1	1	

ELENCO ASTE

Simbologia

Asta = Numero dell'asta
N1 = Nodo iniziale
N2 = Nodo finale
Sez. = Numero della sezione
Va = Numero del vincolo asta
Par. = Numero dei parametri aggiuntivi
Rot. = Rotazione
FF = Filo fisso
Dy1 = Scost. filo fisso Y1
Dy2 = Scost. filo fisso Y2
Dz1 = Scost. filo fisso Z1
Dz2 = Scost. filo fisso Z2
TC1 = Tipo collegamento iniziale
TC2 = Tipo collegamento finale
Kt = Coeff. di sottofondo su suolo elastico alla Winkler

Asta	N1	N2	Sez.	Va	Par.	Rot. <grad>	FF	Dy1 <cm>	Dy2 <cm>	Dz1 <cm>	Dz2 <cm>	TC1	TC2	Kt <daN/cmc>
1	1	101	3	3		0.00	55	-11.00	-11.00	0.00	0.00	PF	FEI	
2	2	102	3	3		0.00	55	-11.00	-11.00	0.00	0.00	PF	FRM	
3	3	103	3	3		0.00	55	-11.00	-11.00	0.00	0.00	PF	FEI	
4	4	104	3	3		0.00	55	0.00	0.00	0.00	0.00	PF	CS	
5	5	105	3	3		0.00	55	0.00	0.00	0.00	0.00	PF	FRM	
6	6	106	3	3		0.00	55	0.00	0.00	0.00	0.00	PF	CS	
7	7	107	3	3		0.00	55	0.00	0.00	0.00	0.00	PF	CS	
8	8	108	3	3		0.00	55	0.00	0.00	0.00	0.00	PF	FREI	
9	9	109	3	3		0.00	55	0.00	0.00	0.00	0.00	PF	CS	
101	101	102	6	1		0.00	22	-11.00	-11.00	0.00	0.00	FR	FREI	
101	102	103	6	1		0.00	22	-11.00	-11.00	0.00	0.00	FRM	FRESI	
102	-1	-2	6	1		0.00	22	0.00	0.00	0.00	0.00	CA	CA	
102	-2	-3	6	1		0.00	22	0.00	0.00	0.00	0.00	CA	CA	

```
 103 104 105    6  1        0.00 22   0.00   0.00 0.00 0.00 ND  ND
 103 105 106    6  1        0.00 22   0.00   0.00 0.00 0.00 FRM ND
 104 107 108    6  1        0.00 22   0.00   0.00 0.00 0.00 ND  ND
 104 108 109    6  1        0.00 22   0.00   0.00 0.00 0.00 ND  ND
 105 101  -1    6  1        0.00 22   0.00   0.00 0.00 0.00 ND  ND
 105  -1 104    6  1        0.00 22   0.00   0.00 0.00 0.00 ND  ND
 105 104 107    6  1        0.00 22   0.00   0.00 0.00 0.00 ND  ND
 106 102  -2    7  1        0.00 22   0.00   0.00 0.00 0.00 FRM CAA
 106  -2 105    7  1        0.00 22   0.00   0.00 0.00 0.00 CAA CAA
 106 105 108    6  1        0.00 22   0.00   0.00 0.00 0.00 ND  FREI
 107 103  -3    6  1        0.00 22   0.00   0.00 0.00 0.00 ND  ND
 107  -3 106    6  1        0.00 22   0.00   0.00 0.00 0.00 ND  ND
 107 106 109    6  1        0.00 22   0.00   0.00 0.00 0.00 ND  ND
```

ELENCO TIPI PLINTI/PALI

Simbologia

```
Tl    = Numero del tipo plinto/palo
Tipo  = Tipologia
        Gra = Gradoni
        Pir = Piramidale
        P = Palo
        T3 = Triangolare 3 pali
        T3B = Triangolare 3 pali + bicchiere
        R = Rettangolare
        RB = Rettangolare + bicchiere
        R1 = Rettangolare 1 palo
        R1B = Rettangolare 1 palo + bicchiere
        R2x = Rettangolare 2 pali dir. X
        R2xB = Rettangolare 2 pali dir. X + bicchiere
        R2y = Rettangolare 2 pali dir. Y
        R2B = Rettangolare 2 pali dir. Y + bicchiere
        R4 = Rettangolare 4 pali
        R4B = Rettangolare 4 pali + bicchiere
        P5 = Pentagonale 5 pali
        P5B = Pentagonale 5 pali + bicchiere
        E6 = Esagonale 6 pali
        E6B = Esagonale 6 pali + bicchiere
Tp    = Tipo palo
        ND = Non definito
        BP = Battuto prefabbricato
        BGO = Battuto gettato in opera
        T = Trivellato
        TEC = Trivellato con elica continua
        MP = Micropalo
Comm. = Commento
A1    = Prima dimensione plinto/palo in dir. X
A2    = Seconda dimensione plinto/palo in dir. X
B1    = Prima dimensione plinto/palo in dir. Y
B2    = Seconda dimensione plinto/palo in dir. Y
H1    = Altezza parte inferiore plinto/palo
c1    = Allargamento magrone in dir. X
c2    = Allargamento magrone in dir. Y
h     = Altezza magrone
Crit. = Numero del criterio di progetto
```

Tl	Tipo	Tp	Comm.	A1 <m>	A2 <m>	B1 <m>	B2 <m>	H1 <m>	c1 <m>	c2 <m>	h <m>	Crit.	Tl	Tipo	Tp	Comm.	A1 <m>	A2 <m>	B1 <m>	B2 <m>	H1 <m>	c1 <m>	c2 <m>	h <m>	Crit.
2	R	--		0.60	0.60	0.60	0.60	0.20	0.15	0.15	0.15	1	3	R	--		0.45	0.45	0.45	0.45	0.20	0.15	0.15	0.15	1

ELENCO PLINTI/PALI

Simbologia

PL   = Plinto/Palo
Tl   = Numero del tipo plinto/palo
Nodo = Nodo plinto/palo
Kt   = Coeff. di sottofondo su suolo elastico alla Winkler

PL	Tl	Nodo	Kt <daN/cmc>	PL	Tl	Nodo	Kt <daN/cmc>	PL	Tl	Nodo	Kt <daN/cmc>	PL	Tl	Nodo	Kt <daN/cmc>	PL	Tl	Nodo	Kt <daN/cmc>
1	3	1	0.82	2	2	2	0.59	3	3	3	0.82	4	3	4	0.82	5	2	5	0.59
6	3	6	0.82	7	3	7	0.82	8	3	8	0.82	9	3	9	0.82				

ELENCO TIPI SOLAI

Simbologia

Ts   = Numero del tipo solaio
Comm.   = Commento
Rc   = Ripartizione carichi
  UN = Unidirezionale
  PP = A piastra perimetrale
  PB = A piastra bisettrice
Qps   = Carico permanente strutturale
Qpn   = Carico permanente non strutturale
QA   = Primo carico accidentale
QA2   = Secondo carico accidentale
QA3   = Terzo carico accidentale
Rip. ter. = Ripartizione su aste terminali
Rip. int. = Ripartizione su aste interne
Lfl   = Larghezza fascia laterale
Zcv   = Quota di riferimento del piano di campagna
s   = Coeff. di riduzione

Ts	Comm.	Rc	Qps <daN/mq>	Qpn <daN/mq>	QA <daN/mq>	QA2 <daN/mq>	QA3 <daN/mq>	Rip. ter.	Rip. int.	Lfl <m>	Zcv <m>	s
1		PP	215.00	40.00	350.00	0.00	0.00	--	--	--	0.00	0.33

ELENCO SOLAI

Simbologia

Sol. = Numero del solaio
Ts   = Numero del tipo solaio
Ord. = Orditura
Nodi = Nodi del solaio

Sol.	Ts	Ord. <grad>	Nodi	Sol.	Ts	Ord. <grad>	Nodi	Sol.	Ts	Ord. <grad>	Nodi
100	1	90.00	101 102 -2 -1	101	1	90.00	-1 -2 105 104	102	1	90.00	-2 -3 106 105
103	1	90.00	105 106 109 108	104	1	90.00	104 105 108 107	105	1	90.00	102 103 -3 -2

CONDIZIONI DI CARICO ELEMENTARI:

Simbologia

CCE   = Numero della condizione di carico elementare
Comm.   = Commento
Tipo CCE = Tipo di CCE per calcolo agli stati limite
Sic.   = Contributo alla sicurezza
  F = a favore
  S = a sfavore
  A = ambigua

Var.   = Tipo di variabilità
           B = di base
           I = indipendente
           A = ambigua
Dir.   = Direzione del vento
Tipo   = Tipologia di pressione vento
           M = Massimizzata
           E = Esterna
           I = Interna
Mx   = Moltiplicatore della massa in dir. X
My   = Moltiplicatore della massa in dir. Y
Mz   = Moltiplicatore della massa in dir. Z
Jpx   = Moltiplicatore del momento d'inerzia intorno all'asse X
Jpy   = Moltiplicatore del momento d'inerzia intorno all'asse Y
Jpz   = Moltiplicatore del momento d'inerzia intorno all'asse Z

Condizioni di carico elementari

CCE	Comm.	Tipo CCE	Sic.	Var.	Dir. <grad>	Tipo	Mx	My	Mz	Jpx	Jpy	Jpz
1	Peso+ps	1 D.M. 08 Permanenti strutturali	S	--	--	--	1.00	1.00	0.00	0.00	0.00	1.00
2	qpn	2 D.M. 08 Permanenti non strutturali	S	--	--	--	1.00	1.00	0.00	0.00	0.00	1.00
3	QACC1	4 D.M. 08 Variabili Categoria B Uffici	S	B	--	--	1.00	1.00	0.00	0.00	0.00	1.00

ELENCO CARICHI ASTE

CONDIZIONE DI CARICO 1: Peso+ps

ELENCO PESO PROPRIO ASTE

Simbologia

Sez. = Numero della sezione
Comm. = Commento
A   = Area
Mat. = Materiale
P   = Peso specifico
PL   = Peso specifico a metro lineare

Sez.	Comm.	A <cmq>	Mat.	P <daN/mc>	PL <daN/m>
3	HEB220	91.043100	Acciaio	7850.00	71.47
7	HEA220	64.342900	Acciaio	7850.00	50.51
6	IPE240	39.117500	Acciaio	7850.00	30.71

ELENCO CARICHI ASTE

CONDIZIONE DI CARICO 1: Peso+ps

CARICHI DISTRIBUITI

Simbologia

Asta = Numero dell'asta
N1   = Nodo iniziale
N2   = Nodo finale
E   = Elemento provenienza del carico
       S = Solaio
       T = Tamponatura
NE   = Numero elemento di provenienza del carico
T   = Tipo di carico
       QA = Primo carico accidentale
       QA2 = Secondo carico accidentale
       QA3 = Terzo carico accidentale
       QPS = Carico permanente strutturale
       QPN = Carico permanente non strutturale
       VE = Vento
       M = Manuale
DC   = Direzione del carico
       XG,YG,ZG = secondo gli assi globali

XL,YL,ZL = secondo gli assi locali
Xi = Distanza iniziale
Qi = Carico iniziale
Xf = Distanza finale
Qf = Carico finale

Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>	Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>
101	101	102	S	100	QPS	ZG	0.00	214.48	5.00	214.48	101	102	103	S	105	QPS	ZG	0.00	214.48	5.00	214.48
102	-1	-2	S	100	QPS	ZG	0.00	214.48	5.00	214.48	102	-1	-2	S	101	QPS	ZG	0.00	214.48	5.00	214.48
102	-2	-3	S	102	QPS	ZG	0.00	214.48	5.00	214.48	102	-2	-3	S	105	QPS	ZG	0.00	214.48	5.00	214.48
103	104	105	S	101	QPS	ZG	0.00	214.48	5.00	214.48	103	104	105	S	104	QPS	ZG	0.00	234.17	5.00	234.17
103	105	106	S	102	QPS	ZG	0.00	214.48	5.00	214.48	103	105	106	S	103	QPS	ZG	0.00	234.17	5.00	234.17
104	107	108	S	104	QPS	ZG	0.00	234.17	5.00	234.17	104	108	109	S	103	QPS	ZG	0.00	234.17	5.00	234.17
105	101	-1	S	100	QPS	ZG	0.00	214.48	3.32	214.48	105	-1	104	S	101	QPS	ZG	0.00	214.48	3.32	214.48
105	104	107	S	104	QPS	ZG	0.00	234.17	3.86	234.17	106	102	-2	S	100	QPS	ZG	0.00	214.48	3.32	214.48
106	102	-2	S	105	QPS	ZG	0.00	214.48	3.32	214.48	106	-2	105	S	101	QPS	ZG	0.00	214.48	3.32	214.48
106	-2	105	S	102	QPS	ZG	0.00	214.48	3.32	214.48	106	105	108	S	103	QPS	ZG	0.00	234.17	3.86	234.17
106	105	108	S	104	QPS	ZG	0.00	234.17	3.86	234.17	107	103	-3	S	105	QPS	ZG	0.00	214.48	3.32	214.48
107	-3	106	S	102	QPS	ZG	0.00	214.48	3.32	214.48	107	106	109	S	103	QPS	ZG	0.00	234.17	3.86	234.17

ELENCO CARICHI ASTE

CONDIZIONE DI CARICO 2: qpn

CARICHI DISTRIBUITI

Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>	Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>
101	101	102	S	100	QPN	ZG	0.00	39.90	5.00	39.90	101	102	103	S	105	QPN	ZG	0.00	39.90	5.00	39.90
102	-1	-2	S	100	QPN	ZG	0.00	39.90	5.00	39.90	102	-1	-2	S	101	QPN	ZG	0.00	39.90	5.00	39.90
102	-2	-3	S	102	QPN	ZG	0.00	39.90	5.00	39.90	102	-2	-3	S	105	QPN	ZG	0.00	39.90	5.00	39.90
103	104	105	S	101	QPN	ZG	0.00	39.90	5.00	39.90	103	104	105	S	104	QPN	ZG	0.00	43.57	5.00	43.57
103	105	106	S	102	QPN	ZG	0.00	39.90	5.00	39.90	103	105	106	S	103	QPN	ZG	0.00	43.57	5.00	43.57
104	107	108	S	104	QPN	ZG	0.00	43.57	5.00	43.57	104	108	109	S	103	QPN	ZG	0.00	43.57	5.00	43.57
105	101	-1	S	100	QPN	ZG	0.00	39.90	3.32	39.90	105	-1	104	S	101	QPN	ZG	0.00	39.90	3.32	39.90
105	104	107	S	104	QPN	ZG	0.00	43.57	3.86	43.57	106	102	-2	S	100	QPN	ZG	0.00	39.90	3.32	39.90
106	102	-2	S	105	QPN	ZG	0.00	39.90	3.32	39.90	106	-2	105	S	101	QPN	ZG	0.00	39.90	3.32	39.90
106	-2	105	S	102	QPN	ZG	0.00	39.90	3.32	39.90	106	105	108	S	103	QPN	ZG	0.00	43.57	3.86	43.57
106	105	108	S	104	QPN	ZG	0.00	43.57	3.86	43.57	107	103	-3	S	105	QPN	ZG	0.00	39.90	3.32	39.90
107	-3	106	S	102	QPN	ZG	0.00	39.90	3.32	39.90	107	106	109	S	103	QPN	ZG	0.00	43.57	3.86	43.57

ELENCO CARICHI ASTE

CONDIZIONE DI CARICO 3: QACC1

CARICHI DISTRIBUITI

Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>
101	101	102	S	100	QA	ZG	0.00	349.16	5.00	349.16
102	-1	-2	S	100	QA	ZG	0.00	349.16	5.00	349.16
102	-2	-3	S	102	QA	ZG	0.00	349.16	5.00	349.16
103	104	105	S	101	QA	ZG	0.00	349.16	5.00	349.16
103	105	106	S	102	QA	ZG	0.00	349.16	5.00	349.16
104	107	108	S	104	QA	ZG	0.00	381.21	5.00	381.21
105	101	-1	S	100	QA	ZG	0.00	349.16	3.32	349.16
105	104	107	S	104	QA	ZG	0.00	381.21	3.86	381.21
106	102	-2	S	105	QA	ZG	0.00	349.16	3.32	349.16
106	-2	105	S	102	QA	ZG	0.00	349.16	3.32	349.16
106	105	108	S	104	QA	ZG	0.00	381.21	3.86	381.21
107	-3	106	S	102	QA	ZG	0.00	349.16	3.32	349.16
101	102	103	S	105	QA	ZG	0.00	349.16	5.00	349.16
102	-1	-2	S	101	QA	ZG	0.00	349.16	5.00	349.16
102	-2	-3	S	105	QA	ZG	0.00	349.16	5.00	349.16
103	104	105	S	104	QA	ZG	0.00	381.21	5.00	381.21
103	105	106	S	103	QA	ZG	0.00	381.21	5.00	381.21
104	108	109	S	103	QA	ZG	0.00	381.21	5.00	381.21
105	-1	104	S	101	QA	ZG	0.00	349.16	3.32	349.16
106	102	-2	S	100	QA	ZG	0.00	349.16	3.32	349.16
106	-2	105	S	101	QA	ZG	0.00	349.16	3.32	349.16
106	105	108	S	103	QA	ZG	0.00	381.21	3.86	381.21
107	103	-3	S	105	QA	ZG	0.00	349.16	3.32	349.16
107	106	109	S	103	QA	ZG	0.00	381.21	3.86	381.21

PARAMETRI DI CALCOLO
La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con:
ModeSt ver. 8.14, prodotto da Tecnisoft s.a.s. - Prato

La struttura è stata calcolata utilizzando come solutore agli elementi finiti:
Xfinest ver. 2014, prodotto da Ce.A.S. S.r.l. - Milano

Tipo di normativa: stati limite D.M. 08
Tipo di calcolo: analisi sismica dinamica
Vincoli esterni: Considera sempre vincoli assegnati in modellazione
Schematizzazione piani rigidi: metodo Master-Slave
Modalità di recupero masse secondarie: trasferire all'impalcato più vicino con modifica XY baricentro

Generazione combinazioni
- Lineari: Sì
- Valuta spostamenti e non sollecitazioni: No
- buckling: No

Opzioni di calcolo
- Sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali con una riduzione del 20%
- Calcolo con offset rigidi dai nodi: No
- Uniformare i carichi variabili: No
- Massimizzare i carichi variabili: No
- Minimo carico da considerare: 0.00 <daN/m>
- Recupero carichi zone rigide: taglio e momento flettente
- Modalità di combinazione momento torcente: disaccoppiare le azioni

Opzioni del solutore
- Tipo di elemento bidimensionale: QF46
- Calcolo sforzo nei nodi: No
- Trascura deformabilità a taglio delle aste: No
- Analisi dinamica con metodo di Lanczos: Sì
- Check sequenza di Sturm: Sì
- Soluzione matrice con metodo ver. 5.1: No
- Analisi non lineare con Newton modificato: No
- Usa formulazione secante per buckling: No
- Trascura buckling torsionale: No

Dati struttura
- Zona sismica: zona 2
- Sito di costruzione: prato LON. 11.10220 LAT. 43.87770
  Contenuto tra ID reticolo: 19613 19612 19391 19390

Simbologia

TCC = Tipo di combinazione di carico
      SLU = Stato limite ultimo
      SLU S = Stato limite ultimo (azione sismica)
      SLE R = Stato limite d'esercizio, combinazione rara
      SLE F = Stato limite d'esercizio, combinazione frequente

SLE Q = Stato limite d'esercizio, combinazione quasi permanente
SLD = Stato limite di danno
SLV = Stato limite di salvaguardia della vita
SLC = Stato limite di prevenzione del collasso
SLO = Stato limite di operatività
SLU I = Stato limite di resistenza al fuoco
T_R = Periodo di ritorno <anni>
Ag = Accelerazione orizzontale massima al sito
FO = Valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale
TC* = Periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale <sec>
S_S = Coefficiente di amplificazione stratigrafica
C_C = Coefficiente funzione della categoria del suolo

TCC	T_R	Ag <g>	FO	TC*	S_S	C_C
SLD	50	0.0605	2.55	0.27	1.20	1.43
SLV	475	0.1421	2.43	0.30	1.20	1.40

- Edificio esistente: No
- Tipo di opera: Opera ordinaria
- Vita nominale V_N: 50.00
- Classe d'uso: Classe II
- SL Esercizio: SLO-Pvr No, SLD-Pvr 63.00
- SL Ultimi: SLV-Pvr 10.00, SLC-Pvr No
- Classe di duttilità: Classe B
- Quota di riferimento: 0.00 <m>
- Altezza della struttura: 3.80 <m>
- Numero piani edificio: 1
- Coefficiente θ: 0.00
- Edificio regolare in altezza: Sì
- Edificio regolare in pianta: Sì
- Forze orizzontali convenzionali per stati limite non sismici: 1.00%
- Genera stati limite per verifiche di resistenza al fuoco: No

Dati di piano

Simbologia

Imp. = Numero dell'impalcato
Lx = Dimensione del piano in dir. X
Ly = Dimensione del piano in dir. Y
Ex = Eccentricità in dir. X
Ey = Eccentricità in dir. Y
Ea = Eccentricità complessiva

Imp.	Lx <m>	Ly <m>	Ex <m>	Ey <m>	Ea <m>
1	10.00	10.50	0.50	0.53	0.72

Dati di calcolo
- Categoria del suolo di fondazione: B
- Tipologia edificio: c.a. o prefabbricato a telaio a più piani e più campate

Coeff. C_1: 0.075
Periodo T_1: 0.20413
Coeff. λ SLD: 1.00
Coeff. λ SLV: 1.00
Rapporto di sovraresistenza (α_u/α_1): 1.30
Valore di riferimento del fattore di struttura (q_0): 3.90
Fattore riduttivo (K_w): 1.00
Fattore riduttivo regolarità in altezza (KR): 1.00
Fattore di struttura (q): 2.00

- Categoria topografica: T1 - Superficie pianeggiante, pendii e rilievi isolati con inclinazione media i<=15°
- Coeff. amplificazione topografica S_T: 1.00
- Fattore di struttura per sisma verticale (qv): 1.50
- Modalità di calcolo modi di vibrare: Autovalori
- Numero modi: 3
- Modi da considerare: Tali da movimentare una percentuale di massa pari a 85.00%
- Trascura modi con massa movimentata minore di: No

- Smorzamento spettro: 5.00%

- Angolo di ingresso del sisma: 0.00 <grad>

CONDIZIONI DI CARICO ELEMENTARI:

Simbologia

CCE = Numero della condizione di carico elementare
Comm. = Commento
Tipo CCE = Tipo di CCE per calcolo agli stati limite
Sic. = Contributo alla sicurezza
F = a favore
S = a sfavore
A = ambigua
Var. = Tipo di variabilità
B = di base
I = indipendente
A = ambigua
Dir. = Direzione del vento
Tipo = Tipologia di pressione vento
M = Massimizzata
E = Esterna
I = Interna
Mx = Moltiplicatore della massa in dir. X
My = Moltiplicatore della massa in dir. Y
Mz = Moltiplicatore della massa in dir. Z
Jpx = Moltiplicatore del momento d'inerzia intorno all'asse X
Jpy = Moltiplicatore del momento d'inerzia intorno all'asse Y
Jpz = Moltiplicatore del momento d'inerzia intorno all'asse Z

CCE	Comm.	Tipo CCE	Sic.	Var.	Dir. <grad>	Tipo	Mx	My	Mz	Jpx	Jpy	Jpz
1	Peso+ps	1	S	--	--	--	1.00	1.00	0.00	0.00	0.00	1.00
2	qpn	2	S	--	--	--	1.00	1.00	0.00	0.00	0.00	1.00
3	QACC1	4	S	B	--	--	1.00	1.00	0.00	0.00	0.00	1.00

ELENCO TIPI CCE DEFINITI:

Simbologia

Tipo CCE = Tipo condizione di carico elementare
Comm. = Commento
Tipo = Tipologia
G = Permanente
Qv = Variabile vento
Q = Variabile
I = Da ignorare
A = Azione eccezionale
P = Precompressione
Durata = Durata del carico
N = Non definita
P = Permanente
L = Lunga
M = Media
B = Breve
I = Istantanea
γ min. = Coeff. $\gamma_{min.}$
γ max = Coeff. γ_{max}
ψ_0 = Coeff. ψ_0
ψ_1 = Coeff. ψ_1
ψ_2 = Coeff. ψ_2
$\psi_{0,s}$ = Coeff. ψ_0 sismico (D.M. 96)

Tipo CCE	Comm.	Tipo	Durata	γ min.	γ max	ψ_0	ψ_1	ψ_2	$\psi_{0,s}$
4	D.M. 08 Variabili Categoria B Uffici	Q	N	0.00	1.50	0.70	0.50	0.30	0.00
1	D.M. 08 Permanenti strutturali	G	N	1.00	1.30				

2 D.M. 08 Permanenti non strutturali G N 0.00 1.50

AMBIENTI DI CARICO:

Simbologia

N = Numero
Comm. = Commento
1 = Peso+ps
2 = qpn
3 = QACC1
F = azioni orizzontali convenzionali
SLU = Stato limite ultimo
SLR = Stato limite per combinazioni rare
SLF = Stato limite per combinazioni frequenti
SLQ/D = Stato limite per combinazioni quasi permanenti o di danno
S = Sì
N = No

N	Comm.	1	2	3	F	S	SLU	SLR	SLF	SLQ
1	Calcolo sismico	S	S	S	N	S	S	N	N	N
2	Calcolo statico	S	S	S	S	N	S	S	S	S

ELENCO COMBINAZIONI DI CARICO SIMBOLICHE:

Simbologia

CC = Numero della combinazione delle condizioni di carico elementari
Comm. = Commento
TCC = Tipo di combinazione di carico
SLU = Stato limite ultimo
SLU S = Stato limite ultimo (azione sismica)
SLE R = Stato limite d'esercizio, combinazione rara
SLE F = Stato limite d'esercizio, combinazione frequente
SLE Q = Stato limite d'esercizio, combinazione quasi permanente
SLD = Stato limite di danno
SLV = Stato limite di salvaguardia della vita
SLC = Stato limite di prevenzione del collasso
SLO = Stato limite di operatività
SLU I = Stato limite di resistenza al fuoco

CC	Comm.	TCC	1	2	3	F	S
1	Amb. 1 (Sisma)	SLU S	1	1	ψ_2	-----	1
2	Amb. 2 (SLU)	SLU	γ max	γ max	γ max	1	-----
3	Amb. 2 (SLE R)	SLE R	1	1	1	1	-----
4	Amb. 2 (SLE F)	SLE F	1	1	ψ_1	1	-----
5	Amb. 2 (SLE Q)	SLE Q	1	1	ψ_2	1	-----

Genera le combinazioni con un solo carico di tipo variabile come di base: No

Considera sollecitazioni dinamiche con segno dei modi principali: No

COMBINAZIONI DELLE CCE:

Simbologia

CC = Numero della combinazione delle condizioni di carico elementari
Comm. = Commento
TCC = Tipo di combinazione di carico
SLU = Stato limite ultimo
SLU S = Stato limite ultimo (azione sismica)
SLE R = Stato limite d'esercizio, combinazione rara
SLE F = Stato limite d'esercizio, combinazione frequente
SLE Q = Stato limite d'esercizio, combinazione quasi permanente

SLD = Stato limite di danno
SLV = Stato limite di salvaguardia della vita
SLC = Stato limite di prevenzione del collasso
SLO = Stato limite di operatività
SLU I = Stato limite di resistenza al fuoco
An. = Tipo di analisi
L = Lineare
NL = Non lineare
Bk = buckling
S = Sì
N = No

CC	Comm.	TCC	An.	Bk	1	2	3	F X	F Y	Mt	±S X	±S Y
1	CC 1 - Amb. 1 (SLU S) S Mt+X+0.3Y	SLV	L	N	1.00	1.00	0.30	0.00	0.00	1.00	1.00	0.30
2	CC 2 - Amb. 1 (SLE) S Mt+X+0.3Y	SLD	L	N	1.00	1.00	0.30	0.00	0.00	1.00	1.00	0.30
3	CC 3 - Amb. 1 (SLU S) S Mt+X-0.3Y	SLV	L	N	1.00	1.00	0.30	0.00	0.00	1.00	1.00	-0.30
4	CC 4 - Amb. 1 (SLE) S Mt+X-0.3Y	SLD	L	N	1.00	1.00	0.30	0.00	0.00	1.00	1.00	-0.30
5	CC 5 - Amb. 1 (SLU S) S Mt+0.3X+Y	SLV	L	N	1.00	1.00	0.30	0.00	0.00	1.00	0.30	1.00
6	CC 6 - Amb. 1 (SLE) S Mt+0.3X+Y	SLD	L	N	1.00	1.00	0.30	0.00	0.00	1.00	0.30	1.00
7	CC 7 - Amb. 1 (SLU S) S Mt-0.3X+Y	SLV	L	N	1.00	1.00	0.30	0.00	0.00	1.00	-0.30	1.00
8	CC 8 - Amb. 1 (SLE) S Mt-0.3X+Y	SLD	L	N	1.00	1.00	0.30	0.00	0.00	1.00	-0.30	1.00
9	CC 9 - Amb. 1 (SLU S) S -Mt+X+0.3Y	SLV	L	N	1.00	1.00	0.30	0.00	0.00	-1.00	1.00	0.30
10	CC 10 - Amb. 1 (SLE) S -Mt+X+0.3Y	SLD	L	N	1.00	1.00	0.30	0.00	0.00	-1.00	1.00	0.30
11	CC 11 - Amb. 1 (SLU S) S -Mt+X-0.3Y	SLV	L	N	1.00	1.00	0.30	0.00	0.00	-1.00	1.00	-0.30
12	CC 12 - Amb. 1 (SLE) S -Mt+X-0.3Y	SLD	L	N	1.00	1.00	0.30	0.00	0.00	-1.00	1.00	-0.30
13	CC 13 - Amb. 1 (SLU S) S -Mt+0.3X+Y	SLV	L	N	1.00	1.00	0.30	0.00	0.00	-1.00	0.30	1.00
14	CC 14 - Amb. 1 (SLE) S -Mt+0.3X+Y	SLD	L	N	1.00	1.00	0.30	0.00	0.00	-1.00	0.30	1.00
15	CC 15 - Amb. 1 (SLU S) S -Mt-0.3X+Y	SLV	L	N	1.00	1.00	0.30	0.00	0.00	-1.00	-0.30	1.00
16	CC 16 - Amb. 1 (SLE) S -Mt-0.3X+Y	SLD	L	N	1.00	1.00	0.30	0.00	0.00	-1.00	-0.30	1.00
17	CC 17 - Amb. 2 (SLU) F X	SLU	L	N	1.30	1.50	1.50	1.00	0.00	0.00	0.00	0.00
18	CC 18 - Amb. 2 (SLU) F -X	SLU	L	N	1.30	1.50	1.50	-1.00	0.00	0.00	0.00	0.00
19	CC 19 - Amb. 2 (SLU) F Y	SLU	L	N	1.30	1.50	1.50	0.00	1.00	0.00	0.00	0.00
20	CC 20 - Amb. 2 (SLU) F -Y	SLU	L	N	1.30	1.50	1.50	0.00	-1.00	0.00	0.00	0.00
21	CC 21 - Amb. 2 (SLE R) F X	SLE R	L	N	1.00	1.00	1.00	1.00	0.00	0.00	0.00	0.00
22	CC 22 - Amb. 2 (SLE R) F -X	SLE R	L	N	1.00	1.00	1.00	-1.00	0.00	0.00	0.00	0.00
23	CC 23 - Amb. 2 (SLE R) F Y	SLE R	L	N	1.00	1.00	1.00	0.00	1.00	0.00	0.00	0.00
24	CC 24 - Amb. 2 (SLE R) F -Y	SLE R	L	N	1.00	1.00	1.00	0.00	-1.00	0.00	0.00	0.00
25	CC 25 - Amb. 2 (SLE F) F X	SLE F	L	N	1.00	1.00	0.50	1.00	0.00	0.00	0.00	0.00
26	CC 26 - Amb. 2 (SLE F) F -X	SLE F	L	N	1.00	1.00	0.50	-1.00	0.00	0.00	0.00	0.00
27	CC 27 - Amb. 2 (SLE F) F Y	SLE F	L	N	1.00	1.00	0.50	0.00	1.00	0.00	0.00	0.00
28	CC 28 - Amb. 2 (SLE F) F -Y	SLE F	L	N	1.00	1.00	0.50	0.00	-1.00	0.00	0.00	0.00
29	CC 29 - Amb. 2 (SLE Q) F X	SLE Q	L	N	1.00	1.00	0.30	1.00	0.00	0.00	0.00	0.00
30	CC 30 - Amb. 2 (SLE Q) F -X	SLE Q	L	N	1.00	1.00	0.30	-1.00	0.00	0.00	0.00	0.00
31	CC 31 - Amb. 2 (SLE Q) F Y	SLE Q	L	N	1.00	1.00	0.30	0.00	1.00	0.00	0.00	0.00
32	CC 32 - Amb. 2 (SLE Q) F -Y	SLE Q	L	N	1.00	1.00	0.30	0.00	-1.00	0.00	0.00	0.00

ELENCO BARICENTRI E MASSE IMPALCATI:

Simbologia

Imp. = Numero dell'impalcato
X = Coordinata X
Y = Coordinata Y
Z = Coordinata Z
Mo = Massa orizzontale
Jpz = Momento d'inerzia polare intorno all'asse Z

Imp.	X <m>	Y <m>	Z <m>	Mo <kg>	Jpz <kg*mq>
1	5.00	5.25	3.95	42199.20	777270.00

TOTALI MASSE IMPALCATI:

Mo <kg>	Jpz <kg*mq>
42199.20	777270.00

ELENCO FORZE SISMICHE DI IMPALCATO

Simbologia

Imp. = Numero dell'impalcato
cx = Coeff. c in dir. X
cy = Coeff. c in dir. Y
Mz = Momento intorno all'asse Z

Imp.	cx	cy	Mz <daNm>
1	1.00	1.00	5559.44

TOTALI FORZE SISMICHE:

Mz <daNm>
5559.44

ELENCO FORZE SISMICHE DI IMPALCATO

Imp.	cx	cy	Mz <daNm>
1	1.00	1.00	6217.14

TOTALI FORZE SISMICHE:

Mz <daNm>
6217.14

ELENCO PESI E FORZE FITTIZIE IMPALCATI:

Simbologia

Imp. = Numero dell'impalcato
Peso = Peso
Fx = Forza in dir. X
Fy = Forza in dir. Y

Imp.	Peso <daN>	Fx <daN>	Fy <daN>
1	67122.40	671.22	671.22

ELENCO MODI DI VIBRARE, MASSE PARTECIPANTI E COEFFICIENTI DI PARTECIPAZIONE

Simbologia

Modo = Numero del modo di vibrare
C = * indica che il modo è stato considerato
Per. = Periodo
Diff. = Minima differenza percentuale dagli altri periodi
Φx = Coefficiente di partecipazione in dir. X
Φy = Coefficiente di partecipazione in dir. Y
Φz = Coefficiente di partecipazione in dir. Z
%Mx = Percentuale massa partecipante in dir. X
%My = Percentuale massa partecipante in dir. Y
%Mz = Percentuale massa partecipante in dir. Z
%Jpz = Percentuale momento d'inerzia polare partecipante intorno all'asse Z

Modo	C	Per.	Diff.	Φx	Φy	Φz	%Mx	%My	%Mz	%Jpz

1	*	0.9100	34.53	-0.00	-64.96	0.00	0.000	100.000	0.000	0.000
2	*	0.6764	27.62	63.90	-0.00	0.00	96.767	0.000	0.000	3.233
3	*	0.5300	27.62	11.68	0.00	0.00	3.233	0.000	0.000	96.767
Tot.cons.							100.00	100.00	0.00	100.00

ELENCO COEFFICIENTI DI RISPOSTA

Simbologia

Modo = Numero del modo di vibrare
Sx = Coefficiente di risposta (moltiplicato per 100) in dir. X
Sy = Coefficiente di risposta (moltiplicato per 100) in dir. Y

Stato limite di danno	Modo	Sx	Sy
	1	7.86	7.86
	2	10.57	10.57
	3	13.49	13.49

Stato limite di salvaguardia della vita	Modo	Sx	Sy
	1	9.56	9.56
	2	12.86	12.86
	3	16.41	16.41

Verifica pushover
SPOSTAMENTI RELATIVI MASSIMI ALLO SLD:

Simbologia

N1 = Nodo1
N2 = Nodo2
h = Altezza teorica
δ = Spostamento relativo
δ/h = Rapporto (moltiplicato per 1000) tra lo spostamento relativo e l'altezza
CC = Numero della combinazione delle condizioni di carico elementari

N1	N2	h <m>	δ <cm>	δ/h	CC	N1	N2	h <m>	δ <cm>	δ/h	CC	N1	N2	h <m>	δ <cm>	δ/h	CC	N1	N2	h <m>	δ <cm>	δ/h	CC
1	101	3.95	2.10913	5.340	14	2	102	3.95	1.89695	4.802	6	3	103	3.95	2.22646	5.637	6	4	104	3.95	2.13872	5.414	14
5	105	3.95	1.79323	4.540	8	6	106	3.95	2.12395	5.377	6	7	107	3.95	2.17088	5.496	14	8	108	3.95	1.83138	4.636	8
9	109	3.95	2.10534	5.330	6																		

Min = 4.54
Max = 5.64

Elenco unità geotecniche

1 :
Classificazione: Non classificato

Pesi:
- Peso specifico del terreno naturale: γ = 1800.00 daN/mc
- Peso specifico del terreno saturo: γ_{sat} = 2000.00 daN/mc

Parametri plastici:
- Angolo di attrito efficace: ϕ' = 31.67 grad
  correlata alla stratigrafia 1
  valutata come valore medio risultante dalle seguenti correlazioni:

Correlazione	ϕ' <grad>

Terzaghi e Peck (1948)	31.67

- Coesione efficace: c' = 500.00 daN/mq
- Coesione non drenata: c_u = 10480.00 daN/mq
  correlata alla stratigrafia 1
  valutata come valore medio risultante dalle seguenti correlazioni:

Correlazione	c_u <daN/mq>
Hara et al. (1971)	10480.00

Caratteristiche litostatiche:
- Grado di sovraconsolidazione: OCR = 10.00
  correlata alla stratigrafia 1
  valutata come valore medio risultante dalle seguenti correlazioni:

Correlazione	OCR
SPT Mayne e Kemper (1988)	10.00

- Coeff. di spinta a riposo: κ_0 = 1.59
  calcolato utilizzando le seguenti opzioni:
  -Calcolo di k0 Jaky(1936)
  -Calcolo di α Kulhawy (1989)

Parametri elastici:
- Modulo elastico normale: E = 540000.00 daN/mq
- Modulo elastico tangenziale: G = 245455.00 daN/mq
- Esponente del parametro tensionale: k_j = 0.00
- Coeff. di Poisson: ν = 0.10
- Modulo edometrico: E_{ed} = 552273.00 daN/mq
- Modulo elastico non drenato: E_u = 736364.00 daN/mq
  correlati alla stratigrafia 1
  Tipo di prova SPT, Stroud 1989
  Fattore elastico riduzione modulo secante: 1.00

2 :
Classificazione: Incoerente

Pesi:
- Peso specifico del terreno naturale: γ = 1850.00 daN/mc
- Peso specifico del terreno saturo: γ_{sat} = 2000.00 daN/mc

Parametri plastici:
- Angolo di attrito efficace: ϕ' = 31.35 grad
  correlata alla stratigrafia 1
  valutata come valore medio risultante dalle seguenti correlazioni:

Correlazione	ϕ' <grad>
Terzaghi e Peck (1948)	31.35

- Coesione efficace: c' = 500.00 daN/mq

Caratteristiche litostatiche:
- Grado di sovraconsolidazione: OCR = 7.71
  correlata alla stratigrafia 1
  valutata come valore medio risultante dalle seguenti correlazioni:

Correlazione	OCR
SPT Mayne e Kemper (1988)	7.71

- Coeff. di spinta a riposo: κ_0 = 1.39
  calcolato utilizzando le seguenti opzioni:
  -Calcolo di k0 Jaky(1936)
  -Calcolo di α Kulhawy (1989)

Parametri elastici:
- Modulo elastico normale: E = 585000.00 daN/mq
- Modulo elastico tangenziale: G = 265909.00 daN/mq
- Esponente del parametro tensionale: k_j = 0.00
- Coeff. di Poisson: ν = 0.10
- Modulo edometrico: E_{ed} = 598295.00 daN/mq

- Modulo elastico non drenato: E_u = 0.00 daN/mq

Elenco colonne stratigrafiche

Prove in sito

Report grafico complessivo
Le verifiche degli elementi di fondazione sono state effettuate utilizzando l'approccio 2.

Coefficienti parziali per le azioni, per verifiche in condizioni statiche:
Permanenti strutturali, sicurezza a favore γ_A = 1.00;
Permanenti strutturali, sicurezza a sfavore γ_A = 1.30;
Permanenti non strutturali, sicurezza a favore γ_A = 0.00;
Permanenti non strutturali, sicurezza a sfavore γ_A = 1.50;
Variabili, sicurezza a favore γ_A = 0.00;
Variabili, sicurezza a sfavore γ_A = 1.50.

I coefficienti parziali per le azioni sono posti pari all'unità per le verifiche in condizioni sismiche.

Tali coefficienti sono comunque desumibili dalla tabella delle combinazioni delle CCE (Parametri di calcolo).

Coefficienti parziali per i parametri geotecnici:
Tangente dell'angolo di attrito γ_M = 1.00;
Coesione efficace γ_M = 1.00;
Coesione non drenata γ_M = 1.00;

Coefficienti parziali per la resistenza delle fondazioni superficiali:
Capacità portante γ_R = 2.30;
Scorrimento γ_R = 1.10;

Coefficienti parziali per la resistenza delle fondazioni profonde:
Per pali infissi:
Resistenza alla base γ_R,b = 1.15;
Resistenza laterale in compressione γ_R,s = 1.15;
Resistenza laterale in trazione γ_R,t = 1.25;
Per pali trivellati:
Resistenza alla base γ_R,b = 1.35;
Resistenza laterale in compressione γ_R,s = 1.15;
Resistenza laterale in trazione γ_R,t = 1.25;
Per pali ad elica continua:
Resistenza alla base γ_R,b = 1.30;
Resistenza laterale in compressione γ_R,s = 1.15;
Resistenza laterale in trazione γ_R,t = 1.25;

Fattore di correlazione per la determinazione della resistenza caratteristica desumibile dai criteri di progetto.
Fondazioni superficiali

Simbologia

B = Base della fondazione
L = Lunghezza della fondazione (L>B)
D = Profondità del piano di posa della fondazione
β = Inclinazione del piano di campagna
η = Inclinazione del piano di posa della fondazione
γ_r = Peso specifico rappresentativo del terreno di fondazione
$\sigma_{v0,f}$ = Pressione verticale alla profondità del piano di posa della fondazione
φ'_r = Angolo di attrito rappresentativo del terreno di fondazione
c'_r = Coesione efficace rappresentativa del terreno di fondazione
N_q = Coefficiente di capacità portante relativo al sovraccarico laterale
N_c = Coefficiente di capacità portante relativo alla coesione del terreno di fondazione
N_g = Coefficiente di capacità portante relativo al peso del terreno di fondazione
s_c = Fattore di forma relativo alla coesione
s_g = Fattore di forma relativo al peso del terreno
CC = Numero della combinazione delle condizioni di carico elementari
N = Sforzo normale

Mx = Momento intorno all'asse X
My = Momento intorno all'asse Y
B' = Base della fondazione reagente
L' = Lunghezza della fondazione reagente
q_{lim} = Pressione limite
R_d = Resistenza di progetto (Carico limite)
Sic. = Sicurezza a rottura

Verifiche capacità portante
Verifiche di capacità portante per rottura generale in condizioni statiche
Metodo utilizzato: Terzaghi

Plinto n. 1

B=0.90 <m> L=0.90 <m> D=0.20 <m> β=0.00 <grad> η=0.00 <grad> γ_r=1818.99 <daN/mc>
$\sigma_{v0,f}$=360.00 <daN/mq>

Verifiche in condizioni drenate

φ'_r=31.55 <grad> c'_r=500.00 <daN/mq>
N_q=27.00 N_c=42.35 N_g=24.87 s_c=1.30 s_g=0.80

CC	N <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	q_{lim} <daN/mq>	R_d <daN>	Sic.
17	7871.35	-213.32	98.73	0.85	0.87	52552.00	16908.00	2.15
18	8058.79	-212.22	125.36	0.85	0.87	52579.70	16830.90	2.09
19	7903.95	-200.95	112.11	0.85	0.87	52612.60	16930.90	2.14
20	8026.19	-224.59	111.98	0.84	0.87	52520.00	16808.20	2.09

Verifiche di capacità portante per rottura generale in condizioni statiche
Metodo utilizzato: Terzaghi

Plinto n. 4

B=0.90 <m> L=0.90 <m> D=0.20 <m> β=0.00 <grad> η=0.00 <grad> γ_r=1818.99 <daN/mc>
$\sigma_{v0,f}$=360.00 <daN/mq>

Verifiche in condizioni drenate

φ'_r=31.55 <grad> c'_r=500.00 <daN/mq>
N_q=27.00 N_c=42.35 N_g=24.87 s_c=1.30 s_g=0.80

CC	N <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	q_{lim} <daN/mq>	R_d <daN>	Sic.
17	12930.50	156.97	205.53	0.87	0.88	52957.50	17506.20	1.35
18	13099.30	158.70	229.53	0.86	0.88	52898.60	17422.10	1.33
19	12958.20	176.39	217.72	0.87	0.87	52924.70	17400.00	1.34
20	13071.60	139.28	217.34	0.87	0.88	52931.10	17527.10	1.34

Verifiche di capacità portante per rottura generale in condizioni statiche
Metodo utilizzato: Terzaghi

Plinto n. 2

B=1.20 <m> L=1.20 <m> D=0.20 <m> β=0.00 <grad> η=0.00 <grad> γ_r=1826.75 <daN/mc>
$\sigma_{v0,f}$=360.00 <daN/mq>

Verifiche in condizioni drenate

φ'_r=31.50 <grad> c'_r=500.00 <daN/mq>
N_q=26.84 N_c=42.17 N_g=24.67 s_c=1.30 s_g=0.80

CC	N <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	q_{lim} <daN/mq>	R_d <daN>	Sic.
17	15489.60	-422.77	-22.28	1.15	1.20	57719.60	34410.90	2.22
18	15489.60	-422.77	22.28	1.15	1.20	57719.60	34410.90	2.22
19	15419.40	-409.41	-0.00	1.15	1.20	57746.30	34554.30	2.24
20	15559.80	-436.12	-0.00	1.14	1.20	57693.10	34433.50	2.21

Verifiche di capacità portante per rottura generale in condizioni statiche
Metodo utilizzato: Terzaghi

Plinto n. 3

B=0.90 <m> L=0.90 <m> D=0.20 <m> β=0.00 <grad> η=0.00 <grad> γ_r=1818.99 <daN/mc>
$\sigma_{v0,f}$=360.00 <daN/mq>

Verifiche in condizioni drenate

φ'_r=31.55 <grad> c'_r=500.00 <daN/mq>
N_q=27.00 N_c=42.35 N_g=24.87 s_c=1.30 s_g=0.80

CC	N <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	q_{lim} <daN/mq>	R_d <daN>	Sic.
17	8058.79	-212.22	-125.36	0.85	0.87	52579.70	16830.90	2.09
18	7871.35	-213.32	-98.73	0.85	0.87	52552.00	16908.00	2.15
19	7903.95	-200.95	-112.11	0.85	0.87	52612.60	16930.90	2.14
20	8026.19	-224.59	-111.98	0.84	0.87	52520.00	16808.20	2.09

Verifiche di capacità portante per rottura generale in condizioni statiche
Metodo utilizzato: Terzaghi

Plinto n. 5

B=1.20 <m> L=1.20 <m> D=0.20 <m> β=0.00 <grad> η=0.00 <grad> γ_r=1826.75 <daN/mc>
$\sigma_{v0,f}$=360.00 <daN/mq>

Verifiche in condizioni drenate

φ'_r=31.50 <grad> c'_r=500.00 <daN/mq>
N_q=26.84 N_c=42.17 N_g=24.67 s_c=1.30 s_g=0.80

CC	N <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	q_{lim} <daN/mq>	R_d <daN>	Sic.
17	26005.70	289.45	-20.09	1.18	1.20	58302.20	35779.00	1.38
18	26005.70	289.45	20.09	1.18	1.20	58302.20	35779.00	1.38
19	25955.70	308.39	-0.00	1.18	1.20	58275.20	35762.80	1.38
20	26055.70	270.52	-0.00	1.18	1.20	58329.20	35887.20	1.38

Verifiche di capacità portante per rottura generale in condizioni statiche
Metodo utilizzato: Terzaghi

Plinto n. 6

B=0.90 <m> L=0.90 <m> D=0.20 <m> β=0.00 <grad> η=0.00 <grad> γ_r=1818.99 <daN/mc>
$\sigma_{v0,f}$=360.00 <daN/mq>

Verifiche in condizioni drenate

φ'_r=31.55 <grad> c'_r=500.00 <daN/mq>
N_q=27.00 N_c=42.35 N_g=24.87 s_c=1.30 s_g=0.80

CC	N <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	q_{lim} <daN/mq>	R_d <daN>	Sic.
17	13099.30	158.70	-229.53	0.86	0.88	52898.60	17422.10	1.33
18	12930.50	156.97	-205.53	0.87	0.88	52957.50	17506.20	1.35
19	12958.20	176.39	-217.72	0.87	0.87	52924.70	17400.00	1.34
20	13071.60	139.28	-217.34	0.87	0.88	52931.10	17527.10	1.34

Verifiche di capacità portante per rottura generale in condizioni statiche
Metodo utilizzato: Terzaghi

Plinto n. 9

B=0.90 <m> L=0.90 <m> D=0.20 <m> β=0.00 <grad> η=0.00 <grad> γ_r=1818.99 <daN/mc>
$\sigma_{v0,f}$=360.00 <daN/mq>

Verifiche in condizioni drenate

φ'_r=31.55 <grad> c'_r=500.00 <daN/mq>
N_q=27.00 N_c=42.35 N_g=24.87 s_c=1.30 s_g=0.80

CC	N	Mx	My	B'	L'	q_{lim}	R_d	Sic.

	<daN>	<daNm>	<daNm>	<m>	<m>	<daN/mq>	<daN>	
17	5036.76	74.73	-117.79	0.85	0.87	52686.40	17010.50	3.38
18	4862.68	73.45	-95.40	0.86	0.87	52822.80	17194.60	3.54
19	5069.29	87.83	-106.56	0.86	0.87	52772.00	17034.60	3.36
20	4830.15	60.34	-106.63	0.86	0.88	52733.80	17170.10	3.55

Verifiche di capacità portante per rottura generale in condizioni statiche
Metodo utilizzato: Terzaghi

Plinto n. 8

B=0.90 <m> L=0.90 <m> D=0.20 <m> β=0.00 <grad> η=0.00 <grad> γ_r=1818.99 <daN/mc>
$\sigma_{v0,f}$=360.00 <daN/mq>

Verifiche in condizioni drenate

φ'_r=31.55 <grad> c'_r=500.00 <daN/mq>
N_q=27.00 N_c=42.35 N_g=24.87 s_c=1.30 s_g=0.80

CC	N	Mx	My	B'	L'	q_{lim}	R_d	Sic.
	<daN>	<daNm>	<daNm>	<m>	<m>	<daN/mq>	<daN>	
17	8020.91	95.01	-18.86	0.88	0.90	53104.10	18114.50	2.26
18	8020.91	95.01	18.86	0.88	0.90	53104.10	18114.50	2.26
19	8137.60	108.72	-0.00	0.87	0.90	53049.30	18127.90	2.23
20	7904.23	81.30	-0.00	0.88	0.90	53160.60	18293.80	2.31

Verifiche di capacità portante per rottura generale in condizioni statiche
Metodo utilizzato: Terzaghi

Plinto n. 7

B=0.90 <m> L=0.90 <m> D=0.20 <m> β=0.00 <grad> η=0.00 <grad> γ_r=1818.99 <daN/mc>
$\sigma_{v0,f}$=360.00 <daN/mq>

Verifiche in condizioni drenate

φ'_r=31.55 <grad> c'_r=500.00 <daN/mq>
N_q=27.00 N_c=42.35 N_g=24.87 s_c=1.30 s_g=0.80

CC	N	Mx	My	B'	L'	q_{lim}	R_d	Sic.
	<daN>	<daNm>	<daNm>	<m>	<m>	<daN/mq>	<daN>	
17	4862.68	73.45	95.40	0.86	0.87	52822.80	17194.60	3.54
18	5036.76	74.73	117.79	0.85	0.87	52686.40	17010.50	3.38
19	5069.29	87.83	106.56	0.86	0.87	52772.00	17034.60	3.36
20	4830.15	60.34	106.63	0.86	0.88	52733.80	17170.10	3.55

Cedimenti
Metodo utilizzato: Bowles

Simbologia

B = Base della fondazione
L = Lunghezza della fondazione (L>B)
D = Profondità del piano di posa della fondazione
H = Spessore del terreno responsabile del cedimento
E_r = Modulo elastico rappresentativo del terreno di fondazione
ν_r = Coefficiente di Poisson rappresentativo del terreno di fondazione
I_s = Coefficiente di influenza
I_f = Coefficiente di profondità
kw = Costante di sottofondo
CC = Numero della combinazione delle condizioni di carico elementari
N = Sforzo normale
q_{es} = Pressione di esercizio
Ced = Cedimento calcolato

Plinto n. 1
B=0.90 <m> L=0.90 <m> D=0.20 <m> H=4.50 <m> E_r=582000.00 <daN/mq> ν_r=0.10
I_s=0.51 I_f=0.78 kw=819116.00 <daN/mc>

CC	N	q_{es}	Ced
	<daN>	<daN/mq>	<cm>

1	5020.93	6198.68	0.76
2	4622.79	5707.14	0.70
3	4783.17	5905.15	0.72
4	4492.50	5546.30	0.68
5	4690.08	5790.22	0.71
6	4441.50	5483.33	0.67
7	4168.74	5146.59	0.63
8	4155.82	5130.65	0.63
9	5260.53	6494.48	0.79
10	4765.62	5883.48	0.72
11	5022.77	6200.95	0.76
12	4635.34	5722.64	0.70
13	4929.68	6086.03	0.74
14	4584.33	5659.67	0.69
15	4408.34	5442.39	0.66
16	4298.66	5306.99	0.65
17	7871.35	9717.71	1.19
18	8058.79	9949.13	1.21
19	7903.95	9757.97	1.19
20	8026.19	9908.87	1.21
21	5645.73	6970.03	0.85
22	5833.17	7201.44	0.88
23	5678.33	7010.29	0.86
24	5800.56	7161.19	0.87
25	4242.84	5238.07	0.64
26	4430.28	5469.48	0.67
27	4275.44	5278.32	0.64
28	4397.67	5429.23	0.66
29	3681.68	4545.29	0.55
30	3869.12	4776.70	0.58
31	3714.29	4585.54	0.56
32	3836.52	4736.44	0.58

Plinto n. 4

B=0.90 <m> L=0.90 <m> D=0.20 <m> H=4.50 <m> E_r=582000.00 <daN/mq> ν_r=0.10
I_s=0.51 I_f=0.78 kw=819116.00 <daN/mc>

CC	N <daN>	q_{es} <daN/mq>	Ced <cm>
1	7374.16	9103.90	1.11
2	6987.80	8626.91	1.05
3	7153.55	8831.55	1.08
4	6866.92	8477.68	1.03
5	7163.59	8843.94	1.08
6	6872.42	8484.47	1.04
7	6762.50	8348.77	1.02
8	6652.64	8213.14	1.00
9	7204.25	8894.13	1.09
10	6886.51	8501.86	1.04
11	6983.64	8621.78	1.05
12	6765.63	8352.63	1.02
13	6993.68	8634.18	1.05
14	6771.13	8359.42	1.02
15	6592.59	8139.00	0.99
16	6551.35	8088.09	0.99
17	12930.50	15963.60	1.95
18	13099.30	16172.00	1.97
19	12958.20	15997.80	1.95
20	13071.60	16137.80	1.97
21	9197.02	11354.30	1.39
22	9365.76	11562.70	1.41
23	9224.68	11388.50	1.39
24	9338.09	11528.50	1.41
25	6795.00	8388.88	1.02
26	6963.74	8597.21	1.05
27	6822.66	8423.04	1.03
28	6936.08	8563.06	1.05
29	5834.19	7202.70	0.88
30	6002.94	7411.03	0.90
31	5861.86	7236.86	0.88
32	5975.27	7376.88	0.90

Plinto n. 2

B=1.20 <m> L=1.20 <m> D=0.20 <m> H=6.00 <m> E_r=583000.00 <daN/mq> ν_r=0.10
I_s=0.51 I_f=0.82 kw=586565.00 <daN/mc>

CC	N <daN>	q_{es} <daN/mq>	Ced <cm>
1	8035.38	5580.12	0.95
2	7973.64	5537.25	0.94
3	7762.24	5390.45	0.92
4	7823.98	5433.32	0.93
5	8354.04	5801.42	0.99
6	8148.25	5658.51	0.96
7	8354.04	5801.42	0.99
8	8148.25	5658.51	0.96
9	8035.38	5580.12	0.95
10	7973.64	5537.25	0.94
11	7762.24	5390.45	0.92
12	7823.98	5433.32	0.93
13	8354.04	5801.42	0.99
14	8148.25	5658.51	0.96
15	8354.04	5801.42	0.99
16	8148.25	5658.51	0.96
17	15489.60	10756.60	1.83
18	15489.60	10756.60	1.83
19	15419.40	10707.90	1.83
20	15559.80	10805.40	1.84
21	11117.20	7720.26	1.32
22	11117.20	7720.26	1.32
23	11047.00	7671.50	1.31
24	11187.40	7769.02	1.32
25	8305.43	5767.66	0.98
26	8305.43	5767.66	0.98
27	8235.22	5718.90	0.97
28	8375.64	5816.42	0.99
29	7180.74	4986.62	0.85
30	7180.74	4986.62	0.85
31	7110.53	4937.87	0.84
32	7250.95	5035.38	0.86

Plinto n. 3

B=0.90 <m> L=0.90 <m> D=0.20 <m> H=4.50 <m> E_r=582000.00 <daN/mq> ν_r=0.10
I_s=0.51 I_f=0.78 kw=819116.00 <daN/mc>

CC	N <daN>	q_{es} <daN/mq>	Ced <cm>
1	5260.53	6494.48	0.79
2	4765.62	5883.49	0.72
3	5022.77	6200.95	0.76
4	4635.34	5722.64	0.70
5	4929.68	6086.03	0.74
6	4584.33	5659.67	0.69
7	4408.34	5442.39	0.66
8	4298.66	5306.99	0.65
9	5020.93	6198.68	0.76
10	4622.79	5707.14	0.70
11	4783.17	5905.15	0.72
12	4492.51	5546.30	0.68
13	4690.08	5790.22	0.71
14	4441.50	5483.33	0.67
15	4168.74	5146.59	0.63
16	4155.82	5130.65	0.63
17	8058.79	9949.13	1.21
18	7871.35	9717.71	1.19
19	7903.95	9757.97	1.19
20	8026.19	9908.87	1.21
21	5833.17	7201.44	0.88
22	5645.73	6970.03	0.85
23	5678.33	7010.29	0.86
24	5800.56	7161.19	0.87
25	4430.28	5469.48	0.67
26	4242.84	5238.07	0.64
27	4275.44	5278.32	0.64
28	4397.67	5429.23	0.66

29	3869.12	4776.70	0.58
30	3681.68	4545.29	0.55
31	3714.29	4585.54	0.56
32	3836.52	4736.44	0.58

Plinto n. 5

B=1.20 <m> L=1.20 <m> D=0.20 <m> H=6.00 <m> E_r=583000.00 <daN/mq> ν_r=0.10
I_s=0.51 I_f=0.82 kw=586565.00 <daN/mc>

CC	N <daN>	q_{es} <daN/mq>	Ced <cm>
1	12877.30	8942.55	1.52
2	12833.30	8912.03	1.52
3	12682.80	8807.53	1.50
4	12726.80	8838.05	1.51
5	13104.10	9100.07	1.55
6	12957.60	8998.35	1.53
7	13104.10	9100.07	1.55
8	12957.60	8998.35	1.53
9	12877.30	8942.55	1.52
10	12833.30	8912.03	1.52
11	12682.80	8807.53	1.50
12	12726.80	8838.05	1.51
13	13104.10	9100.07	1.55
14	12957.60	8998.35	1.53
15	13104.10	9100.07	1.55
16	12957.60	8998.35	1.53
17	26005.70	18059.50	3.08
18	26005.70	18059.50	3.08
19	25955.70	18024.80	3.07
20	26055.70	18094.20	3.08
21	18488.10	12839.00	2.19
22	18488.10	12839.00	2.19
23	18438.20	12804.30	2.18
24	18538.10	12873.70	2.19
25	13581.10	9431.29	1.61
26	13581.10	9431.29	1.61
27	13531.10	9396.59	1.60
28	13631.00	9466.00	1.61
29	11618.20	8068.22	1.38
30	11618.20	8068.22	1.38
31	11568.30	8033.51	1.37
32	11668.20	8102.93	1.38

Plinto n. 6

B=0.90 <m> L=0.90 <m> D=0.20 <m> H=4.50 <m> E_r=582000.00 <daN/mq> ν_r=0.10
I_s=0.51 I_f=0.78 kw=819116.00 <daN/mc>

CC	N <daN>	q_{es} <daN/mq>	Ced <cm>
1	7204.25	8894.13	1.09
2	6886.51	8501.86	1.04
3	6983.64	8621.78	1.05
4	6765.63	8352.63	1.02
5	6993.68	8634.18	1.05
6	6771.13	8359.42	1.02
7	6592.59	8139.00	0.99
8	6551.35	8088.09	0.99
9	7374.16	9103.90	1.11
10	6987.80	8626.91	1.05
11	7153.55	8831.55	1.08
12	6866.92	8477.68	1.03
13	7163.59	8843.94	1.08
14	6872.42	8484.47	1.04
15	6762.50	8348.77	1.02
16	6652.64	8213.14	1.00
17	13099.30	16172.00	1.97
18	12930.50	15963.60	1.95
19	12958.20	15997.80	1.95
20	13071.60	16137.80	1.97
21	9365.76	11562.70	1.41
22	9197.02	11354.30	1.39
23	9224.68	11388.50	1.39

24	9338.10	11528.50	1.41
25	6963.74	8597.21	1.05
26	6795.00	8388.89	1.02
27	6822.66	8423.04	1.03
28	6936.08	8563.06	1.05
29	6002.94	7411.03	0.90
30	5834.19	7202.70	0.88
31	5861.86	7236.86	0.88
32	5975.27	7376.88	0.90

Plinto n. 9

B=0.90 <m> L=0.90 <m> D=0.20 <m> H=4.50 <m> E_r=582000.00 <daN/mq> ν_r=0.10
I_s=0.51 I_f=0.78 kw=819116.00 <daN/mc>

CC	N <daN>	q_{es} <daN/mq>	Ced <cm>
1	3646.90	4502.35	0.55
2	3231.77	3989.84	0.49
3	3181.73	3928.06	0.48
4	2976.88	3675.16	0.45
5	3687.79	4552.82	0.56
6	3254.17	4017.50	0.49
7	3257.66	4021.80	0.49
8	3018.48	3726.52	0.45
9	3716.59	4588.39	0.56
10	3273.32	4041.13	0.49
11	3251.42	4014.10	0.49
12	3018.43	3726.45	0.45
13	3757.48	4638.86	0.57
14	3295.72	4068.79	0.50
15	3327.35	4107.84	0.50
16	3060.03	3777.81	0.46
17	5036.76	6218.22	0.76
18	4862.68	6003.31	0.73
19	5069.29	6258.38	0.76
20	4830.15	5963.14	0.73
21	3709.21	4579.28	0.56
22	3535.14	4364.36	0.53
23	3741.75	4619.44	0.56
24	3502.60	4324.20	0.53
25	2896.15	3575.50	0.44
26	2722.08	3360.59	0.41
27	2928.69	3615.66	0.44
28	2689.54	3320.42	0.41
29	2570.93	3173.99	0.39
30	2396.85	2959.08	0.36
31	2603.46	3214.15	0.39
32	2364.32	2918.91	0.36

Plinto n. 8

B=0.90 <m> L=0.90 <m> D=0.20 <m> H=4.50 <m> E_r=582000.00 <daN/mq> ν_r=0.10
I_s=0.51 I_f=0.78 kw=819116.00 <daN/mc>

CC	N <daN>	q_{es} <daN/mq>	Ced <cm>
1	4393.84	5424.50	0.66
2	4291.24	5297.83	0.65
3	3939.90	4864.07	0.59
4	4042.50	4990.74	0.61
5	4923.45	6078.33	0.74
6	4581.44	5656.10	0.69
7	4923.45	6078.33	0.74
8	4581.44	5656.10	0.69
9	4393.84	5424.50	0.66
10	4291.24	5297.83	0.65
11	3939.90	4864.07	0.59
12	4042.50	4990.74	0.61
13	4923.45	6078.33	0.74
14	4581.44	5656.10	0.69
15	4923.45	6078.33	0.74
16	4581.44	5656.10	0.69
17	8020.91	9902.36	1.21
18	8020.91	9902.36	1.21

19	8137.60	10046.40	1.23
20	7904.23	9758.30	1.19
21	5776.44	7131.41	0.87
22	5776.44	7131.41	0.87
23	5893.13	7275.47	0.89
24	5659.76	6987.35	0.85
25	4356.17	5377.99	0.66
26	4356.17	5377.99	0.66
27	4472.86	5522.05	0.67
28	4239.48	5233.93	0.64
29	3788.06	4676.62	0.57
30	3788.06	4676.62	0.57
31	3904.75	4820.68	0.59
32	3671.38	4532.56	0.55

Plinto n. 7

B=0.90 <m> L=0.90 <m> D=0.20 <m> H=4.50 <m> E_r=582000.00 <daN/mq> ν_r=0.10
I_s=0.51 I_f=0.78 kw=819116.00 <daN/mc>

CC	N <daN>	q_{es} <daN/mq>	Ced <cm>
1	3716.59	4588.39	0.56
2	3273.32	4041.13	0.49
3	3251.42	4014.10	0.49
4	3018.43	3726.45	0.45
5	3757.48	4638.86	0.57
6	3295.72	4068.79	0.50
7	3327.35	4107.84	0.50
8	3060.03	3777.81	0.46
9	3646.90	4502.35	0.55
10	3231.77	3989.84	0.49
11	3181.73	3928.06	0.48
12	2976.88	3675.16	0.45
13	3687.79	4552.82	0.56
14	3254.17	4017.50	0.49
15	3257.66	4021.80	0.49
16	3018.48	3726.52	0.45
17	4862.68	6003.31	0.73
18	5036.76	6218.22	0.76
19	5069.29	6258.38	0.76
20	4830.15	5963.14	0.73
21	3535.14	4364.36	0.53
22	3709.21	4579.27	0.56
23	3741.75	4619.44	0.56
24	3502.60	4324.20	0.53
25	2722.08	3360.59	0.41
26	2896.15	3575.50	0.44
27	2928.69	3615.66	0.44
28	2689.54	3320.42	0.41
29	2396.85	2959.08	0.36
30	2570.93	3173.99	0.39
31	2603.46	3214.15	0.39
32	2364.32	2918.91	0.36

Criteri di analisi geotecnica e progetto delle fondazioni

Fondazioni superficiali

Generali

Generali

Condizioni di calcolo per terreni coesivi — Sia drenate che non drenate

Calcolo di a' dal rapporto con c'

1

Calcolo di a_u dal rapporto con c_u

1

Calcolo di σ'dal rapporto con ϕ'

1

Considera l'angolo di attrito in deformazione piana per fondazioni nastriformi

No

Calcolo dei parametri rappresentativi per terreni stratificati

Media pesata
-Calcola i valori medi dell'angolo di attrito secondo la sua tangente
No
Capacità portante in condizioni statiche
Calcolo della capacità portante per rottura generale
Terzaghi (1943)
-Combinazione dei fattori di forma e di inclinazione del carico Considera solo i fattori di forma
-Considera il fattore di riduzione per platee
No
-Considera gli effetti dell'eccentricità del carico con un unico fattore riduttivo
No
Considera eccentricità e inclinazione dei carichi attraverso domini di interazione
No
-Parametro correttivo del momento
0
-Parametro correttivo del carico orizzontale
0
Calcolo della capacità portante per rottura locale
Si

Terzaghi (1943)
Calcolo della capacità portante per rottura per punzonamento
No
Calcolo della capacità portante per scorrimento
No
-Percentuale di carico orizzontale assorbito dai cordoli <%>
0
-Percentuale di spinta passiva mobilitata <%>
0
Calcolo della capacità portante per sollevamento
No
Capacità portante in condizioni sismiche
Calcolo della capacità portante per rottura generale
No
Riduzione dell'angolo d'attrito per terreni incoerenti ben addensati
No
Calcolo della capacità portante per scorrimento
No
-Percentuale di carico orizzontale assorbito dai cordoli <%>
0
-Percentuale di spinta passiva mobilitata <%>
0
Cedimenti
Cedimenti
Bowles
-Spessore del terreno responsabile del cedimento
 -Dal rapporto con le dimensioni della fondazione pari a
5.0
Considera pressioni di esercizio al netto delle tensioni litostatiche
No
Calcola costante di sottofondo per pressioni di esercizio
No
Limita costante di sottofondo ad un valore
No

Fondazioni profonde

Generali

Generali
Calcolo capacità portante per carichi verticali Secondo formule statiche
Considera capacità portante
Entrambe
Condizioni di calcolo per terreni coesivi Sia drenate che non drenate
Calcolo della profondità critica
No
Effettua calcolo elasto-plastico per cedimenti
Si
Effettua calcolo elasto-plastico per spostamenti orizzontali

Si
Rapporto di elasticità trazione/compressione pari a
1
Fattori di correlazione
1.7
Considera fattori di correlazione anche per carichi orizzontali
No
Considera peso del palo
No
Attrito laterale limite da prove in sito
Correlato con prove CPT
No
Correlato con prove SPT
No
Fattore di riduzione attrito laterale per pali trivellati
No
Pressione limite alla base da prove in sito
Correlata con prove CPT
No
Correlata con prove SPT
No
Fattore di riduzione pressione limite alla base per pali trivellati
No
Spostamenti orizzontali
Spostamenti orizzontali Risposta elastica in funzione della stratigrafia
Specifici
1 2 3 4 5 6 7 8 9 10

Attrito laterale limite
Calcolo dell'attrito laterale limite
Si Si Si Si Si Si Si Si Si Si
-Condizioni non drenate
 -Calcolo di α
 -Pari a
 -A.G.I. (1984)
x x x x x x x x x x
 -A.P.I. (1984)
 -Viggiani (1999)
 -Olson e Dennis (1982)
 -Stas e Kulhavy (1984)
 -Skempton (1986)
 -Reese e O'Neill (1989)
-Metodo di Bustamente e Doix (1985) per micropali
No No No No No No No No No No
 -Iniezioni ripetute
x x x x x x x x x x
 -Unica iniezione
  -Condizioni drenate
-Calcolo di β
 -Pari a
0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3
 -Reese e O'Neill (1989)
 -Calcolato
  -Calcolo di k
   -Pari a
   -Dal rapporto con k_0 pari a
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
   -Fleming (1985)
  -Calcolo di δ
-Pari a <grad>
   -Dal rapporto con ϕ' pari a
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 -Calcolo di a' dal rapporto con c'
1 1 1 1 1 1 1 1 1 1
Calcolo dell'attrito laterale limite per trazione
-Considera i risultati del calcolo per l'attrito laterale limite percompressione con un fattore di riduzione pari a 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7
-Sowa (1970)
No No No No No No No No No No
-Bowles (1991)

No No No No No No No No No No
Considera l'effetto dell'attrito negativo
No No No No No No No No No No
-Coefficiente di Lambe
Pressione limite alla base
Calcolo della pressione limite alla base del palo
Si Si Si Si Si Si Si Si Si Si
-Terzaghi (1943)
x x x x x x x x x x
-Meyerhof (1963)
-Hansen (1970)
-Vesic (1975)
-Berezantzev (1961)
-Berezantzev (1965)
-Stagg e Zienkiewicz (1968)
-Relazione generale, coefficienti di capacità portante
-In condizioni drenate
-N_q
-N_c
-In condizioni non drenate
-N_c
-Fattore di riduzione per terreni coesivi sovraconsolidati
No No No No No No No No No No
Cedimenti
Risposta elastica laterale
-Calcolata dalla rigidezza dello strato
x x x x x x x x x x
-Coefficiente di influenza
4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0
-Pari a <daN/mq>
Risposta elastica alla base
-Calcolata dalla rigidezza dello strato
x x x x x x x x x x
-Pari a <daN/mq>
Spostamenti orizzontali
Risposta elastica
-Vesic (1961)
-Broms (1964)
-Glick (1948)
-Chen (1978)
-Pari a <daN/mq>
-Dal modulo elastico
x x x x x x x x x x
-Coefficiente effetto tridimensionale
2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0
Resistenza limite
-Calcolata dai parametri plastici
x x x x x x x x x x
-Coefficiente effetto tridimensionale resistenza per attrito
3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0
-Coefficiente effetto tridimensionale resistenza per coesione
4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0
-Pari a <daN/mq>

Caratterizzazione

Specifici	1	2	3	4	5	6	7	8	9	10
Informazioni preliminari										
Coefficiente di uniformità	No	No	No	No	No	No	No	No	No	No
-Pari a	0	0	0	0	0	0	0	0	0	0
Definizione della composizione granulometrica, per terreni incoerenti	No	No	No	No	No	No	No	No	No	No
-Sabbia fine uniforme	x	x	x	x	x	x	x	x	x	x
-Sabbia fine ben gradata - sabbia media uniforme										
-Sabbia media ben gradata - sabbia grossa uniforme										

-Sabbia e ghiaia - ghiaia media
Definizione indici compressibilità edometrica, per terreni coesivi No No No No No No No No
No No
-Indice di compressione (Cc) 0 0 0 0 0 0 0 0
0 0
-Indice di ricompressione (Cr) 0 0 0 0 0 0 0 0
0 0
-Considera incremento preconsolidazione costante No No No No No No No No
No No
-Pari a 0 0 0 0 0 0 0 0
0 0
Correggi NSPT se la misura è sottofalda No No No No No No No No
No No
Densità relativa
Correlata con prove SPT
-Terzaghi e Peck (1948) Si Si Si Si Si Si Si Si
Si Si
-Gibbs e Holtz (1957) No No No No No No No No
No No
-Meyerhof (1957) No No No No No No No No
No No
-Schultze e Menzenbach (1961) No No No No No No No No
No No
-Bazaara (1967) No No No No No No No No
No No
-Marcuson e Bieganousky (1977) No No No No No No No No
No No
-Skempton (1986) No No No No No No No No
No No
Correlata con prove CPT
-Schmertmann (1976) Si Si Si Si Si Si Si Si
Si Si
-Jamiolkowski et al. (1985) No No No No No No No No
No No
-Baldi et al. (1986) No No No No No No No No
No No
Elaborazione dei risultati
-Valore medio x x x x x x x x
x x
-Valore minore
Angolo d'attrito
Correlato con prove SPT
-Terzaghi e Peck (1948) Si Si Si Si Si Si Si Si
Si Si
-Schmertmann (1975) No No No No No No No No
No No
-Wolff (1989) No No No No No No No No
No No
-Hatanaka e Uchida (1996) No No No No No No No No
No No
-Road Bridge Specification No No No No No No No No
No No
-Owasaki e Iwasaki No No No No No No No No
No No
-Japanese National Railway No No No No No No No No
No No
-Peck-Hanson e Thornburn No No No No No No No No
No No
-De Mello No No No No No No No No
No No
Correlato con prove CPT
-Robertson e Campanella (1983) Si Si Si Si Si Si Si Si
Si Si
-Durgunoglu e Mitchell No No No No No No No No
No No
-Caquot No No No No No No No No
No No
Correlata con proprietà indice
-In funzione della densità relativa, per terreni incoerenti No No No No No No No No
No No
-In funzione dell'indice di plasticità, per terreni coesivi No No No No No No No No
No No
Elaborazione dei risultati

-Valore medio x x x x x x x x x x
-Valore minore
Coesione non drenata
Correlata con prove SPT
-Hara et al. (1971) Si Si Si Si Si Si Si Si Si Si
-Stroud (1974) No No No No No No No No No No
Correlata con prove CPT
-Mayne e Kemper (1988) Si Si Si Si Si Si Si Si Si Si
-Lunne e Eide No No No No No No No No No No
Correlata con proprietà indice
-Bjerrum e Simons (1960) No No No No No No No No No No
-Skempton (1953) No No No No No No No No No No
-Calcolata da $\sigma'v_0$ con moltiplicatore pari a No No No No No No No No No No
Pari a 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
Elaborazione dei risultati
-Valore medio x x x x x x x x x x
-Valore minore
Caratteristiche litostatiche
Grado di sovraconsolidazione
-Correlato con prove SPT
-Mayne e Kemper (1988) Si No No No No No No No No No
-Correlato con prove CPT
-Mayne e Kemper (1988) No No No No No No No No No No
-Elaborazione dei risultati
-Valore medio x x x x x x x x x x
-Valore minore
Coefficiente di spinta a riposo
-Calcolo di k_0 (NC)
-Jaky (1936) x x x x x x x x x x
-Brooker e Ireland (1965)
-Alpan (1967)
-Massarsch (1979)
-Correlato con Dr
-Calcolato dal coefficiente di Poisson
-Calcolo di α
-Pari a
-Kulhawy (1989) x x x x x x x x x x
-Alpan (1967) per terreni coesivi
-Alpan (1967) per terreni incoerenti
-Correlato con Dr
Parametri elastici
Correlati con prove GFS
Correlati con prove SPT
-Stroud e Butler (1975)
-Stroud (1989) x x x x x x x x x x
-Schmertmann (1978)
-Farrent
-Menzenbach e Malcev
-D'Appolonia
-Schulze e Menzenbach
-Crespellani e Vannucchi
-Ohsaki e Iwasaki, per sabbie
-Ohsaki e Iwasaki, per sabbie con fini
Correlati con prove CPT
-Schmertmann (1977)
-Robertson e Campanella (1983)
-Kulhawy e Mayne (1990)

-Rix e Stokoe (1992)
-Mayne e Rix (1993)
Fattore correttivo 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0

PIU – PROGETTO INNOVAZIONE URBANA

OPERAZIONE COWORKING, MEDIALIBRARY

A6 – RELAZIONE GEOTECNICA

NUOVO TOTEM

(OTTOBRE 2017)

Introduzione

Sistemi di riferimento
Le coordinate, i carichi concentrati, i cedimenti, le reazioni vincolari e gli spostamenti dei NODI sono riferiti ad una terna destra cartesiana globale con l'asse Z verticale rivolto verso l'alto.
I carichi in coordinate locali e le sollecitazioni delle ASTE sono riferite ad una terna destra cartesiana locale così definita:
- origine nel nodo iniziale dell'asta;
- asse X coincidente con l'asse dell'asta e con verso dal nodo iniziale al nodo finale;
- immaginando la trave a sezione rettangolare l'asse Y è parallelo alla base e l'asse Z è parallelo all'altezza. La rotazione dell'asta comporta quindi una rotazione di tutta la terna locale.

Si può immaginare la terna locale di un'asta comunque disposta nello spazio come derivante da quella globale dopo una serie di trasformazioni:
- una rotazione intorno all'asse Z che porti l'asse X a coincidere con la proiezione dell'asse dell'asta sul piano orizzontale;
- una traslazione lungo il nuovo asse X così definito in modo da portare l'origine a coincidere con la proiezione del nodo iniziale dell'asta sul piano orizzontale;
- una traslazione lungo l'asse Z che porti l'origine a coincidere con il nodo iniziale dell'asta;
- una rotazione intorno all'asse Y così definito che porti l'asse X a coincidere con l'asse dell'asta;
- una rotazione intorno all'asse X così definito pari alla rotazione dell'asta.

In pratica le travi prive di rotazione avranno sempre l'asse Z rivolto verso l'alto e l'asse Y nel piano del solaio, mentre i pilastri privi di rotazione avranno l'asse Y parallelo all'asse Y globale e l'asse Z parallelo ma controverso all'asse X globale. Da notare quindi che per i pilastri la "base" è il lato parallelo a Y.

Le sollecitazioni ed i carichi in coordinate locali negli ELEMENTI BIDIMENSIONALI e nei MURI sono riferiti ad una terna destra cartesiana locale così definita:
- origine nel primo nodo dell'elemento;
- asse X coincidente con la congiungente il primo ed il secondo nodo dell'elemento;
- asse Y definito come prodotto vettoriale fra il versore dell'asse X e il versore della congiungente il primo e il quarto nodo. Asse Z a formare con gli altri due una terna destrorsa.

Praticamente un elemento verticale con l'asse X locale coincidente con l'asse X globale ha anche gli altri assi locali coincidenti con quelli globali.

Rotazioni e momenti
Seguendo il principio adottato per tutti i carichi che sono positivi se CONTROVERSI agli assi, anche i momenti concentrati e le rotazioni impresse in coordinate globali risultano positivi se CONTROVERSI al segno positivo delle rotazioni. Il segno positivo dei momenti e delle rotazioni è quello orario per l'osservatore posto nell'origine: X ruota su Y, Y ruota su Z, Z ruota su X. In pratica è sufficiente adottare la regola della mano destra: col pollice rivolto nella direzione dell'asse, la rotazione che porta a chiudere il palmo della mano corrisponde al segno positivo.

Normativa di riferimento
La normativa di riferimento è la seguente:
- Legge n. 64 del 2/2/1974 - Provvedimenti per le costruzioni con particolari prescrizioni per le zone sismiche.

- D.M. del 24/1/1986 - Norme tecniche relative alle costruzioni sismiche.

- Legge n. 1086 del 5/11/1971 - Norme per la disciplina delle opere di conglomerato cementizio armato, normale e precompresso ed a struttura metallica.

- D.M. del 14/2/1992 - Norme tecniche per l'esecuzione delle opere in c.a. normale e precompresso e per le strutture metalliche.

- D.M. del 9/1/1996 - Norme tecniche per l'esecuzione delle opere in c.a. normale e precompresso e per le strutture metalliche.

- D.M. del 16/1/1996 - Norme tecniche per le costruzioni in zone sismiche.

- Circolare n. 21745 del 30/7/1981 - Legge n. 219 del 14/5/1981 - Art. 10 - Istruzioni relative al

rafforzamento degli edifici in muratura danneggiati dal sisma.

- Regione Autonoma Friuli Venezia Giulia - Legge Regionale n. 30 del 20/6/1977 - Documentazione tecnica per la progettazione e direzione delle opere di riparazione degli edifici - Documento Tecnico n. 2 - Raccomandazioni per la riparazione strutturale degli edifici in muratura.

- D.M. del 20/11/1987 - Norme Tecniche per la progettazione, esecuzione e collaudo degli edifici in muratura e per il loro consolidamento.

- Norme Tecniche C.N.R. n. 10011-85 del 18/4/1985 - Costruzioni di acciaio - Istruzioni per il calcolo, l'esecuzione, il collaudo e la manutenzione.

- Norme Tecniche C.N.R. n. 10025-84 del 14/12/1984 - Istruzioni per il progetto, l'esecuzione ed il controllo delle strutture prefabbricate in conglomerato cementizio e per le strutture costruite con sistemi industrializzati di acciaio - Istruzioni per il calcolo, l'esecuzione, il collaudo e la manutenzione.

- Circolare n. 65 del 10/4/1997 - Istruzioni per l'applicazione delle "Norme tecniche per le costruzioni in zone sismiche" di cui al D.M. del 16/1/1996.

- Eurocodice 5 - Progettazione delle strutture di legno.

- DIN 1052 - Metodi di verifica per il legno.

- D.M. del 14/1/2008 - Norme tecniche per le costruzioni. Le verifiche degli elementi di fondazione sono eseguite utilizzando l'Approccio 2.

- Circolare n. 617 del 2/2/2009 - Istruzioni per l'applicazione delle "Nuove norme tecniche per le costruzioni" di cui al D.M. del 14/1/2008.

- Documento Tecnico CNR-DT 200 R1/2012 - Istruzioni per la Progettazione, l'Esecuzione ed il Controllo di Interventi di Consolidamento Statico mediante l'utilizzo di Compositi Fibrorinforzati.

- Eurocodice 3 - Progettazione delle strutture in acciaio.

Unità di misura
Le unità di misura adottate sono le seguenti:
- lunghezze : m
- forze : daN
- masse : kg
- temperature : gradi centigradi
- angoli : gradi sessadecimali o radianti

ELENCO VINCOLI NODI

Simbologia

Vn = Numero del vincolo nodo
Comm. = Commento
TV = Tipo vincolo se valutato da stratigrafia
SP = Plinto senza pali
CP = Palo o plinto con pali
Sx = Spostamento in dir. X (L=libero, B=bloccato, E=elastico)
Sy = Spostamento in dir. Y (L=libero, B=bloccato, E=elastico)
Sz = Spostamento in dir. Z (L=libero, B=bloccato, E=elastico)
Rx = Rotazione intorno all'asse X (L=libera, B=bloccata, E=elastica)
Ry = Rotazione intorno all'asse Y (L=libera, B=bloccata, E=elastica)
Rz = Rotazione intorno all'asse Z (L=libera, B=bloccata, E=elastica)
RL = Rotazione libera
Ly = Lunghezza (dir. Y locale)
Lz = Larghezza (dir. Z locale)
Kt = Coeff. di sottofondo su suolo elastico alla Winkler

Vn	Comm.	TV	Sx	Sy	Sz	Rx	Ry	Rz	RL	Ly <m>	Lz <m>	Kt <daN/cmc>
1	Libero		L	L	L	L	L	L				
6		CP	E	E	E	E	E	B				f(strat.)

Vn	Comm.	TV	Sx	Sy	Sz	Rx	Ry	Rz	RL	Ly <m>	Lz <m>	Kt <daN/cmc>
2	Incastro		B	B	B	B	B	B				
6		SP	B	B	E	E	E	B				f(strat.)

ELENCO COSTANTI ELASTICHE NODALI

Simbologia

Nodo = Numero del nodo
Kx = Costante elastica in dir. X
Ky = Costante elastica in dir. Y
Kz = Costante elastica in dir. Z
KRx = Costante elastica intorno all'asse X
KRy = Costante elastica intorno all'asse Y

Nodo	Kx <daN/cm>	Ky <daN/cm>	Kz <daN/cm>	KRx <daNm/rad>	KRy <daNm/rad>	Nodo	Kx <daN/cm>	Ky <daN/cm>	Kz <daN/cm>	KRx <daNm/rad>	KRy <daNm/rad>
1	--	--	63037.50	7585510.00	7585510.00	2	--	--	63037.50	7585510.00	7585510.00
3	--	--	63037.50	7585510.00	7585510.00	4	--	--	63037.50	7585510.00	7585510.00

ELENCO NODI

Simbologia

Nodo = Numero del nodo
X = Coordinata X del nodo
Y = Coordinata Y del nodo
Z = Coordinata Z del nodo
Imp. = Numero dell'impalcato
Vn = Numero del vincolo nodo

Nodo	X <m>	Y <m>	Z <m>	Imp.	Vn	Nodo	X <m>	Y <m>	Z <m>	Imp.	Vn	Nodo	X <m>	Y <m>	Z <m>	Imp.	Vn
-284	14.10	-22.29	19.50	0	1	-283	12.50	-22.29	19.50	0	1	-282	13.30	-23.49	19.50	0	1
-281	14.10	-24.69	19.50	0	1	-280	12.50	-24.69	19.50	0	1	-279	14.12	-22.27	17.69	0	1
-278	12.48	-22.27	17.69	0	1	-277	14.12	-24.71	17.69	0	1	-276	12.48	-24.71	17.69	0	1
-275	14.14	-22.25	15.88	0	1	-274	12.46	-22.25	15.88	0	1	-273	14.14	-24.73	15.88	0	1
-272	12.46	-24.73	15.88	0	1	-271	14.16	-22.23	14.06	0	1	-270	12.44	-22.23	14.06	0	1
-269	13.30	-23.49	14.06	0	1	-268	14.16	-24.75	14.06	0	1	-267	12.44	-24.75	14.06	0	1
-266	14.18	-22.21	12.25	0	1	-265	12.43	-22.21	12.25	0	1	-264	14.18	-24.77	12.25	0	1
-263	12.43	-24.77	12.25	0	1	-262	14.19	-22.20	10.44	0	1	-261	12.41	-22.20	10.44	0	1
-260	14.19	-24.78	10.44	0	1	-259	12.41	-24.78	10.44	0	1	-258	14.21	-22.18	8.63	0	1
-257	12.39	-22.18	8.63	0	1	-256	13.30	-23.49	8.63	0	1	-255	14.21	-24.80	8.63	0	1
-254	12.39	-24.80	8.63	0	1	-253	14.23	-22.16	6.81	0	1	-252	12.37	-22.16	6.81	0	1
-251	14.23	-24.82	6.81	0	1	-250	12.37	-24.82	6.81	0	1	-249	14.25	-22.14	5.00	0	1
-248	13.30	-22.14	5.00	0	1	-247	12.35	-22.14	5.00	0	1	-246	6.05	-22.14	5.00	0	1
-245	6.05	-22.48	5.00	0	1	-244	14.25	-22.82	5.00	0	1	-243	12.35	-22.82	5.00	0	1
-242	6.05	-22.82	5.00	0	1	-241	6.05	-23.15	5.00	0	1	-240	14.25	-23.49	5.00	0	1
-239	12.35	-23.49	5.00	0	1	-238	6.05	-23.49	5.00	0	1	-237	6.05	-23.83	5.00	0	1
-236	14.25	-24.16	5.00	0	1	-235	12.35	-24.16	5.00	0	1	-234	6.05	-24.16	5.00	0	1
-233	6.05	-24.50	5.00	0	1	-232	20.88	-24.84	5.00	0	2	-231	14.25	-24.84	5.00	0	1
-230	13.30	-24.84	5.00	0	1	-229	12.35	-24.84	5.00	0	1	-228	6.05	-24.84	5.00	0	1
-227	6.05	-22.14	4.67	0	1	-226	6.05	-22.48	4.67	0	1	-225	6.05	-22.82	4.67	0	1
-224	6.05	-23.15	4.67	0	1	-223	6.05	-23.49	4.67	0	1	-222	6.05	-23.83	4.67	0	1
-221	6.05	-24.16	4.67	0	1	-220	6.05	-24.50	4.67	0	1	-219	6.05	-24.84	4.67	0	1
-218	6.05	-22.14	4.33	0	1	-217	6.05	-22.48	4.33	0	1	-216	6.05	-22.82	4.33	0	1
-215	6.05	-23.15	4.33	0	1	-214	6.05	-23.49	4.33	0	1	-213	6.05	-23.83	4.33	0	1
-212	6.05	-24.16	4.33	0	1	-211	6.05	-24.50	4.33	0	1	-210	6.05	-24.84	4.33	0	1
-209	14.25	-22.14	4.00	0	1	-208	13.30	-22.14	4.00	0	1	-207	12.35	-22.14	4.00	0	1
-206	6.05	-22.14	4.00	0	1	-205	6.05	-22.48	4.00	0	1	-204	14.25	-22.82	4.00	0	1
-203	12.35	-22.82	4.00	0	1	-202	6.05	-22.82	4.00	0	1	-201	6.05	-23.15	4.00	0	1
-200	14.25	-23.49	4.00	0	1	-199	12.35	-23.49	4.00	0	1	-198	6.05	-23.49	4.00	0	1
-197	6.05	-23.83	4.00	0	1	-196	14.25	-24.16	4.00	0	1	-195	12.35	-24.16	4.00	0	1
-194	6.05	-24.16	4.00	0	1	-193	6.05	-24.50	4.00	0	1	-192	14.25	-24.84	4.00	0	1
-191	13.30	-24.84	4.00	0	1	-190	12.35	-24.84	4.00	0	1	-189	6.05	-24.84	4.00	0	1
-188	6.05	-22.14	3.67	0	1	-187	6.05	-22.48	3.67	0	1	-186	6.05	-22.82	3.67	0	1

-185	6.05	-23.15	3.67	0	1	-184	6.05	-23.49	3.67	0	1	-183	6.05	-23.83	3.67	0	1
-182	6.05	-24.16	3.67	0	1	-181	6.05	-24.50	3.67	0	1	-180	6.05	-24.84	3.67	0	1
-179	6.05	-22.14	3.33	0	1	-178	6.05	-22.48	3.33	0	1	-177	6.05	-22.82	3.33	0	1
-176	6.05	-23.15	3.33	0	1	-175	6.05	-23.49	3.33	0	1	-174	6.05	-23.83	3.33	0	1
-173	6.05	-24.16	3.33	0	1	-172	6.05	-24.50	3.33	0	1	-171	6.05	-24.84	3.33	0	1
-170	14.25	-22.14	3.00	0	1	-169	13.30	-22.14	3.00	0	1	-168	12.35	-22.14	3.00	0	1
-167	6.05	-22.14	3.00	0	1	-166	6.05	-22.48	3.00	0	1	-165	14.25	-22.82	3.00	0	1
-164	12.35	-22.82	3.00	0	1	-163	6.05	-22.82	3.00	0	1	-162	6.05	-23.15	3.00	0	1
-161	14.25	-23.49	3.00	0	1	-160	12.35	-23.49	3.00	0	1	-159	6.05	-23.49	3.00	0	1
-158	6.05	-23.83	3.00	0	1	-157	14.25	-24.16	3.00	0	1	-156	12.35	-24.16	3.00	0	1
-155	6.05	-24.16	3.00	0	1	-154	6.05	-24.50	3.00	0	1	-153	14.25	-24.84	3.00	0	1
-152	13.30	-24.84	3.00	0	1	-151	12.35	-24.84	3.00	0	1	-150	6.05	-24.84	3.00	0	1
-149	6.05	-22.14	2.67	0	1	-148	6.05	-22.48	2.67	0	1	-147	6.05	-22.82	2.67	0	1
-146	6.05	-23.15	2.67	0	1	-145	6.05	-23.49	2.67	0	1	-144	6.05	-23.83	2.67	0	1
-143	6.05	-24.16	2.67	0	1	-142	6.05	-24.50	2.67	0	1	-141	6.05	-24.84	2.67	0	1
-140	6.05	-22.14	2.33	0	1	-139	6.05	-22.48	2.33	0	1	-138	6.05	-22.82	2.33	0	1
-137	6.05	-23.15	2.33	0	1	-136	6.05	-23.49	2.33	0	1	-135	6.05	-23.83	2.33	0	1
-134	6.05	-24.16	2.33	0	1	-133	6.05	-24.50	2.33	0	1	-132	6.05	-24.84	2.33	0	1
-131	14.25	-22.14	2.00	0	1	-130	13.30	-22.14	2.00	0	1	-129	12.35	-22.14	2.00	0	1
-128	6.05	-22.14	2.00	0	1	-127	6.05	-22.48	2.00	0	1	-126	14.25	-22.82	2.00	0	1
-125	12.35	-22.82	2.00	0	1	-124	6.05	-22.82	2.00	0	1	-123	6.05	-23.15	2.00	0	1
-122	14.25	-23.49	2.00	0	1	-121	12.35	-23.49	2.00	0	1	-120	6.05	-23.49	2.00	0	1
-119	6.05	-23.83	2.00	0	1	-118	14.25	-24.16	2.00	0	1	-117	12.35	-24.16	2.00	0	1
-116	6.05	-24.16	2.00	0	1	-115	6.05	-24.50	2.00	0	1	-114	14.25	-24.84	2.00	0	1
-113	13.30	-24.84	2.00	0	1	-112	12.35	-24.84	2.00	0	1	-111	6.05	-24.84	2.00	0	1
-110	6.05	-22.14	1.67	0	1	-109	6.05	-22.48	1.67	0	1	-108	6.05	-22.82	1.67	0	1
-107	6.05	-23.15	1.67	0	1	-106	6.05	-23.49	1.67	0	1	-105	6.05	-23.83	1.67	0	1
-104	6.05	-24.16	1.67	0	1	-103	6.05	-24.50	1.67	0	1	-102	6.05	-24.84	1.67	0	1
-101	6.05	-22.14	1.33	0	1	-100	6.05	-22.48	1.33	0	1	-99	6.05	-22.82	1.33	0	1
-98	6.05	-23.15	1.33	0	1	-97	6.05	-23.49	1.33	0	1	-96	6.05	-23.83	1.33	0	1
-95	6.05	-24.16	1.33	0	1	-94	6.05	-24.50	1.33	0	1	-93	6.05	-24.84	1.33	0	1
-92	14.25	-22.14	1.00	0	1	-91	13.30	-22.14	1.00	0	1	-90	12.35	-22.14	1.00	0	1
-89	6.05	-22.14	1.00	0	1	-88	6.05	-22.48	1.00	0	1	-87	14.25	-22.82	1.00	0	1
-86	12.35	-22.82	1.00	0	1	-85	6.05	-22.82	1.00	0	1	-84	6.05	-23.15	1.00	0	1
-83	14.25	-23.49	1.00	0	1	-82	12.35	-23.49	1.00	0	1	-81	6.05	-23.49	1.00	0	1
-80	6.05	-23.83	1.00	0	1	-79	14.25	-24.16	1.00	0	1	-78	12.35	-24.16	1.00	0	1
-77	6.05	-24.16	1.00	0	1	-76	6.05	-24.50	1.00	0	1	-75	14.25	-24.84	1.00	0	1
-74	13.30	-24.84	1.00	0	1	-73	12.35	-24.84	1.00	0	1	-72	6.05	-24.84	1.00	0	1
-71	6.05	-22.14	0.67	0	1	-70	6.05	-22.48	0.67	0	1	-69	6.05	-22.82	0.67	0	1
-68	6.05	-23.15	0.67	0	1	-67	6.05	-23.49	0.67	0	1	-66	6.05	-23.83	0.67	0	1
-65	6.05	-24.16	0.67	0	1	-64	6.05	-24.50	0.67	0	1	-63	6.05	-24.84	0.67	0	1
-62	6.05	-22.14	0.33	0	1	-61	6.05	-22.48	0.33	0	1	-60	6.05	-22.82	0.33	0	1
-59	6.05	-23.15	0.33	0	1	-58	6.05	-23.49	0.33	0	1	-57	6.05	-23.83	0.33	0	1
-56	6.05	-24.16	0.33	0	1	-55	6.05	-24.50	0.33	0	1	-54	6.05	-24.84	0.33	0	1
-50	13.30	-22.14	0.00	0	1	-46	6.05	-22.14	0.00	0	2	-41	6.05	-22.48	0.00	0	2
-38	14.25	-22.82	0.00	0	1	-37	12.35	-22.82	0.00	0	1	-36	6.05	-22.82	0.00	0	2
-31	6.05	-23.15	0.00	0	2	-28	14.25	-23.49	0.00	0	1	-27	12.35	-23.49	0.00	0	1
-26	6.05	-23.49	0.00	0	2	-21	6.05	-23.83	0.00	0	2	-18	14.25	-24.16	0.00	0	1
-17	12.35	-24.16	0.00	0	1	-16	6.05	-24.16	0.00	0	2	-11	6.05	-24.50	0.00	0	2
-5	13.30	-24.84	0.00	0	1	-1	6.05	-24.84	0.00	0	2	1	12.35	-24.84	0.00	0	6
2	14.25	-24.84	0.00	0	6	3	12.35	-22.14	0.00	0	6	4	14.25	-22.14	0.00	0	6
101	20.88	-22.14	5.00	0	2												

ELENCO MATERIALI

Simbologia

Mat. = Numero del materiale
Comm. = Commento
P = Peso specifico
E = Modulo elastico
G = Modulo elastico tangenziale
ν = Coeff. di Poisson
α = Coeff. di dilatazione termica

Mat.	Comm.	P <daN/mc>	E <daN/cmq>	G <daN/cmq>	ν	α
1	Calcestruzzo	2500	300000.00	130000.00	0.1	1.000000E-05
2	Acciaio	7850	2100000.00	800000.00	0.3	1.000000E-05

6	MURATURA	1500	8000.00	1300.00	0.2	0.02

ELENCO SEZIONI ASTE

Simbologia

Sez. = Numero della sezione
Comm. = Commento
Tipo = Tipologia
- 2C = Doppia C lato labbri
- 2Cdx = Doppia C lato costola
- 2I = Doppia I
- 2L = Doppia L lato labbri
- 2Ldx = Doppia L lato costole
- C = Sezione a C
- Cdx = C destra
- Cir. = Circolare
- Cir.c = Circolare cava
- I = Sezione a I
- L = Sezione a L
- Ldx = L destra
- Om. = Omega
- Pg = Pi greco
- Pr = Poligono regolare
- Prc = Poligono regolare cavo
- Pc = Per coordinate
- Ia = Inerzie assegnate
- R = Rettangolare
- Rc = Rettangolare cava
- T = Sezione a T
- U = Sezione a U
- Ur = U rovescia
- V = Sezione a V
- Vr = V rovescia
- Z = Sezione a Z
- Zdx = Z destra
- Ts = T stondata
- Ls = L stondata
- Cs = C stondata
- Is = I stondata
- Dis. = Disegnata

Mem. = Membratura
- G = Generica
- T = Trave
- P = Pilastro

Ver. = Verifica prevista
- N = Nessuna
- C = Cemento armato
- A = Acciaio
- L = Legno

B = Base
H = Altezza
s = Spessore ala
r = Raggio raccordo anima-ala
r1 = Raggio in testa ala
Ma = Numero del materiale
C = Numero del criterio di progetto
Crit. C.I. = Criterio di progetto collegamento iniziale
Crit. C.F. = Criterio di progetto collegamento finale

Sez.	Comm.	Tipo	Mem.	Ver.	B <cm>	H <cm>	s <cm>	r <cm>	r1 <cm>	Ma	C	Crit. C.I.	Crit. C.F.
1	P40X40	R	P	C	40.00	40.00				1	5		
15	L100x10	Ls	G	A	10.00	10.00	1.00	1.20	0.60	2	1	2	2
17	L120x10	Ls	G	A	12.00	12.00	1.00	1.30	0.65	2	1	2	2
19	L80x7	Ls	G	A	8.00	8.00	0.70	1.00	0.00	2	1	6	6
20		Ls	G	A	8.00	8.00	0.70	1.00	0.00	2	2	5	5

ELENCO VINCOLI ASTE

Simbologia

Va   = Numero del vincolo asta
Comm. = Commento
Tipo = Tipologia
        SVI = Definizione di vincolamenti interni
        ELA = Vincolo su suolo elastico alla Winkler
        BIE-RTC = Biella resistente a trazione e a compressione
        BIE-RC = Biella resistente solo a compressione
        BIE-RT = Biella resistente solo a trazione
Ni   = Sforzo normale nodo iniziale (0=sbloccato, 1=bloccato)
Tyi   = Taglio in dir. Y locale nodo iniziale (0=sbloccato, 1=bloccato)
Tzi   = Taglio in dir. Z locale nodo iniziale (0=sbloccato, 1=bloccato)
Mxi   = Momento intorno all'asse X locale nodo iniziale (0=sbloccato, 1=bloccato)
Myi   = Momento intorno all'asse Y locale nodo iniziale (0=sbloccato, 1=bloccato)
Mzi   = Momento intorno all'asse Z locale nodo iniziale (0=sbloccato, 1=bloccato)
Nf   = Sforzo normale nodo finale (0=sbloccato, 1=bloccato)
Tyf   = Taglio in dir. Y locale nodo finale (0=sbloccato, 1=bloccato)
Tzf   = Taglio in dir. Z locale nodo finale (0=sbloccato, 1=bloccato)
Mxf   = Momento intorno all'asse X locale nodo finale (0=sbloccato, 1=bloccato)
Myf   = Momento intorno all'asse Y locale nodo finale (0=sbloccato, 1=bloccato)
Mzf   = Momento intorno all'asse Z locale nodo finale (0=sbloccato, 1=bloccato)
Kt   = Coeff. di sottofondo su suolo elastico alla Winkler

Va	Comm.	Tipo	Ni	Tyi	Tzi	Mxi	Myi	Mzi	Nf	Tyf	Tzf	Mxf	Myf	Mzf	Kt <daN/cmc>
1	Inc+Inc	SVI	1	1	1	1	1	1	1	1	1	1	1	1	
4	Cer+Cer	SVI	1	1	1	0	0	0	1	1	1	1	0	0	

ELENCO ASTE

Simbologia

Asta = Numero dell'asta
N1   = Nodo iniziale
N2   = Nodo finale
Sez. = Numero della sezione
Va   = Numero del vincolo asta
Par. = Numero dei parametri aggiuntivi
Rot. = Rotazione
FF   = Filo fisso
Dy1 = Scost. filo fisso Y1
Dy2 = Scost. filo fisso Y2
Dz1 = Scost. filo fisso Z1
Dz2 = Scost. filo fisso Z2
Kt   = Coeff. di sottofondo su suolo elastico alla Winkler

Asta	N1	N2	Sez.	Va	Par.	Rot. <grad>	FF	Dy1 <cm>	Dy2 <cm>	Dz1 <cm>	Dz2 <cm>	Kt <daN/cmc>
0	-228	-233	1			0.00	11	0.00	0.00	0.00	0.00	
0	-233	-234	1			0.00	11	0.00	0.00	0.00	0.00	
0	-234	-237	1			0.00	11	0.00	0.00	0.00	0.00	
0	-237	-238	1			0.00	11	0.00	0.00	0.00	0.00	
0	-238	-241	1			0.00	11	0.00	0.00	0.00	0.00	
0	-241	-242	1			0.00	11	0.00	0.00	0.00	0.00	
0	-242	-245	1			0.00	11	0.00	0.00	0.00	0.00	
0	-245	-246	1			0.00	11	0.00	0.00	0.00	0.00	
0	-228	-229	1			0.00	11	0.00	0.00	0.00	0.00	
0	-246	-247	1			0.00	11	0.00	0.00	0.00	0.00	
0	-235	-229	1			0.00	55	0.00	0.00	0.00	0.00	
0	-239	-235	1			0.00	55	0.00	0.00	0.00	0.00	
0	-243	-239	1			0.00	55	0.00	0.00	0.00	0.00	
0	-236	-231	1			0.00	55	0.00	0.00	0.00	0.00	
0	-247	-243	1			0.00	55	0.00	0.00	0.00	0.00	
0	-240	-236	1			0.00	55	0.00	0.00	0.00	0.00	
0	-244	-240	1			0.00	55	0.00	0.00	0.00	0.00	
0	-249	-244	1			0.00	55	0.00	0.00	0.00	0.00	

0	-231	-232		1	0.00	11	0.00	0.00	0.00	0.00
0	-249	101		1	0.00	11	0.00	0.00	0.00	0.00
0	-232	101		1	0.00	22	0.00	0.00	0.00	0.00
1	1	-73	1	1	0.00	11	-12.50	-12.50	13.50	13.50
1	-73	-112	1	1	0.00	11	-12.50	-12.50	13.50	13.50
1	-112	-151	1	1	0.00	11	-12.50	-12.50	13.50	13.50
1	-151	-190	1	1	0.00	11	-12.50	-12.50	13.50	13.50
1	-190	-229	1	1	0.00	11	-12.50	-12.50	13.50	13.50
2	2	-75	1	1	180.00	33	12.50	12.50	13.50	13.50
2	-75	-114	1	1	180.00	33	12.50	12.50	13.50	13.50
2	-114	-153	1	1	180.00	33	12.50	12.50	13.50	13.50
2	-153	-192	1	1	180.00	33	12.50	12.50	13.50	13.50
2	-192	-231	1	1	180.00	33	12.50	12.50	13.50	13.50
3	3	-90	1	1	0.00	33	12.50	12.50	13.50	13.50
3	-90	-129	1	1	0.00	33	12.50	12.50	13.50	13.50
3	-129	-168	1	1	0.00	33	12.50	12.50	13.50	13.50
3	-168	-207	1	1	0.00	33	12.50	12.50	13.50	13.50
3	-207	-247	1	1	0.00	33	12.50	12.50	13.50	13.50
4	4	-92	1	1	180.00	11	-12.50	-12.50	13.50	13.50
4	-92	-131	1	1	180.00	11	-12.50	-12.50	13.50	13.50
4	-131	-170	1	1	180.00	11	-12.50	-12.50	13.50	13.50
4	-170	-209	1	1	180.00	11	-12.50	-12.50	13.50	13.50
4	-209	-249	1	1	180.00	11	-12.50	-12.50	13.50	13.50
301	-250	-251	19	4	0.00	55	0.00	0.00	0.00	0.00
302	-254	-255	19	4	0.00	55	0.00	0.00	0.00	0.00
303	-259	-260	19	4	0.00	55	0.00	0.00	0.00	0.00
304	-263	-264	19	4	0.00	55	0.00	0.00	0.00	0.00
305	-267	-268	19	4	0.00	55	0.00	0.00	0.00	0.00
306	-272	-273	19	4	0.00	55	0.00	0.00	0.00	0.00
307	-276	-277	19	4	0.00	55	0.00	0.00	0.00	0.00
308	-280	-281	19	4	270.00	55	0.00	0.00	0.00	0.00
309	-283	-284	19	4	270.00	55	0.00	0.00	0.00	0.00
310	-279	-278	19	4	0.00	55	0.00	0.00	0.00	0.00
311	-275	-274	19	4	0.00	55	0.00	0.00	0.00	0.00
312	-271	-270	19	4	0.00	55	0.00	0.00	0.00	0.00
313	-266	-265	19	4	0.00	55	0.00	0.00	0.00	0.00
314	-262	-261	19	4	0.00	55	0.00	0.00	0.00	0.00
315	-258	-257	19	4	0.00	55	0.00	0.00	0.00	0.00
316	-253	-252	19	4	0.00	55	0.00	0.00	0.00	0.00
317	-250	-252	19	4	180.00	55	0.00	0.00	0.00	0.00
318	-254	-257	19	4	180.00	55	0.00	0.00	0.00	0.00
319	-259	-261	19	4	180.00	55	0.00	0.00	0.00	0.00
320	-263	-265	19	4	180.00	55	0.00	0.00	0.00	0.00
321	-267	-270	19	4	180.00	55	0.00	0.00	0.00	0.00
322	-272	-274	19	4	180.00	55	0.00	0.00	0.00	0.00
323	-276	-278	19	4	180.00	55	0.00	0.00	0.00	0.00
324	-283	-280	19	4	270.00	55	0.00	0.00	0.00	0.00
325	-281	-284	19	4	270.00	55	0.00	0.00	0.00	0.00
326	-279	-277	19	4	180.00	55	0.00	0.00	0.00	0.00
327	-275	-273	19	4	180.00	55	0.00	0.00	0.00	0.00
328	-268	-271	19	4	0.00	55	0.00	0.00	0.00	0.00
329	-266	-264	19	4	180.00	55	0.00	0.00	0.00	0.00
330	-262	-260	19	4	180.00	55	0.00	0.00	0.00	0.00
331	-258	-255	19	4	180.00	55	0.00	0.00	0.00	0.00
332	-253	-251	19	4	180.00	55	0.00	0.00	0.00	0.00
333	-229	-251	15	4	0.00	11	0.00	0.00	0.00	0.00
334	-251	-254	15	4	180.00	11	0.00	0.00	0.00	0.00
335	-254	-260	15	4	0.00	11	0.00	0.00	0.00	0.00
336	-260	-263	15	4	180.00	11	0.00	0.00	0.00	0.00
337	-229	-250	17	4	228.00	77	0.00	0.00	0.00	0.00
337	-250	-254	17	4	228.00	77	0.00	0.00	0.00	0.00
337	-254	-259	17	4	228.00	77	0.00	0.00	0.00	0.00
337	-259	-263	17	4	228.00	77	0.00	0.00	0.00	0.00
337	-263	-267	17	4	228.00	77	0.00	0.00	0.00	0.00
337	-267	-272	17	4	228.00	77	0.00	0.00	0.00	0.00
337	-272	-276	17	4	228.00	77	0.00	0.00	0.00	0.00
337	-276	-280	17	4	228.00	77	0.00	0.00	0.00	0.00
338	-231	-251	17	4	224.00	55	0.00	0.00	0.00	0.00
338	-251	-255	17	4	224.00	55	0.00	0.00	0.00	0.00
338	-255	-260	17	4	224.00	55	0.00	0.00	0.00	0.00
338	-260	-264	17	4	224.00	55	0.00	0.00	0.00	0.00
338	-264	-268	17	4	224.00	55	0.00	0.00	0.00	0.00
338	-268	-273	17	4	224.00	55	0.00	0.00	0.00	0.00

338	-273	-277	17	4	224.00	55	0.00	0.00	0.00	0.00
338	-277	-281	17	4	224.00	55	0.00	0.00	0.00	0.00
339	-263	-268	15	4	0.00	11	0.00	0.00	0.00	0.00
340	-268	-272	15	4	180.00	11	0.00	0.00	0.00	0.00
341	-272	-277	15	4	0.00	11	0.00	0.00	0.00	0.00
342	-277	-280	15	4	180.00	11	0.00	0.00	0.00	0.00
343	-250	-257	15	4	180.00	11	0.00	0.00	0.00	0.00
344	-255	-262	15	4	0.00	11	0.00	0.00	0.00	0.00
345	-276	-283	15	4	180.00	11	0.00	0.00	0.00	0.00
346	-259	-265	15	4	180.00	11	0.00	0.00	0.00	0.00
347	-231	-253	15	4	2.00	11	0.00	0.00	0.00	0.00
348	-264	-271	15	4	0.00	11	0.00	0.00	0.00	0.00
349	-267	-274	15	4	180.00	11	0.00	0.00	0.00	0.00
350	-273	-279	15	4	0.00	11	0.00	0.00	0.00	0.00
351	-280	-282	20	4	0.00	55	0.00	0.00	0.00	0.00
351	-282	-284	20	4	0.00	55	0.00	0.00	0.00	0.00
352	-254	-256	20	4	0.00	55	0.00	0.00	0.00	0.00
352	-256	-258	20	4	0.00	55	0.00	0.00	0.00	0.00
353	-269	-268	20	4	0.00	55	0.00	0.00	0.00	0.00
353	-270	-269	20	4	0.00	55	0.00	0.00	0.00	0.00
354	-256	-255	20	4	0.00	55	0.00	0.00	0.00	0.00
354	-257	-256	20	4	0.00	55	0.00	0.00	0.00	0.00
355	-282	-281	20	4	0.00	55	0.00	0.00	0.00	0.00
355	-283	-282	20	4	0.00	55	0.00	0.00	0.00	0.00
356	-267	-269	20	4	0.00	55	0.00	0.00	0.00	0.00
356	-269	-271	20	4	0.00	55	0.00	0.00	0.00	0.00
357	-253	-255	15	4	180.00	11	0.00	0.00	0.00	0.00
358	-265	-267	15	4	0.00	11	0.00	0.00	0.00	0.00
359	-279	-281	15	4	180.00	11	0.00	0.00	0.00	0.00
360	-259	-257	15	4	270.00	11	0.00	0.00	0.00	0.00
361	-274	-276	15	4	0.00	11	0.00	0.00	0.00	0.00
362	-271	-273	15	4	180.00	11	0.00	0.00	0.00	0.00
363	-247	-250	15	4	0.00	11	0.00	0.00	0.00	0.00
364	-262	-264	15	4	180.00	11	0.00	0.00	0.00	0.00
365	-278	-284	15	4	270.00	11	0.00	0.00	0.00	0.00
366	-275	-278	15	4	36.00	11	0.00	0.00	0.00	0.00
367	-270	-275	15	4	270.00	11	0.00	0.00	0.00	0.00
368	-270	-266	15	4	180.00	11	0.00	0.00	0.00	0.00
369	-253	-249	17	4	225.00	55	0.00	0.00	0.00	0.00
369	-258	-253	17	4	225.00	55	0.00	0.00	0.00	0.00
369	-262	-258	17	4	225.00	55	0.00	0.00	0.00	0.00
369	-266	-262	17	4	225.00	55	0.00	0.00	0.00	0.00
369	-271	-266	17	4	225.00	55	0.00	0.00	0.00	0.00
369	-275	-271	17	4	225.00	55	0.00	0.00	0.00	0.00
369	-279	-275	17	4	225.00	55	0.00	0.00	0.00	0.00
369	-284	-279	17	4	225.00	55	0.00	0.00	0.00	0.00
370	-247	-252	17	4	225.00	55	0.00	0.00	0.00	0.00
370	-252	-257	17	4	225.00	55	0.00	0.00	0.00	0.00
370	-257	-261	17	4	225.00	55	0.00	0.00	0.00	0.00
370	-261	-265	17	4	225.00	55	0.00	0.00	0.00	0.00
370	-265	-270	17	4	225.00	55	0.00	0.00	0.00	0.00
370	-270	-274	17	4	225.00	55	0.00	0.00	0.00	0.00
370	-274	-278	17	4	225.00	55	0.00	0.00	0.00	0.00
370	-278	-283	17	4	225.00	55	0.00	0.00	0.00	0.00
371	-261	-266	15	4	180.00	11	0.00	0.00	0.00	0.00
372	-261	-258	15	4	180.00	11	0.00	0.00	0.00	0.00
373	-252	-258	15	4	180.00	11	0.00	0.00	0.00	0.00
374	-249	-252	15	4	0.00	33	0.00	0.00	0.00	0.00

ELENCO TIPI ELEMENTI BIDIMENSIONALI

Simbologia

Tb = Numero del tipo muro/elemento bidimensionale
Comm. = Commento
Tipo = Tipologia
F = Membranale e Flessionale
M = Membranale
W-RC = Winkler resistente solo a compressione
W-RTC = Winkler resistente a trazione e a compressione
Uso = Utilizzo

G = Generico
P = Parete
S = Soletta/Platea
N = Nucleo
M = Muratura ordinaria
L = Pilastro
MA = Muratura armata
X = Pannello X-LAM

Mat. = Numero del materiale
Crit. = Numero del criterio di progetto
Spess. = Spessore
Kt = Coeff. di sottofondo su suolo elastico alla Winkler

Tb	Comm.	Tipo	Uso	Mat.	Crit.	Spess. <cm>	Kt <daN/cmc>	Tb	Comm.	Tipo	Uso	Mat.	Crit.	Spess. <cm>	Kt <daN/cmc>
4	SETTO 30 F	P		1	1	30.00		6	SETTO 20 F	P		1	5	20.00	

ELENCO ELEMENTI BIDIMENSIONALI

Simbologia

Bid. = Numero del muro/elemento bidimensionale
Tb = Numero del tipo muro/elemento bidimensionale
FF = Filo fisso
Dy1 = Scost. filo fisso Y1
Dy2 = Scost. filo fisso Y2
Kt = Coeff. di sottofondo su suolo elastico alla Winkler
NN = Nodi

Bid.	Tb	FF	Dy1 <cm>	Dy2 <cm>	Kt <daN/cmc>	NN	Bid.	Tb	FF	Dy1 <cm>	Dy2 <cm>	Kt <daN/cmc>	NN
106	4	11	0.00	0.00		-226 -227 -246 -245	106	4	11	0.00	0.00		-225 -226 -245 -242
106	4	11	0.00	0.00		-217 -218 -227 -226	106	4	11	0.00	0.00		-216 -217 -226 -225
106	4	11	0.00	0.00		-205 -206 -218 -217	106	4	11	0.00	0.00		-181 -182 -194 -193
106	4	11	0.00	0.00		-180 -181 -193 -189	106	4	11	0.00	0.00		-172 -173 -182 -181
106	4	11	0.00	0.00		-171 -172 -181 -180	106	4	11	0.00	0.00		-154 -155 -173 -172
106	4	11	0.00	0.00		-183 -184 -198 -197	106	4	11	0.00	0.00		-182 -183 -197 -194
106	4	11	0.00	0.00		-174 -175 -184 -183	106	4	11	0.00	0.00		-173 -174 -183 -182
106	4	11	0.00	0.00		-158 -159 -175 -174	106	4	11	0.00	0.00		-185 -186 -202 -201
106	4	11	0.00	0.00		-184 -185 -201 -198	106	4	11	0.00	0.00		-176 -177 -186 -185
106	4	11	0.00	0.00		-175 -176 -185 -184	106	4	11	0.00	0.00		-162 -163 -177 -176
106	4	11	0.00	0.00		-187 -188 -206 -205	106	4	11	0.00	0.00		-186 -187 -205 -202
106	4	11	0.00	0.00		-178 -179 -188 -187	106	4	11	0.00	0.00		-177 -178 -187 -186
106	4	11	0.00	0.00		-166 -167 -179 -178	106	4	11	0.00	0.00		-220 -221 -234 -233
106	4	11	0.00	0.00		-219 -220 -233 -228	106	4	11	0.00	0.00		-211 -212 -221 -220
106	4	11	0.00	0.00		-210 -211 -220 -219	106	4	11	0.00	0.00		-193 -194 -212 -211
106	4	11	0.00	0.00		-222 -223 -238 -237	106	4	11	0.00	0.00		-221 -222 -237 -234
106	4	11	0.00	0.00		-213 -214 -223 -222	106	4	11	0.00	0.00		-212 -213 -222 -221
106	4	11	0.00	0.00		-197 -198 -214 -213	106	4	11	0.00	0.00		-224 -225 -242 -241

```
 106  4 11   0.00   0.00          -223 -224 -241 -238     106  4 11   0.00   0.00          -215 -
216 -225 -224
 106  4 11   0.00   0.00          -214 -215 -224 -223     106  4 11   0.00   0.00          -201 -
202 -216 -215
 106  4 11   0.00   0.00          -202 -205 -217 -216     106  4 11   0.00   0.00          -198 -
201 -215 -214
 106  4 11   0.00   0.00          -194 -197 -213 -212     106  4 11   0.00   0.00          -189 -
193 -211 -210
 106  4 11   0.00   0.00          -163 -166 -178 -177     106  4 11   0.00   0.00          -159 -
162 -176 -175
 106  4 11   0.00   0.00          -155 -158 -174 -173     106  4 11   0.00   0.00          -150 -
154 -172 -171
 106  4 11   0.00   0.00          -124 -127 -139 -138     106  4 11   0.00   0.00          -120 -
123 -137 -136
 106  4 11   0.00   0.00          -116 -119 -135 -134     106  4 11   0.00   0.00          -111 -
115 -133 -132
 106  4 11   0.00   0.00          -85 -88 -100 -99        106  4 11   0.00   0.00          -81 -84
-98 -97
 106  4 11   0.00   0.00          -77 -80 -96 -95         106  4 11   0.00   0.00          -72 -76
-94 -93
 106  4 11   0.00   0.00          -36 -41 -61 -60         106  4 11   0.00   0.00          -26 -31
-59 -58
 106  4 11   0.00   0.00          -16 -21 -57 -56         106  4 11   0.00   0.00          -107 -
108 -124 -123
 106  4 11   0.00   0.00          -80 -81 -97 -96         106  4 11   0.00   0.00          -95 -96
-105 -104
 106  4 11   0.00   0.00          -96 -97 -106 -105       106  4 11   0.00   0.00          -104 -
105 -119 -116
 106  4 11   0.00   0.00          -105 -106 -120 -119     106  4 11   0.00   0.00          -76 -77
-95 -94
 106  4 11   0.00   0.00          -93 -94 -103 -102       106  4 11   0.00   0.00          -94 -95
-104 -103
 106  4 11   0.00   0.00          -102 -103 -115 -111     106  4 11   0.00   0.00          -103 -
104 -116 -115
 106  4 11   0.00   0.00          -41 -46 -62 -61         106  4 11   0.00   0.00          -60 -61
-70 -69
 106  4 11   0.00   0.00          -61 -62 -71 -70         106  4 11   0.00   0.00          -69 -70
-88 -85
 106  4 11   0.00   0.00          -70 -71 -89 -88         106  4 11   0.00   0.00          -31 -36
-60 -59
 106  4 11   0.00   0.00          -58 -59 -68 -67         106  4 11   0.00   0.00          -59 -60
-69 -68
 106  4 11   0.00   0.00          -67 -68 -84 -81         106  4 11   0.00   0.00          -68 -69
-85 -84
 106  4 11   0.00   0.00          -21 -26 -58 -57         106  4 11   0.00   0.00          -56 -57
-66 -65
 106  4 11   0.00   0.00          -57 -58 -67 -66         106  4 11   0.00   0.00          -65 -66
-80 -77
 106  4 11   0.00   0.00          -66 -67 -81 -80         106  4 11   0.00   0.00          -11 -16
-56 -55
 106  4 11   0.00   0.00          -54 -55 -64 -63         106  4 11   0.00   0.00          -55 -56
-65 -64
 106  4 11   0.00   0.00          -63 -64 -76 -72         106  4 11   0.00   0.00          -64 -65
-77 -76
 106  4 11   0.00   0.00          -148 -149 -167 -166     106  4 11   0.00   0.00          -147 -
148 -166 -163
 106  4 11   0.00   0.00          -139 -140 -149 -148     106  4 11   0.00   0.00          -138 -
139 -148 -147
 106  4 11   0.00   0.00          -127 -128 -140 -139     106  4 11   0.00   0.00          -88 -89
-101 -100
 106  4 11   0.00   0.00          -99 -100 -109 -108      106  4 11   0.00   0.00          -100 -
101 -110 -109
 106  4 11   0.00   0.00          -108 -109 -127 -124     106  4 11   0.00   0.00          -109 -
110 -128 -127
 106  4 11   0.00   0.00          -84 -85 -99 -98         106  4 11   0.00   0.00          -97 -98
-107 -106
 106  4 11   0.00   0.00          -98 -99 -108 -107       106  4 11   0.00   0.00          -106 -
107 -123 -120
 106  4 11   0.00   0.00          -143 -144 -158 -155     106  4 11   0.00   0.00          -135 -
136 -145 -144
 106  4 11   0.00   0.00          -134 -135 -144 -143     106  4 11   0.00   0.00          -119 -
120 -136 -135
 106  4 11   0.00   0.00          -146 -147 -163 -162     106  4 11   0.00   0.00          -145 -
```

146 -162 -159
 106 4 11   0.00   0.00   -137 -138 -147 -146   106 4 11   0.00   0.00   -136 -
137 -146 -145
 106 4 11   0.00   0.00   -123 -124 -138 -137   106 4 11   0.00   0.00   -115 -
116 -134 -133
 106 4 11   0.00   0.00   -144 -145 -159 -158   106 4 11   0.00   0.00   -1 -11 -
55 -54
 106 4 11   0.00   0.00   -141 -142 -154 -150   106 4 11   0.00   0.00   -133 -
134 -143 -142
 106 4 11   0.00   0.00   -132 -133 -142 -141   106 4 11   0.00   0.00   -142 -
143 -155 -154
 107 6 33 12.50 12.50   -50 -91 -90 3   107 6 33 12.50 12.50   4 -92 -
91 -50
 107 6 33 12.50 12.50   -130 -169 -168 -129   107 6 33 12.50 12.50   -91 -130
-129 -90
 107 6 33 12.50 12.50   -92 -131 -130 -91   107 6 33 12.50 12.50   -169 -
208 -207 -168
 107 6 33 12.50 12.50   -208 -248 -247 -207   107 6 33 12.50 12.50   -209 -
249 -248 -208
 107 6 33 12.50 12.50   -131 -170 -169 -130   107 6 33 12.50 12.50   -170 -
209 -208 -169
 108 6 33 13.50 13.50   -118 -79 -75 -114   108 6 33 13.50 13.50   -79 -18
2 -75
 108 6 33 13.50 13.50   -122 -83 -79 -118   108 6 33 13.50 13.50   -249 -
209 -204 -244
 108 6 33 13.50 13.50   -83 -28 -18 -79   108 6 33 13.50 13.50   -87 -38
-28 -83
 108 6 33 13.50 13.50   -126 -87 -83 -122   108 6 33 13.50 13.50   -165 -
126 -122 -161
 108 6 33 13.50 13.50   -157 -118 -114 -153   108 6 33 13.50 13.50   -196 -
157 -153 -192
 108 6 33 13.50 13.50   -236 -196 -192 -231   108 6 33 13.50 13.50   -131 -92
-87 -126
 108 6 33 13.50 13.50   -170 -131 -126 -165   108 6 33 13.50 13.50   -161 -
122 -118 -157
 108 6 33 13.50 13.50   -200 -161 -157 -196   108 6 33 13.50 13.50   -240 -
200 -196 -236
 108 6 33 13.50 13.50   -92 4 -38 -87   108 6 33 13.50 13.50   -204 -
165 -161 -200
 108 6 33 13.50 13.50   -244 -204 -200 -240   108 6 33 13.50 13.50   -209 -
170 -165 -204
 109 6 11 -13.50 -13.50   -37 -86 -90 3   109 6 11 -13.50 -13.50   -86 -125
-129 -90
 109 6 11 -13.50 -13.50   -199 -239 -243 -203   109 6 11 -13.50 -13.50   -195 -
235 -239 -199
 109 6 11 -13.50 -13.50   -27 -82 -86 -37   109 6 11 -13.50 -13.50   -203 -
243 -247 -207
 109 6 11 -13.50 -13.50   -164 -203 -207 -168   109 6 11 -13.50 -13.50   -125 -
164 -168 -129
 109 6 11 -13.50 -13.50   -190 -229 -235 -195   109 6 11 -13.50 -13.50   -151 -
190 -195 -156
 109 6 11 -13.50 -13.50   -160 -199 -203 -164   109 6 11 -13.50 -13.50   -121 -
160 -164 -125
 109 6 11 -13.50 -13.50   -82 -121 -125 -86   109 6 11 -13.50 -13.50   1 -73 -
78 -17
 109 6 11 -13.50 -13.50   -117 -156 -160 -121   109 6 11 -13.50 -13.50   -156 -
195 -199 -160
 109 6 11 -13.50 -13.50   -17 -78 -82 -27   109 6 11 -13.50 -13.50   -78 -117
-121 -82
 109 6 11 -13.50 -13.50   -73 -112 -117 -78   109 6 11 -13.50 -13.50   -112 -
151 -156 -117
 110 6 11 -12.50 -12.50   2 -75 -74 -5   110 6 11 -12.50 -12.50   -114 -
153 -152 -113
 110 6 11 -12.50 -12.50   -75 -114 -113 -74   110 6 11 -12.50 -12.50   -191 -
230 -229 -190
 110 6 11 -12.50 -12.50   -152 -191 -190 -151   110 6 11 -12.50 -12.50   -113 -
152 -151 -112
 110 6 11 -12.50 -12.50   -74 -113 -112 -73   110 6 11 -12.50 -12.50   -5 -74 -
73 1
 110 6 11 -12.50 -12.50   -192 -231 -230 -191   110 6 11 -12.50 -12.50   -153 -
192 -191 -152

ELENCO TIPI PLINTI/PALI

Simbologia

Tl = Numero del tipo plinto/palo
Tipo = Tipologia
Gra = Gradoni
Pir = Piramidale
P = Palo
T3 = Triangolare 3 pali
T3B = Triangolare 3 pali + bicchiere
R = Rettangolare
RB = Rettangolare + bicchiere
R1 = Rettangolare 1 palo
R1B = Rettangolare 1 palo + bicchiere
R2x = Rettangolare 2 pali dir. X
R2xB = Rettangolare 2 pali dir. X + bicchiere
R2y = Rettangolare 2 pali dir. Y
R2B = Rettangolare 2 pali dir. Y + bicchiere
R4 = Rettangolare 4 pali
R4B = Rettangolare 4 pali + bicchiere
P5 = Pentagonale 5 pali
P5B = Pentagonale 5 pali + bicchiere
E6 = Esagonale 6 pali
E6B = Esagonale 6 pali + bicchiere
Tp = Tipo palo
ND = Non definito
BP = Battuto prefabbricato
BGO = Battuto gettato in opera
T = Trivellato
TEC = Trivellato con elica continua
MP = Micropalo
Comm. = Commento
A1 = Prima dimensione plinto/palo in dir. X
A2 = Seconda dimensione plinto/palo in dir. X
A3 = Terza dimensione plinto/palo in dir. X
B1 = Prima dimensione plinto/palo in dir. Y
B2 = Seconda dimensione plinto/palo in dir. Y
B3 = Terza dimensione plinto/palo in dir. Y
H1 = Altezza parte inferiore plinto/palo
H2 = Altezza parte superiore plinto/palo
c1 = Allargamento magrone in dir. X
c2 = Allargamento magrone in dir. Y
h = Altezza magrone
Crit. = Numero del criterio di progetto

Tl	Tipo	Tp	Comm.	A1 <m>	A2 <m>	A3 <m>	B1 <m>	B2 <m>	B3 <m>	H1 <m>	H2 <m>	c1 <m>	c2 <m>	h <m>	Crit.
1	Gra	--		1.50	0.80	1.50	1.50	0.80	1.50	0.70	1.00	0.15	0.15	0.15	1

ELENCO PLINTI/PALI

Simbologia

PL = Plinto/Palo
Tl = Numero del tipo plinto/palo
Nodo = Nodo plinto/palo
Kt = Coeff. di sottofondo su suolo elastico alla Winkler

PL	Tl	Nodo	Kt <daN/cmc>	PL	Tl	Nodo	Kt <daN/cmc>	PL	Tl	Nodo	Kt <daN/cmc>	PL	Tl	Nodo	Kt <daN/cmc>
1	1	1	0.44	2	1	2	0.44	3	1	3	0.44	4	1	4	0.44

ELENCO TIPI SOLAI

Simbologia

```
Ts        = Numero del tipo solaio
Comm.     = Commento
Rc        = Ripartizione carichi
            UN = Unidirezionale
            PP = A piastra perimetrale
            PB = A piastra bisettrice
Qps       = Carico permanente strutturale
Qpn       = Carico permanente non strutturale
QA        = Primo carico accidentale
QA2       = Secondo carico accidentale
QA3       = Terzo carico accidentale
Rip. ter. = Ripartizione su aste terminali
Rip. int. = Ripartizione su aste interne
Lfl       = Larghezza fascia laterale
Zcv       = Quota di riferimento del piano di campagna
s         = Coeff. di riduzione
```

Ts	Comm.	Rc	Qps	Qpn	QA	QA2	QA3	Rip. ter.	Rip. int.	Lfl	Zcv	s
			<daN/mq>	<daN/mq>	<daN/mq>	<daN/mq>	<daN/mq>			<m>	<m>	
10	PASSERELLA SPIROL 35	UN	400.00	80.00	400.00	80.00	0.00	50.00	50.00	0.00	0.00	1.00

ELENCO SOLAI

Simbologia

```
Sol. = Numero del solaio
Ts   = Numero del tipo solaio
Ord. = Orditura
Nodi = Nodi del solaio
```

Sol.	Ts	Ord. <grad>	Nodi
100	10	0.00	-249 -244 -240 -236 -231 -232 101
300	10	0.00	-228 -233 -234 -237 -238 -241 -242 -245 -246 -247 -243 -239 -235 -229

ELENCO TIPI RETICOLARI

Simbologia

```
Tr    = Numero del tipo reticolare
Tipo  = Tipologia
Comm. = Commento
Crit. = Numero del criterio di progetto
```

Tr	Tipo	Comm.	Crit.
1	Saldata	TRALICCIO	7

ELENCO TIPI TAMPONATURE

Simbologia

```
Tt    = Numero del tipo tamponatura
Comm. = Commento
Qpn   = Carico permanente non strutturale
Rcg   = Ripartizione carichi gravitazionali
        AP = Sull'asta di piede
        AL = Sulle aste laterali
        APT = Sulle aste di piede e di testa
Rcv   = Ripartizione carichi vento
        AP = Sull'asta di piede
```

AL = Sulle aste laterali
APT = Sulle aste di piede e di testa
PP = A piastra perimetrale
PB = A piastra bisettrice
Zcv = Quota di riferimento del piano di campagna
P = Puntoni equivalenti
S = Genera i puntoni equivalenti
N = Non genera i puntoni equivalenti
Tipo = Tipologia
C = Area di carico
V = Area di carico e verifica
Crit. = Criterio di progetto

Tt	Comm.	Qpn <daN/mq>	Rcg	Rcv	Zcv <m>	P	Tipo	Crit.
1	TAMPONATURA CW	150.00	AP	AL	0.00	N	C	--

CONDIZIONI DI CARICO ELEMENTARI:

Simbologia

CCE = Numero della condizione di carico elementare
Comm. = Commento
Tipo CCE = Tipo di CCE per calcolo agli stati limite
Sic. = Contributo alla sicurezza
F = a favore
S = a sfavore
A = ambigua
Var. = Tipo di variabilità
B = di base
I = indipendente
A = ambigua
Dir. = Direzione del vento
Tipo = Tipologia di pressione vento
M = Massimizzata
E = Esterna
I = Interna
Mx = Moltiplicatore della massa in dir. X
My = Moltiplicatore della massa in dir. Y
Mz = Moltiplicatore della massa in dir. Z
Jpx = Moltiplicatore del momento d'inerzia intorno all'asse X
Jpy = Moltiplicatore del momento d'inerzia intorno all'asse Y
Jpz = Moltiplicatore del momento d'inerzia intorno all'asse Z

Condizioni di carico elementari

CCE	Comm.	Tipo CCE	Sic.	Var.	Dir.	Tipo	Mx	My	Mz	Jpx	Jpy	Jpz
<grad>												
1	PERMANENTI ST	1 D.M. 08 Permanenti strutturali	S	--	--	--	1.00	1.00	0.00	0.00	0.00	1.00
2	PERMANENTI NST	2 D.M. 08 Permanenti non strutturali	S	--	--	--	1.00	1.00	0.00	0.00	0.00	1.00
3	ACCIDENTALI	5 D.M. 08 Variabili Categoria C Ambienti suscettibili di affollamento	S	B	--	--	1.00	1.00	0.00	0.00	0.00	1.00
4	VENTO	10 D.M. 08 Variabili Vento	S	B	--	--	1.00	1.00	0.00	0.00	0.00	1.00
5	NEVE	11 D.M. 08 Variabili Neve (a quota <= 1000 m s.l.m.)	S	B	--	--	1.00	1.00	0.00	0.00	0.00	1.00
6	VENTO Y	10 D.M. 08 Variabili Vento	S	B	--	--	1.00	1.00	0.00	0.00	0.00	1.00

ELENCO CARICHI ASTE

CONDIZIONE DI CARICO 1: PERMANENTI ST

ELENCO PESO PROPRIO ASTE

Simbologia

Sez. = Numero della sezione
Comm. = Commento
A   = Area
Mat. = Materiale
P   = Peso specifico
PL   = Peso specifico a metro lineare

Sez.	Comm.	A <cmq>	Mat.	P <daN/mc>	PL <daN/m>	Sez.	Comm.	A <cmq>	Mat.	P <daN/mc>	PL <daN/m>
1	P40X40	1600.000000	Calcestruzzo	2500.00	400.00	15	L100x10	19.154600	Acciaio	7850.00	15.04
17	L120x10	23.181400	Acciaio	7850.00	18.20	19	L80x7	10.924700	Acciaio	7850.00	8.58
20		10.924700	Acciaio	7850.00	8.58						

ELENCO CARICHI ASTE

CONDIZIONE DI CARICO 1: PERMANENTI ST

CARICHI DISTRIBUITI

Simbologia

Asta = Numero dell'asta
N1   = Nodo iniziale
N2   = Nodo finale
E   = Elemento provenienza del carico
       S = Solaio
       T = Tamponatura
NE   = Numero elemento di provenienza del carico
T   = Tipo di carico
       QA = Primo carico accidentale
       QA2 = Secondo carico accidentale
       QA3 = Terzo carico accidentale
       QPS = Carico permanente strutturale
       QPN = Carico permanente non strutturale
       VE = Vento
       M = Manuale
DC   = Direzione del carico
       XG,YG,ZG = secondo gli assi globali
       XL,YL,ZL = secondo gli assi locali
Xi   = Distanza iniziale
Qi   = Carico iniziale
Xf   = Distanza finale
Qf   = Carico finale

Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>	Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>
0	-228	-233	S	300	QPS	ZG	0.00	1260.00	0.34	1260.00	0	-233	-234	S	300	QPS	ZG	0.00	1260.00	0.34	1260.00
0	-234	-237	S	300	QPS	ZG	0.00	1260.00	0.34	1260.00	0	-237	-238	S	300	QPS	ZG	0.00	1260.00	0.34	1260.00
0	-238	-241	S	300	QPS	ZG	0.00	1260.00	0.34	1260.00	0	-241	-242	S	300	QPS	ZG	0.00	1260.00	0.34	1260.00
0	-242	-245	S	300	QPS	ZG	0.00	1260.00	0.34	1260.00	0	-245	-246	S	300	QPS	ZG	0.00	1260.00	0.34	1260.00
0	-235	-229	S	300	QPS	ZG	0.00	1260.00	0.68	1260.00	0	-239	-235	S	300	QPS	ZG	0.00	1260.00	0.68	1260.00
0	-243	-239	S	300	QPS	ZG	0.00	1260.00	0.68	1260.00	0	-236	-231	S	100	QPS	ZG	0.00	1326.00	0.68	1326.00
0	-247	-243	S	300	QPS	ZG	0.00	1260.00	0.68	1260.00	0	-240	-236	S	100	QPS	ZG	0.00	1326.00	0.68	

1326.00
   0 -244 -240 S 100 QPS ZG 0.00 1326.00 0.68 1326.00   0 -249 -244 S 100 QPS ZG 0.00 1326.00 0.68
1326.00
   0 -232 101 S 100 QPS ZG 0.00 1326.00 2.70 1326.00

ELENCO CARICHI ASTE

CONDIZIONE DI CARICO 2: PERMANENTI NST

CARICHI DISTRIBUITI

Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>	Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>
0	-228	-233	S	300	QPN	ZG	0.00	252.00	0.34	252.00	0	-233	-234	S	300	QPN	ZG	0.00	252.00	0.34	252.00
0	-234	-237	S	300	QPN	ZG	0.00	252.00	0.34	252.00	0	-237	-238	S	300	QPN	ZG	0.00	252.00	0.34	252.00
0	-238	-241	S	300	QPN	ZG	0.00	252.00	0.34	252.00	0	-241	-242	S	300	QPN	ZG	0.00	252.00	0.34	252.00
0	-242	-245	S	300	QPN	ZG	0.00	252.00	0.34	252.00	0	-245	-246	S	300	QPN	ZG	0.00	252.00	0.34	252.00
0	-235	-229	S	300	QPN	ZG	0.00	252.00	0.68	252.00	0	-239	-235	S	300	QPN	ZG	0.00	252.00	0.68	252.00
0	-243	-239	S	300	QPN	ZG	0.00	252.00	0.68	252.00	0	-236	-231	S	100	QPN	ZG	0.00	265.20	0.68	265.20
0	-247	-243	S	300	QPN	ZG	0.00	252.00	0.68	252.00	0	-240	-236	S	100	QPN	ZG	0.00	265.20	0.68	265.20
0	-244	-240	S	100	QPN	ZG	0.00	265.20	0.68	265.20	0	-249	-244	S	100	QPN	ZG	0.00	265.20	0.68	265.20
0	-232	101	S	100	QPN	ZG	0.00	265.20	2.70	265.20	337	-229	-250	S	--	M	ZG	0.00	40.00	1.81	40.00
337	-250	-254	S	--	M	ZG	0.00	40.00	1.81	40.00	337	-254	-259	S	--	M	ZG	0.00	40.00	1.81	40.00
337	-259	-263	S	--	M	ZG	0.00	40.00	1.81	40.00	337	-263	-267	S	--	M	ZG	0.00	40.00	1.81	40.00
337	-267	-272	S	--	M	ZG	0.00	40.00	1.81	40.00	337	-272	-276	S	--	M	ZG	0.00	40.00	1.81	40.00
337	-276	-280	S	--	M	ZG	0.00	40.00	1.81	40.00	338	-231	-251	S	--	M	ZG	0.00	40.00	1.81	40.00
338	-251	-255	S	--	M	ZG	0.00	40.00	1.81	40.00	338	-255	-260	S	--	M	ZG	0.00	40.00	1.81	40.00
338	-260	-264	S	--	M	ZG	0.00	40.00	1.81	40.00	338	-264	-268	S	--	M	ZG	0.00	40.00	1.81	40.00
338	-268	-273	S	--	M	ZG	0.00	40.00	1.81	40.00	338	-273	-277	S	--	M	ZG	0.00	40.00	1.81	40.00
338	-277	-281	S	--	M	ZG	0.00	40.00	1.81	40.00	369	-253	-249	S	--	M	ZG	0.00	40.00	1.81	40.00
369	-258	-253	S	--	M	ZG	0.00	40.00	1.81	40.00	369	-262	-258	S	--	M	ZG	0.00	40.00	1.81	40.00
369	-266	-262	S	--	M	ZG	0.00	40.00	1.81	40.00	369	-271	-266	S	--	M	ZG	0.00	40.00	1.81	40.00
369	-275	-271	S	--	M	ZG	0.00	40.00	1.81	40.00	369	-279	-275	S	--	M	ZG	0.00	40.00	1.81	40.00
369	-284	-279	S	--	M	ZG	0.00	40.00	1.81	40.00	370	-247	-252	S	--	M	ZG	0.00	40.00	1.81	40.00
370	-252	-257	S	--	M	ZG	0.00	40.00	1.81	40.00	370	-257	-261	S	--	M	ZG	0.00	40.00	1.81	40.00
370	-261	-265	S	--	M	ZG	0.00	40.00	1.81	40.00	370	-265	-270	S	--	M	ZG	0.00	40.00	1.81	40.00
370	-270	-274	S	--	M	ZG	0.00	40.00	1.81	40.00	370	-274	-278	S	--	M	ZG	0.00	40.00	1.81	40.00
370	-278	-283	S	--	M	ZG	0.00	40.00	1.81	40.00											

ELENCO CARICHI ASTE

CONDIZIONE DI CARICO 3: ACCIDENTALI

CARICHI DISTRIBUITI

Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>	Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>
0	-228	-233	S	300	QA	ZG	0.00	1260.00	0.34	1260.00	0	-233	-234	S	300	QA	ZG	0.00	1260.00	0.34	1260.00
0	-234	-237	S	300	QA	ZG	0.00	1260.00	0.34	1260.00	0	-237	-238	S	300	QA	ZG	0.00	1260.00	0.34	1260.00
0	-238	-241	S	300	QA	ZG	0.00	1260.00	0.34	1260.00	0	-241	-242	S	300	QA	ZG	0.00	1260.00	0.34	1260.00
0	-242	-245	S	300	QA	ZG	0.00	1260.00	0.34	1260.00	0	-245	-246	S	300	QA	ZG	0.00	1260.00	0.34	1260.00
0	-235	-229	S	300	QA	ZG	0.00	1260.00	0.68	1260.00	0	-239	-235	S	300	QA	ZG	0.00	1260.00	0.68	1260.00
0	-243	-239	S	300	QA	ZG	0.00	1260.00	0.68	1260.00	0	-236	-231	S	100	QA	ZG	0.00	1326.00	0.68	1326.00
0	-247	-243	S	300	QA	ZG	0.00	1260.00	0.68	1260.00	0	-240	-236	S	100	QA	ZG	0.00	1326.00	0.68	1326.00
0	-244	-240	S	100	QA	ZG	0.00	1326.00	0.68	1326.00	0	-249	-244	S	100	QA	ZG	0.00	1326.00	0.68	1326.00
0	-232	101	S	100	QA	ZG	0.00	1326.00	2.70	1326.00											

ELENCO CARICHI ASTE

CONDIZIONE DI CARICO 4: VENTO

CARICHI DISTRIBUITI

Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>	Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>
337	-229	-250	S	--	M	XG	0.00	-340.00	1.81	-340.00	337	-250	-254	S	--	M	XG	0.00	-340.00	1.81	-340.00
337	-254	-259	S	--	M	XG	0.00	-340.00	1.81	-340.00	337	-259	-263	S	--	M	XG	0.00	-340.00	1.81	-340.00
337	-263	-267	S	--	M	XG	0.00	-340.00	1.81	-340.00	337	-267	-272	S	--	M	XG	0.00	-340.00	1.81	-340.00
337	-272	-276	S	--	M	XG	0.00	-340.00	1.81	-340.00	337	-276	-280	S	--	M	XG	0.00	-340.00	1.81	-340.00
370	-247	-252	S	--	M	XG	0.00	-340.00	1.81	-340.00	370	-252	-257	S	--	M	XG	0.00	-340.00	1.81	-340.00
370	-257	-261	S	--	M	XG	0.00	-340.00	1.81	-340.00	370	-261	-265	S	--	M	XG	0.00	-340.00	1.81	-340.00
370	-265	-270	S	--	M	XG	0.00	-340.00	1.81	-340.00	370	-270	-274	S	--	M	XG	0.00	-340.00	1.81	-340.00
370	-274	-278	S	--	M	XG	0.00	-340.00	1.81	-340.00	370	-278	-283	S	--	M	XG	0.00	-340.00	1.81	-340.00

ELENCO CARICHI ASTE

CONDIZIONE DI CARICO 5: NEVE

CARICHI DISTRIBUITI

Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>	Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>
0	-228	-233	S	300	QA2	ZG	0.00	252.00	0.34	252.00	0	-233	-234	S	300	QA2	ZG	0.00	252.00	0.34	252.00
0	-234	-237	S	300	QA2	ZG	0.00	252.00	0.34	252.00	0	-237	-238	S	300	QA2	ZG	0.00	252.00	0.34	252.00
0	-238	-241	S	300	QA2	ZG	0.00	252.00	0.34	252.00	0	-241	-242	S	300	QA2	ZG	0.00	252.00	0.34	252.00
0	-242	-245	S	300	QA2	ZG	0.00	252.00	0.34	252.00	0	-245	-246	S	300	QA2	ZG	0.00	252.00	0.34	252.00
0	-235	-229	S	300	QA2	ZG	0.00	252.00	0.68	252.00	0	-239	-235	S	300	QA2	ZG	0.00	252.00	0.68	252.00
0	-243	-239	S	300	QA2	ZG	0.00	252.00	0.68	252.00	0	-236	-231	S	100	QA2	ZG	0.00	265.20	0.68	265.20
0	-247	-243	S	300	QA2	ZG	0.00	252.00	0.68	252.00	0	-240	-236	S	100	QA2	ZG	0.00	265.20	0.68	265.20
0	-244	-240	S	100	QA2	ZG	0.00	265.20	0.68	265.20	0	-249	-244	S	100	QA2	ZG	0.00	265.20	0.68	265.20
0	-232	101	S	100	QA2	ZG	0.00	265.20	2.70	265.20											

ELENCO CARICHI ASTE

CONDIZIONE DI CARICO 6: VENTO Y

CARICHI DISTRIBUITI

Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>
369	-253	-249	S	--	M	YG	0.00	230.00	1.81	230.00
369	-262	-258	S	--	M	YG	0.00	230.00	1.81	230.00
369	-271	-266	S	--	M	YG	0.00	230.00	1.81	230.00
369	-279	-275	S	--	M	YG	0.00	230.00	1.81	230.00
370	-247	-252	S	--	M	YG	0.00	230.00	1.81	230.00
370	-257	-261	S	--	M	YG	0.00	230.00	1.81	230.00
370	-265	-270	S	--	M	YG	0.00	230.00	1.81	230.00
370	-274	-278	S	--	M	YG	0.00	230.00	1.81	230.00
369	-258	-253	S	--	M	YG	0.00	230.00	1.81	230.00
369	-266	-262	S	--	M	YG	0.00	230.00	1.81	230.00
369	-275	-271	S	--	M	YG	0.00	230.00	1.81	230.00
369	-284	-279	S	--	M	YG	0.00	230.00	1.81	230.00
370	-252	-257	S	--	M	YG	0.00	230.00	1.81	230.00
370	-261	-265	S	--	M	YG	0.00	230.00	1.81	230.00
370	-270	-274	S	--	M	YG	0.00	230.00	1.81	230.00
370	-278	-283	S	--	M	YG	0.00	230.00	1.81	230.00

ELENCO PESO PROPRIO BIDIMENSIONALI

Simbologia

Tb = Numero del tipo muro/elemento bidimensionale
Comm. = Commento
Spess. = Spessore
Mat. = Materiale
P = Peso specifico
PQ = Peso specifico per unità di superficie

Tb	Comm.	Spess. <cm>	Mat.	P <daN/mc>	PQ <daN/mq>
4	SETTO 30	30.00	Calcestruzzo	2500.00	750.00
6	SETTO 20	20.00	Calcestruzzo	2500.00	500.00

Analisi dei carichi da vento

VENTO LATO MLCalcolo delle azioni del vento

Normativa di riferimento:
Norme tecniche per le costruzioni D.M. 14 gennaio 2008 e Circolare 2 febbraio 2009, n. 617 del Ministero delle Infrastrutture e dei Trasporti

Area di ubicazione dell'edificio: Area 3
Toscana, Marche, Umbria, Lazio, Abruzzo, Molise, Puglia, Campania, Basilicata, Calabria(esclusa la Provincia di Reggio Calabria)

Tempo di ritorno 50 <anni>

Altitudine sul livello del mare: 60 <m>

Altezza dell'edificio: 18 <m>

Parametri derivati dall'area di ubicazione (tab. 3.3.I):
Vb,0 (Velocità media del vento): 27 <m/sec>
a0 (Altitudine media): 500 <m>
Ka: 0.020 <1/sec>

Velocità di riferimento: 27.00 <m/sec>

Classificazione della costruzione: Pianta rettangolare con coperture piane, a falde, inclinate o curve

Categoria di esposizione del sito: IV

Parametri derivati dalla categoria di esposizione del sito (tab. 3.3.II):
kr: 0.22 <m>
z0: 0.30 <m>
zmin: 8 <m>

Classe di rugosità del terreno: A
Aree urbane in cui almeno il 15% della superficie sia coperto

da edifici la cui altezza media superi i 15 m

Angolo alfa: 53.0 <grad>

Pressione del vento = qb*ce*cp*cd
qb (Pressione cinetica di riferimento): 45.56 <daN/mq>
ct (Coefficiente topografico): 1.00
ce (Coefficiente di esposizione): 2.20
cd (Coefficiente dinamico): 1.00

Tipologia di superficie:
Una parete con aperture di superficie minore di 1/3 di quella totale

Coefficiente di forma o aerodinamico interno cpi: 0.20
Coefficienti di forma o aerodinamici esterni cpe:
sopravento: 0.80 sopravento su falda: 0.59 sottovento su falda: -0.40 sottovento: -0.40

Pressione interna: 20.03 <daN/mq>
Pressioni esterne:
sopravento: 80.14 <daN/mq> sopravento su falda: 59.10 <daN/mq> sottovento su falda: -40.07 <daN/mq>
sottovento: -40.07 <daN/mq>

VENTO TOTEMCalcolo delle azioni del vento

Normativa di riferimento:
Norme tecniche per le costruzioni D.M. 14 gennaio 2008 e Circolare 2 febbraio
2009, n. 617 del Ministero delle Infrastrutture e dei Trasporti

Area di ubicazione dell'edificio: Area 3
Toscana, Marche, Umbria, Lazio, Abruzzo, Molise, Puglia, Campania, Basilicata, Calabria(esclusa la Provincia di Reggio Calabria)

Tempo di ritorno 50 <anni>

Altitudine sul livello del mare: 60 <m>

Altezza dell'edificio: 18 <m>

Parametri derivati dall'area di ubicazione (tab. 3.3.I):
Vb,0 (Velocità media del vento): 27 <m/sec>
a0 (Altitudine media): 500 <m>
Ka: 0.020 <1/sec>

Velocità di riferimento: 27.00 <m/sec>

Classificazione della costruzione: Torri e pali a traliccio

Categoria di esposizione del sito: IV

Parametri derivati dalla categoria di esposizione del sito (tab. 3.3.II):
kr: 0.22 <m>
z0: 0.30 <m>
zmin: 8 <m>

Classe di rugosità del terreno: A
Aree urbane in cui almeno il 15% della superficie sia coperto
da edifici la cui altezza media superi i 15 m

Pressione del vento = qb*ce*cp*cd
qb (Pressione cinetica di riferimento): 45.56 <daN/mq>
ct (Coefficiente topografico): 1.00
ce (Coefficiente di esposizione): 2.20
cd (Coefficiente dinamico): 1.00

Tipologia di superficie:
Elementi a sezione di forma diversa dalla circolare

Coefficiente di forma (o aerodinamico)cp:
cp: 2.80

Pressione totale <daN/mq>:
pressione: 280.48 <daN/mq>

Nome dell'analisi dei carichi da neve

NEVECalcolo delle azioni della neve

Normativa di riferimento:
Norme tecniche per le costruzioni D.M. 14 gennaio 2008 e Circolare 2 febbraio 2009, n. 617 del Ministero delle Infrastrutture e dei Trasporti

Area di ubicazione dell'edificio: Area 2
Arezzo, Ascoli Piceno, Bari, Campobasso, Chieti, Ferrara, Firenze, Foggia, Genova, Gorizia, Imperia, Isernia, La Spezia, Lucca, Macerata, Mantova, Massa Carrara, Padova, Perugia, Pescara, Pistoia, Prato, Rovigo, Savona, Teramo, Trieste, Venezia, Verona

Altitudine sul livello del mare: 60 <m>

Tipologia di copertura: A due falde

Pressione della neve ps = μ1*qsk*Ce*Ct

Parametri d'input ed intermedi:
Categoria del coefficiente d'esposizione: Normale
Ce (Coefficiente d'esposizione): 1.0
Ct (Coefficiente termico): 1.0
Angolo sinistro di inclinazione della falda : 53.0 <grad>
Angolo destro di inclinazione della falda : 24.0 <grad>
μ1(alfa1) (Coefficiente di forma della copertura): 0.19
μ1(alfa2) (Coefficiente di forma della copertura): 0.80

Carichi agenti:
qsk (Valore di riferimento del carico neve al suolo): 100.00 <daN/mq>
qss (Carico sinistro provocato dalla neve sulle coperture): 18.67 <daN/mq>
qsd (Carico destro provocato dalla neve sulle coperture): 80.00 <daN/mq>

PARAMETRI DI CALCOLO
La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con:
ModeSt ver. 8.14, prodotto da Tecnisoft s.a.s. - Prato

La struttura è stata calcolata utilizzando come solutore agli elementi finiti:
Xfinest ver. 2014, prodotto da Ce.A.S. S.r.l. - Milano

Tipo di normativa: stati limite D.M. 08
Tipo di calcolo: analisi sismica dinamica
Vincoli esterni: Considera sempre vincoli assegnati in modellazione
Schematizzazione piani rigidi: nessun impalcato rigido
Modalità di recupero masse secondarie: mantenere sul nodo masse e forze relative

Generazione combinazioni
- Lineari: Sì
- Valuta spostamenti e non sollecitazioni: No
- buckling: No

Opzioni di calcolo
- Sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali con una riduzione del 20%
- Calcolo con offset rigidi dai nodi: No
- Uniformare i carichi variabili: No
- Massimizzare i carichi variabili: No
- Minimo carico da considerare: 0.00 <daN/m>
- Recupero carichi zone rigide: taglio e momento flettente
- Modalità di combinazione momento torcente: disaccoppiare le azioni

Opzioni del solutore
- Tipo di elemento bidimensionale: QF46
- Calcolo sforzo nei nodi: No
- Trascura deformabilità a taglio delle aste: No
- Analisi dinamica con metodo di Lanczos: Sì
- Check sequenza di Sturm: Sì

- Soluzione matrice con metodo ver. 5.1: No
- Analisi non lineare con Newton modificato: No
- Usa formulazione secante per buckling: No
- Trascura buckling torsionale: No

Dati struttura
- Zona sismica: zona 2
- Sito di costruzione: PRATO LON. 11.10220 LAT. 43.87770
  Contenuto tra ID reticolo: 19613 19612 19391 19390

Simbologia

TCC = Tipo di combinazione di carico
      SLU = Stato limite ultimo
      SLU S = Stato limite ultimo (azione sismica)
      SLE R = Stato limite d'esercizio, combinazione rara
      SLE F = Stato limite d'esercizio, combinazione frequente
      SLE Q = Stato limite d'esercizio, combinazione quasi permanente
      SLD = Stato limite di danno
      SLV = Stato limite di salvaguardia della vita
      SLC = Stato limite di prevenzione del collasso
      SLO = Stato limite di operatività
      SLU I = Stato limite di resistenza al fuoco
T_R = Periodo di ritorno <anni>
Ag = Accelerazione orizzontale massima al sito
FO = Valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale
TC* = Periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale <sec>
S_S = Coefficiente di amplificazione stratigrafica
C_C = Coefficiente funzione della categoria del suolo

TCC	T_R	Ag <g>	FO	TC*	S_S	C_C
SLD	50	0.0605	2.55	0.27	1.20	1.43
SLV	475	0.1421	2.43	0.30	1.20	1.40

- Edificio esistente: No
- Tipo di opera: Opera ordinaria
- Vita nominale V_N: 50.00
- Classe d'uso: Classe II
- SL Esercizio: SLO-Pvr No, SLD-Pvr 63.00
- SL Ultimi: SLV-Pvr 10.00, SLC-Pvr No
- Classe di duttilità: Classe B
- Quota di riferimento: 0.00 <m>
- Altezza della struttura: 19.50 <m>
- Numero piani edificio: 0
- Coefficiente θ: 0.00
- Edificio regolare in altezza: Sì
- Edificio regolare in pianta: Sì
- Forze orizzontali convenzionali per stati limite non sismici: 1.00%
- Genera stati limite per verifiche di resistenza al fuoco: No

Dati di calcolo
- Categoria del suolo di fondazione: B
- Tipologia edificio: c.a. o prefabbricato a telaio a più piani e più campate
Coeff. C_1: 0.075
Periodo T_1: 0.69596
Coeff. λ SLD: 1.00
Coeff. λ SLV: 1.00
Rapporto di sovraresistenza (α_u/α_1): 1.30
Valore di riferimento del fattore di struttura (q_0): 3.90
Fattore riduttivo (K_w): 1.00
Fattore riduttivo regolarità in altezza (KR): 1.00
Fattore di struttura (q): 1.50

- Categoria topografica: T1 - Superficie pianeggiante, pendii e rilievi isolati con inclinazione media i<=15°
- Coeff. amplificazione topografica S_T: 1.00
- Fattore di struttura per sisma verticale (qv): 1.50
- Modalità di calcolo modi di vibrare: Autovalori
- Numero modi: 120
- Modi da considerare: Tali da movimentare una percentuale di massa pari a 85.00%
- Trascura modi con massa movimentata minore di: No
- Smorzamento spettro: 5.00%

- Angolo di ingresso del sisma: 0.00 <grad>

CONDIZIONI DI CARICO ELEMENTARI:

Simbologia

CCE = Numero della condizione di carico elementare
Comm. = Commento
Tipo CCE = Tipo di CCE per calcolo agli stati limite
Sic. = Contributo alla sicurezza
F = a favore
S = a sfavore
A = ambigua
Var. = Tipo di variabilità
B = di base
I = indipendente
A = ambigua
Dir. = Direzione del vento
Tipo = Tipologia di pressione vento
M = Massimizzata
E = Esterna
I = Interna
Mx = Moltiplicatore della massa in dir. X
My = Moltiplicatore della massa in dir. Y
Mz = Moltiplicatore della massa in dir. Z
Jpx = Moltiplicatore del momento d'inerzia intorno all'asse X
Jpy = Moltiplicatore del momento d'inerzia intorno all'asse Y
Jpz = Moltiplicatore del momento d'inerzia intorno all'asse Z

CCE	Comm.	Tipo CCE	Sic.	Var.	Dir. <grad>	Tipo	Mx	My	Mz	Jpx	Jpy	Jpz
1	PERMANENTI ST	1	S	--	--	--	1.00	1.00	0.00	0.00	0.00	1.00
2	PERMANENTI NST	2	S	--	--	--	1.00	1.00	0.00	0.00	0.00	1.00
3	ACCIDENTALI	5	S	B	--	--	1.00	1.00	0.00	0.00	0.00	1.00
4	VENTO	10	S	B	--	--	1.00	1.00	0.00	0.00	0.00	1.00
5	NEVE	11	S	B	--	--	1.00	1.00	0.00	0.00	0.00	1.00
6	VENTO Y	10	S	B	--	--	1.00	1.00	0.00	0.00	0.00	1.00

ELENCO TIPI CCE DEFINITI:

Simbologia

Tipo CCE = Tipo condizione di carico elementare
Comm. = Commento
Tipo = Tipologia
G = Permanente
Qv = Variabile vento
Q = Variabile
I = Da ignorare
A = Azione eccezionale
P = Precompressione
Durata = Durata del carico
N = Non definita
P = Permanente
L = Lunga
M = Media
B = Breve
I = Istantanea
γ min. = Coeff. $\gamma_{min.}$
γ max = Coeff. γ_{max}
ψ_0 = Coeff. ψ_0
ψ_1 = Coeff. ψ_1
ψ_2 = Coeff. ψ_2
$\psi_{0,s}$ = Coeff. ψ_0 sismico (D.M. 96)

Tipo CCE	Comm.	Tipo	Durata	γ min.	γ max	ψ_0	ψ_1	ψ_2	$\psi_{0,s}$

1	D.M. 08 Permanenti strutturali	G	N	1.00	1.30	1.00	1.00	1.00	1.00
2	D.M. 08 Permanenti non strutturali	G	N	0.00	1.50	1.00	1.00	1.00	1.00
5	D.M. 08 Variabili Categoria C Ambienti suscettibili di affollamento	Q	N	0.00	1.50	0.70	0.70	0.60	0.00
10	D.M. 08 Variabili Vento	Q	N	0.00	1.50	0.60	0.20	0.00	0.00
11	D.M. 08 Variabili Neve (a quota <= 1000 m s.l.m.)	Q	N	0.00	1.50	0.50	0.20	0.00	0.00

AMBIENTI DI CARICO:

Simbologia

N = Numero
Comm. = Commento
1 = PERMANENTI ST
2 = PERMANENTI NST
3 = ACCIDENTALI
4 = VENTO
5 = NEVE
6 = VENTO Y
F = azioni orizzontali convenzionali
SLU = Stato limite ultimo
SLR = Stato limite per combinazioni rare
SLF = Stato limite per combinazioni frequenti
SLQ/D = Stato limite per combinazioni quasi permanenti o di danno
S = Sì
N = No

N	Comm.	1	2	3	4	5	6	F	S	SLU	SLR	SLF	SLQ
1	STATICO VENTO Y	S	S	S	N	S	S	N	S	S	S	S	S
2	Calcolo sismico	S	S	S	N	N	N	S	S	S	N	N	N
3	STATICO VENTO X	S	S	S	S	S	N	S	N	S	S	S	S

ELENCO COMBINAZIONI DI CARICO SIMBOLICHE:

Simbologia

CC = Numero della combinazione delle condizioni di carico elementari
Comm. = Commento
TCC = Tipo di combinazione di carico
SLU = Stato limite ultimo
SLU S = Stato limite ultimo (azione sismica)
SLE R = Stato limite d'esercizio, combinazione rara
SLE F = Stato limite d'esercizio, combinazione frequente
SLE Q = Stato limite d'esercizio, combinazione quasi permanente
SLD = Stato limite di danno
SLV = Stato limite di salvaguardia della vita
SLC = Stato limite di prevenzione del collasso
SLO = Stato limite di operatività
SLU I = Stato limite di resistenza al fuoco

CC	Comm.	TCC	1	2	3	4	5	6	F	S
1	Amb. 1 (SLU)	SLU	γ max	γ max	γ max	-----	γ max	γ max	1	-----
2	Amb. 1 (SLE R)	SLE R	1	1	1	-----	1	1	1	-----
3	Amb. 1 (SLE F)	SLE F	1	1	ψ_1	-----	ψ_1	ψ_1	1	-----
4	Amb. 1 (SLE Q)	SLE Q	1	1	ψ_2	-----	ψ_2	ψ_2	1	-----
5	Amb. 2 (Sisma)	SLU S	1	1	ψ_2	-----	-----	-----	-----	1
6	Amb. 3 (SLU)	SLU	γ max	γ max	γ max	γ max	γ max	-----	1	-----
7	Amb. 3 (SLE R)	SLE R	1	1	1	1	1	-----	1	-----
8	Amb. 3 (SLE F)	SLE F	1	1	ψ_1	ψ_1	ψ_1	-----	1	-----
9	Amb. 3 (SLE Q)	SLE Q	1	1	ψ_2	ψ_2	ψ_2	-----	1	-----

Genera le combinazioni con un solo carico di tipo variabile come di base: Sì

Considera sollecitazioni dinamiche con segno dei modi principali: Sì

COMBINAZIONI DELLE CCE:

Simbologia

CC = Numero della combinazione delle condizioni di carico elementari
Comm. = Commento
TCC = Tipo di combinazione di carico
  SLU = Stato limite ultimo
  SLU S = Stato limite ultimo (azione sismica)
  SLE R = Stato limite d'esercizio, combinazione rara
  SLE F = Stato limite d'esercizio, combinazione frequente
  SLE Q = Stato limite d'esercizio, combinazione quasi permanente
  SLD = Stato limite di danno
  SLV = Stato limite di salvaguardia della vita
  SLC = Stato limite di prevenzione del collasso
  SLO = Stato limite di operatività
  SLU I = Stato limite di resistenza al fuoco
An. = Tipo di analisi
  L = Lineare
  NL = Non lineare
Bk = buckling
  S = Sì
  N = No

CC	Comm.	TCC	An.	Bk	1	2	3	4	5	6	F X	F Y	S X	S Y
1	CC 1 - Amb. 1 (SLU) F X	SLU	L	N	1.30	1.50	1.50	0.00	1.50	1.50	1.00	0.00	0.00	0.00
2	CC 2 - Amb. 1 (SLU) F -X	SLU	L	N	1.30	1.50	1.50	0.00	1.50	1.50	-1.00	0.00	0.00	0.00
3	CC 3 - Amb. 1 (SLU) F Y	SLU	L	N	1.30	1.50	1.50	0.00	1.50	1.50	0.00	1.00	0.00	0.00
4	CC 4 - Amb. 1 (SLU) F -Y	SLU	L	N	1.30	1.50	1.50	0.00	1.50	1.50	0.00	-1.00	0.00	0.00
5	CC 5 - Amb. 1 (SLE R) F X	SLE R	L	N	1.00	1.00	1.00	0.00	1.00	1.00	1.00	0.00	0.00	0.00
6	CC 6 - Amb. 1 (SLE R) F -X	SLE R	L	N	1.00	1.00	1.00	0.00	1.00	1.00	-1.00	0.00	0.00	0.00
7	CC 7 - Amb. 1 (SLE R) F Y	SLE R	L	N	1.00	1.00	1.00	0.00	1.00	1.00	0.00	1.00	0.00	0.00
8	CC 8 - Amb. 1 (SLE R) F -Y	SLE R	L	N	1.00	1.00	1.00	0.00	1.00	1.00	0.00	-1.00	0.00	0.00
9	CC 9 - Amb. 1 (SLE F) F X	SLE F	L	N	1.00	1.00	0.70	0.00	0.20	0.20	1.00	0.00	0.00	0.00
10	CC 10 - Amb. 1 (SLE F) F -X	SLE F	L	N	1.00	1.00	0.70	0.00	0.20	0.20	-1.00	0.00	0.00	0.00
11	CC 11 - Amb. 1 (SLE F) F Y	SLE F	L	N	1.00	1.00	0.70	0.00	0.20	0.20	0.00	1.00	0.00	0.00
12	CC 12 - Amb. 1 (SLE F) F -Y	SLE F	L	N	1.00	1.00	0.70	0.00	0.20	0.20	0.00	-1.00	0.00	0.00
13	CC 13 - Amb. 1 (SLE Q) F X	SLE Q	L	N	1.00	1.00	0.60	0.00	0.00	0.00	1.00	0.00	0.00	0.00
14	CC 14 - Amb. 1 (SLE Q) F -X	SLE Q	L	N	1.00	1.00	0.60	0.00	0.00	0.00	-1.00	0.00	0.00	0.00
15	CC 15 - Amb. 1 (SLE Q) F Y	SLE Q	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	1.00	0.00	0.00
16	CC 16 - Amb. 1 (SLE Q) F -Y	SLE Q	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	-1.00	0.00	0.00
17	CC 17 - Amb. 2 (SLU S) S +X+0.3Y	SLV	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	1.00	0.30
18	CC 18 - Amb. 2 (SLE) S +X+0.3Y	SLD	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	1.00	0.30
19	CC 19 - Amb. 2 (SLU S) S +X-0.3Y	SLV	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	1.00	-0.30
20	CC 20 - Amb. 2 (SLE) S +X-0.3Y	SLD	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	1.00	-0.30
21	CC 21 - Amb. 2 (SLU S) S -X+0.3Y	SLV	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	-1.00	0.30
22	CC 22 - Amb. 2 (SLE) S -X+0.3Y	SLD	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	-1.00	0.30
23	CC 23 - Amb. 2 (SLU S) S -X-0.3Y	SLV	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	-1.00	-0.30
24	CC 24 - Amb. 2 (SLE) S -X-0.3Y	SLD	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	-1.00	-0.30
25	CC 25 - Amb. 2 (SLU S) S +0.3X+Y	SLV	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	0.30	1.00
26	CC 26 - Amb. 2 (SLE) S +0.3X+Y	SLD	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	0.30	1.00
27	CC 27 - Amb. 2 (SLU S) S -0.3X+Y	SLV	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	-0.30	1.00
28	CC 28 - Amb. 2 (SLE) S -0.3X+Y	SLD	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	-0.30	1.00
29	CC 29 - Amb. 2 (SLU S) S +0.3X-Y	SLV	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	0.30	-1.00
30	CC 30 - Amb. 2 (SLE) S +0.3X-Y	SLD	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	0.30	-1.00
31	CC 31 - Amb. 2 (SLU S) S -0.3X-Y	SLV	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	-0.30	-1.00
32	CC 32 - Amb. 2 (SLE) S -0.3X-Y	SLD	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	-0.30	-1.00
33	CC 33 - Amb. 3 (SLU) F X	SLU	L	N	1.30	1.50	1.50	1.50	1.50	0.00	1.00	0.00	0.00	0.00
34	CC 34 - Amb. 3 (SLU) F -X	SLU	L	N	1.30	1.50	1.50	1.50	1.50	0.00	-1.00	0.00	0.00	0.00
35	CC 35 - Amb. 3 (SLU) F Y	SLU	L	N	1.30	1.50	1.50	1.50	1.50	0.00	0.00	1.00	0.00	0.00
36	CC 36 - Amb. 3 (SLU) F -Y	SLU	L	N	1.30	1.50	1.50	1.50	1.50	0.00	0.00	-1.00	0.00	0.00
37	CC 37 - Amb. 3 (SLE R) F X	SLE R	L	N	1.00	1.00	1.00	1.00	1.00	0.00	1.00	0.00	0.00	0.00
38	CC 38 - Amb. 3 (SLE R) F -X	SLE R	L	N	1.00	1.00	1.00	1.00	1.00	0.00	-1.00	0.00	0.00	0.00
39	CC 39 - Amb. 3 (SLE R) F Y	SLE R	L	N	1.00	1.00	1.00	1.00	1.00	0.00	0.00	1.00	0.00	0.00
40	CC 40 - Amb. 3 (SLE R) F -Y	SLE R	L	N	1.00	1.00	1.00	1.00	1.00	0.00	0.00	-1.00	0.00	0.00
41	CC 41 - Amb. 3 (SLE F) F X	SLE F	L	N	1.00	1.00	0.70	0.20	0.20	0.00	1.00	0.00	0.00	0.00
42	CC 42 - Amb. 3 (SLE F) F -X	SLE F	L	N	1.00	1.00	0.70	0.20	0.20	0.00	-1.00	0.00	0.00	0.00

43 CC 43 - Amb. 3 (SLE F) F Y	SLE F L	N	1.00	1.00	0.70	0.20	0.20	0.00	0.00	1.00	0.00	0.00
44 CC 44 - Amb. 3 (SLE F) F -Y	SLE F L	N	1.00	1.00	0.70	0.20	0.20	0.00	0.00	-1.00	0.00	0.00
45 CC 45 - Amb. 3 (SLE Q) F X	SLE Q L	N	1.00	1.00	0.60	0.00	0.00	0.00	1.00	0.00	0.00	0.00
46 CC 46 - Amb. 3 (SLE Q) F -X	SLE Q L	N	1.00	1.00	0.60	0.00	0.00	0.00	-1.00	0.00	0.00	0.00
47 CC 47 - Amb. 3 (SLE Q) F Y	SLE Q L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	1.00	0.00	0.00
48 CC 48 - Amb. 3 (SLE Q) F -Y	SLE Q L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	-1.00	0.00	0.00

ELENCO BARICENTRI E MASSE IMPALCATI:

Simbologia

Nodo = Numero del nodo
Mo = Massa orizzontale

Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>
-284	96.18	-283	100.72	-282	25.22	-281	100.72	-280	96.18	-279	171.91	-278	162.79
-277	162.79	-276	171.91										
-275	163.51	-274	172.70	-273	172.70	-272	163.51	-271	180.14	-270	170.87	-269	26.58
-268	170.87	-267	180.14										
-266	164.95	-265	174.29	-264	174.29	-263	164.95	-262	175.08	-261	165.68	-260	165.68
-259	175.08	-258	173.40										
-257	182.87	-256	27.95	-255	182.87	-254	173.40	-253	176.69	-252	167.15	-251	167.15
-250	176.69	-249	1305.87										
-248	242.10	-247	1269.78	-246	411.64	-245	823.28	-244	1814.31	-243	1732.57	-242	823.28
-241	823.28	-240	1814.31										
-239	1732.57	-238	823.28	-237	823.28	-236	1814.31	-235	1732.57	-234	823.28	-233	823.28
-231	1310.65	-230	242.10										
-229	1265.00	-228	411.64	-227	43.00	-226	86.01	-225	86.01	-224	86.01	-223	86.01
-222	86.01	-221	86.01										
-220	86.01	-219	43.00	-218	43.00	-217	86.01	-216	86.01	-215	86.01	-214	86.01
-213	86.01	-212	86.01										
-211	86.01	-210	43.00	-209	821.87	-208	484.20	-207	821.87	-206	43.00	-205	86.01
-204	344.04	-203	344.04										
-202	86.01	-201	86.01	-200	344.04	-199	344.04	-198	86.01	-197	86.01	-196	344.04
-195	344.04	-194	86.01										
-193	86.01	-192	821.87	-191	484.20	-190	821.87	-189	43.00	-188	43.00	-187	86.01
-186	86.01	-185	86.01										
-184	86.01	-183	86.01	-182	86.01	-181	86.01	-180	43.00	-179	43.00	-178	86.01
-177	86.01	-176	86.01										
-175	86.01	-174	86.01	-173	86.01	-172	86.01	-171	43.00	-170	821.87	-169	484.20
-168	821.87	-167	43.00										
-166	86.01	-165	344.04	-164	344.04	-163	86.01	-162	86.01	-161	344.04	-160	344.04
-159	86.01	-158	86.01										
-157	344.04	-156	344.04	-155	86.01	-154	86.01	-153	821.87	-152	484.20	-151	821.87
-150	43.00	-149	43.00										
-148	86.01	-147	86.01	-146	86.01	-145	86.01	-144	86.01	-143	86.01	-142	86.01
-141	43.00	-140	43.00										
-139	86.01	-138	86.01	-137	86.01	-136	86.01	-135	86.01	-134	86.01	-133	86.01
-132	43.00	-131	821.87										
-130	484.20	-129	821.87	-128	43.00	-127	86.01	-126	344.04	-125	344.04	-124	86.01
-123	86.01	-122	344.04										
-121	344.04	-120	86.01	-119	86.01	-118	344.04	-117	344.04	-116	86.01	-115	86.01
-114	821.87	-113	484.20										
-112	821.87	-111	43.00	-110	43.00	-109	86.01	-108	86.01	-107	86.01	-106	86.01
-105	86.01	-104	86.01										
-103	86.01	-102	43.00	-101	43.00	-100	86.01	-99	86.01	-98	86.01	-97	86.01
-96	86.01	-95	86.01										
-94	86.01	-93	43.00	-92	821.87	-91	484.20	-90	821.87	-89	43.00	-88	86.01
-87	344.04	-86	344.04										
-85	86.01	-84	86.01	-83	344.04	-82	344.04	-81	86.01	-80	86.01	-79	344.04
-78	344.04	-77	86.01										
-76	86.01	-75	821.87	-74	484.20	-73	821.87	-72	43.00	-71	43.00	-70	86.01
-69	86.01	-68	86.01										
-67	86.01	-66	86.01	-65	86.01	-64	86.01	-63	43.00	-62	43.00	-61	86.01
-60	86.01	-59	86.01										
-58	86.01	-57	86.01	-56	86.01	-55	86.01	-54	43.00				

TOTALI MASSE NODI:

Mo <kg>
63053.40

ELENCO PESI E FORZE FITTIZIE IMPALCATI:

Simbologia

Nodo = Numero del nodo
Peso = Peso
Fx = Forza in dir. X
Fy = Forza in dir. Y

Nodo	Peso <daN>	Fx Peso <daN>	Fy Fx <daN>	Fy Nodo <daN>	Peso <daN>	Fx <daN>	Fy <daN>	Nodo	Peso <daN>	Fx <daN>	Fy <daN>	Nodo	Peso <daN>	Fx <daN>	Fy <daN>
-284	94.35	0.94	0.94	-283	98.81	0.99	0.99	-282	24.74	0.25	0.25	-281	98.81	0.99	0.99
-280	94.35	0.94	0.94	-279	168.64	1.69	1.69	-278	159.70	1.60	1.60	-277	159.70	1.60	1.60
-276	168.64	1.69	1.69	-275	160.40	1.60	1.60	-274	169.42	1.69	1.69	-273	169.42	1.69	1.69
-272	160.40	1.60	1.60	-271	176.71	1.77	1.77	-270	167.63	1.68	1.68	-269	26.08	0.26	0.26
-268	167.63	1.68	1.68	-267	176.71	1.77	1.77	-266	161.82	1.62	1.62	-265	170.97	1.71	1.71
-264	170.97	1.71	1.71	-263	161.82	1.62	1.62	-262	171.76	1.72	1.72	-261	162.53	1.63	1.63
-260	162.53	1.63	1.63	-259	171.76	1.72	1.72	-258	170.11	1.70	1.70	-257	179.40	1.79	1.79
-256	27.42	0.27	0.27	-255	179.40	1.79	1.79	-254	170.11	1.70	1.70	-253	173.33	1.73	1.73
-252	163.98	1.64	1.64	-251	163.98	1.64	1.64	-250	173.33	1.73	1.73	-249	1549.57	15.50	15.50
-248	237.50	2.38	2.38	-247	1500.80	15.01	15.01	-246	531.39	5.31	5.31	-245	1062.79	10.63	10.63
-244	2316.87	23.17	23.17	-243	2209.95	22.10	22.10	-242	1062.79	10.63	10.63	-241	1062.79	10.63	10.63
-240	2316.87	23.17	23.17	-239	2209.95	22.10	22.10	-238	1062.79	10.63	10.63	-237	1062.79	10.63	10.63
-236	2316.87	23.17	23.17	-235	2209.95	22.10	22.10	-234	1062.79	10.63	10.63	-233	1062.79	10.63	10.63
-231	1554.26	15.54	15.54	-230	237.50	2.38	2.38	-229	1496.11	14.96	14.96	-228	531.39	5.31	5.31
-227	42.19	0.42	0.42	-226	84.38	0.84	0.84	-225	84.38	0.84	0.84	-224	84.38	0.84	0.84
-223	84.38	0.84	0.84	-222	84.38	0.84	0.84	-221	84.38	0.84	0.84	-220	84.38	0.84	0.84
-219	42.19	0.42	0.42	-218	42.19	0.42	0.42	-217	84.38	0.84	0.84	-216	84.37	0.84	0.84
-215	84.38	0.84	0.84	-214	84.38	0.84	0.84	-213	84.38	0.84	0.84	-212	84.38	0.84	0.84
-211	84.38	0.84	0.84	-210	42.19	0.42	0.42	-209	806.25	8.06	8.06	-208	475.00	4.75	4.75
-207	806.25	8.06	8.06	-206	42.19	0.42	0.42	-205	84.37	0.84	0.84	-204	337.50	3.38	3.38
-203	337.50	3.38	3.38	-202	84.37	0.84	0.84	-201	84.37	0.84	0.84	-200	337.50	3.38	3.38
-199	337.50	3.38	3.38	-198	84.37	0.84	0.84	-197	84.37	0.84	0.84	-196	337.50	3.38	3.38
-195	337.50	3.38	3.38	-194	84.38	0.84	0.84	-193	84.37	0.84	0.84	-192	806.25	8.06	8.06
-191	475.00	4.75	4.75	-190	806.25	8.06	8.06	-189	42.19	0.42	0.42	-188	42.19	0.42	0.42
-187	84.38	0.84	0.84	-186	84.38	0.84	0.84	-185	84.38	0.84	0.84	-184	84.38	0.84	0.84
-183	84.38	0.84	0.84	-182	84.38	0.84	0.84	-181	84.38	0.84	0.84	-180	42.19	0.42	0.42
-179	42.19	0.42	0.42	-178	84.38	0.84	0.84	-177	84.38	0.84	0.84	-176	84.38	0.84	0.84
-175	84.38	0.84	0.84	-174	84.38	0.84	0.84	-173	84.38	0.84	0.84	-172	84.38	0.84	0.84
-171	42.19	0.42	0.42	-170	806.25	8.06	8.06	-169	475.00	4.75	4.75	-168	806.25	8.06	8.06
-167	42.19	0.42	0.42	-166	84.37	0.84	0.84	-165	337.50	3.38	3.38	-164	337.50	3.38	3.38
-163	84.37	0.84	0.84	-162	84.37	0.84	0.84	-161	337.50	3.38	3.38	-160	337.50	3.38	3.38
-159	84.37	0.84	0.84												

-158	84.37	0.84	0.84	-157	337.50	3.38	3.38	-156	337.50	3.38	3.38	-155	84.37	0.84
0.84	-154	84.37	0.84	0.84										
-153	806.25	8.06	8.06	-152	475.00	4.75	4.75	-151	806.25	8.06	8.06	-150	42.19	0.42
0.42	-149	42.19	0.42	0.42										
-148	84.38	0.84	0.84	-147	84.38	0.84	0.84	-146	84.38	0.84	0.84	-145	84.38	0.84
0.84	-144	84.38	0.84	0.84										
-143	84.38	0.84	0.84	-142	84.38	0.84	0.84	-141	42.19	0.42	0.42	-140	42.19	0.42
0.42	-139	84.38	0.84	0.84										
-138	84.38	0.84	0.84	-137	84.38	0.84	0.84	-136	84.38	0.84	0.84	-135	84.38	0.84
0.84	-134	84.38	0.84	0.84										
-133	84.38	0.84	0.84	-132	42.19	0.42	0.42	-131	806.25	8.06	8.06	-130	475.00	4.75
4.75	-129	806.25	8.06	8.06										
-128	42.19	0.42	0.42	-127	84.37	0.84	0.84	-126	337.50	3.38	3.38	-125	337.50	3.38
3.38	-124	84.37	0.84	0.84										
-123	84.37	0.84	0.84	-122	337.50	3.38	3.38	-121	337.50	3.38	3.38	-120	84.37	0.84
0.84	-119	84.37	0.84	0.84										
-118	337.50	3.38	3.38	-117	337.50	3.38	3.38	-116	84.37	0.84	0.84	-115	84.37	0.84
0.84	-114	806.25	8.06	8.06										
-113	475.00	4.75	4.75	-112	806.25	8.06	8.06	-111	42.19	0.42	0.42	-110	42.19	0.42
0.42	-109	84.38	0.84	0.84										
-108	84.38	0.84	0.84	-107	84.38	0.84	0.84	-106	84.38	0.84	0.84	-105	84.38	0.84
0.84	-104	84.38	0.84	0.84										
-103	84.38	0.84	0.84	-102	42.19	0.42	0.42	-101	42.19	0.42	0.42	-100	84.38	0.84
0.84	-99	84.38	0.84	0.84										
-98	84.38	0.84	0.84	-97	84.38	0.84	0.84	-96	84.38	0.84	0.84	-95	84.38	0.84
0.84	-94	84.38	0.84	0.84										
-93	42.19	0.42	0.42	-92	806.25	8.06	8.06	-91	475.00	4.75	4.75	-90	806.25	8.06
8.06	-89	42.19	0.42	0.42										
-88	84.37	0.84	0.84	-87	337.50	3.38	3.38	-86	337.50	3.38	3.38	-85	84.37	0.84
0.84	-84	84.37	0.84	0.84										
-83	337.50	3.38	3.38	-82	337.50	3.38	3.38	-81	84.37	0.84	0.84	-80	84.37	0.84
0.84	-79	337.50	3.38	3.38										
-78	337.50	3.38	3.38	-77	84.38	0.84	0.84	-76	84.37	0.84	0.84	-75	806.25	8.06
8.06	-74	475.00	4.75	4.75										
-73	806.25	8.06	8.06	-72	42.19	0.42	0.42	-71	42.19	0.42	0.42	-70	84.38	0.84
0.84	-69	84.38	0.84	0.84										
-68	84.38	0.84	0.84	-67	84.38	0.84	0.84	-66	84.38	0.84	0.84	-65	84.38	0.84
0.84	-64	84.38	0.84	0.84										
-63	42.19	0.42	0.42	-62	42.19	0.42	0.42	-61	84.38	0.84	0.84	-60	84.38	0.84
0.84	-59	84.38	0.84	0.84										
-58	84.38	0.84	0.84	-57	84.38	0.84	0.84	-56	84.38	0.84	0.84	-55	84.38	0.84
0.84	-54	42.19	0.42	0.42										

ELENCO MODI DI VIBRARE, MASSE PARTECIPANTI E COEFFICIENTI DI PARTECIPAZIONE

Simbologia

Modo = Numero del modo di vibrare
C = * indica che il modo è stato considerato
Per. = Periodo
Diff. = Minima differenza percentuale dagli altri periodi
Φx = Coefficiente di partecipazione in dir. X
Φy = Coefficiente di partecipazione in dir. Y
Φz = Coefficiente di partecipazione in dir. Z
%Mx = Percentuale massa partecipante in dir. X
%My = Percentuale massa partecipante in dir. Y
%Mz = Percentuale massa partecipante in dir. Z
%Jpz = Percentuale momento d'inerzia polare partecipante intorno all'asse Z

Modo	C	Per.	Diff.	**Φx**	**Φy**	**Φz**	%Mx	%My	%Mz	%Jpz
1	*	0.3979	24.43	48.78	0.01	0.00	37.745	0.000	0.000	0.000
2	*	0.3198	14.27	0.03	-49.77	0.00	0.000	39.283	0.000	0.000
3	*	0.2798	14.27	-34.41	0.00	0.00	18.779	0.000	0.000	0.000
4	*	0.1235	36.84	-38.94	-0.21	0.00	24.052	0.001	0.000	0.000
5	*	0.0902	22.98	-0.31	38.12	0.00	0.001	23.043	0.000	0.000
6		0.0734	22.98	-0.00	-0.01	0.00	0.000	0.000	0.000	0.000
7		0.0582	26.17	-0.00	0.00	0.00	0.000	0.000	0.000	0.000
8		0.0422	3.20	8.75	0.72	0.00	1.214	0.008	0.000	0.000
9		0.0408	3.20	-0.00	0.07	0.00	0.000	0.000	0.000	0.000

10		0.0363	6.00	0.53	0.03	0.00	0.004	0.000	0.000	0.000
11	*	0.0343	0.93	-0.00	34.92	0.00	0.000	19.339	0.000	0.000
12		0.0340	0.93	-0.43	9.63	0.00	0.003	1.469	0.000	0.000
13	*	0.0318	6.70	-15.64	-0.00	0.00	3.881	0.000	0.000	0.000
14		0.0269	11.45	-0.01	-0.04	0.00	0.000	0.000	0.000	0.000
15	*	0.0241	11.45	-10.11	0.22	0.00	1.620	0.001	0.000	0.000
16		0.0204	3.21	-8.98	-0.55	0.00	1.279	0.005	0.000	0.000
17		0.0197	3.21	-0.01	-0.03	0.00	0.000	0.000	0.000	0.000
18		0.0188	3.43	-0.02	-0.08	0.00	0.000	0.000	0.000	0.000
19		0.0182	0.58	-0.59	3.36	0.00	0.006	0.179	0.000	0.000
20		0.0181	0.58	-0.02	0.23	0.00	0.000	0.001	0.000	0.000
21		0.0164	5.49	-0.01	-0.06	0.00	0.000	0.000	0.000	0.000
22		0.0156	5.49	-0.00	-0.00	0.00	0.000	0.000	0.000	0.000
23		0.0143	0.07	0.16	0.02	0.00	0.000	0.000	0.000	0.000
24		0.0143	0.07	4.32	0.58	0.00	0.296	0.005	0.000	0.000
25		0.0136	0.20	-0.64	-0.00	0.00	0.007	0.000	0.000	0.000
26		0.0136	0.20	-0.99	0.18	0.00	0.015	0.001	0.000	0.000
27		0.0133	2.10	-0.66	1.63	0.00	0.007	0.042	0.000	0.000
28		0.0130	2.38	-0.00	-0.02	0.00	0.000	0.000	0.000	0.000
29		0.0123	4.27	-0.02	0.02	0.00	0.000	0.000	0.000	0.000
30		0.0118	3.38	-9.79	-0.47	0.00	1.519	0.004	0.000	0.000
31		0.0114	0.87	2.95	-1.36	0.00	0.138	0.029	0.000	0.000
32		0.0114	0.87	8.80	0.10	0.00	1.228	0.000	0.000	0.000
33		0.0113	0.88	-0.06	-0.01	0.00	0.000	0.000	0.000	0.000
34		0.0111	1.19	-0.07	0.00	0.00	0.000	0.000	0.000	0.000
35		0.0108	0.41	-0.00	-0.00	0.00	0.000	0.000	0.000	0.000
36		0.0107	0.41	0.11	1.17	0.00	0.000	0.022	0.000	0.000
37		0.0104	0.00	-0.00	0.00	0.00	0.000	0.000	0.000	0.000
38		0.0104	0.00	8.93	-0.00	0.00	1.265	0.000	0.000	0.000
39		0.0104	0.21	-1.33	0.93	0.00	0.028	0.014	0.000	0.000
40		0.0102	1.25	0.12	0.28	0.00	0.000	0.001	0.000	0.000
41		0.0101	1.25	-0.00	0.01	0.00	0.000	0.000	0.000	0.000
42		0.0099	0.13	0.01	0.00	0.00	0.000	0.000	0.000	0.000
43		0.0098	0.13	-0.01	0.03	0.00	0.000	0.000	0.000	0.000
44		0.0097	0.08	0.44	-1.00	0.00	0.003	0.016	0.000	0.000
45		0.0097	0.08	-0.01	0.01	0.00	0.000	0.000	0.000	0.000
46		0.0094	1.52	0.00	-0.00	0.00	0.000	0.000	0.000	0.000
47		0.0093	0.55	-1.48	0.86	0.00	0.035	0.012	0.000	0.000
48		0.0093	0.55	-6.98	-0.43	0.00	0.773	0.003	0.000	0.000
49	*	0.0082	3.31	-0.05	22.59	0.00	0.000	8.096	0.000	0.000
50		0.0080	3.31	-0.02	-1.05	0.00	0.000	0.017	0.000	0.000
51		0.0075	5.62	-0.00	0.00	0.00	0.000	0.000	0.000	0.000
52		0.0069	1.07	2.73	-0.04	0.00	0.118	0.000	0.000	0.000
53		0.0069	0.07	-9.81	0.14	0.00	1.527	0.000	0.000	0.000
54		0.0068	0.07	0.00	-0.00	0.00	0.000	0.000	0.000	0.000
55		0.0065	0.89	1.05	-0.00	0.00	0.017	0.000	0.000	0.000
56		0.0064	0.89	1.31	-0.01	0.00	0.027	0.000	0.000	0.000
57		0.0063	1.27	-0.04	0.00	0.00	0.000	0.000	0.000	0.000
58		0.0062	1.08	-1.96	-0.14	0.00	0.061	0.000	0.000	0.000
59		0.0062	0.45	0.46	-0.08	0.00	0.003	0.000	0.000	0.000
60		0.0061	0.45	3.22	0.01	0.00	0.165	0.000	0.000	0.000
61		0.0061	0.23	-5.13	3.51	0.00	0.417	0.196	0.000	0.000
62		0.0061	0.23	-2.59	-5.61	0.00	0.107	0.499	0.000	0.000
63		0.0060	1.67	2.98	1.32	0.00	0.140	0.027	0.000	0.000
64		0.0059	0.53	-0.10	-0.00	0.00	0.000	0.000	0.000	0.000
65		0.0058	0.53	0.00	16.31	0.00	0.000	4.220	0.000	0.000
66		0.0058	0.89	-0.03	-0.01	0.00	0.000	0.000	0.000	0.000
67		0.0057	1.13	0.01	0.11	0.00	0.000	0.000	0.000	0.000
68		0.0056	1.64	-0.01	0.01	0.00	0.000	0.000	0.000	0.000
69		0.0055	2.23	-0.50	-0.48	0.00	0.004	0.004	0.000	0.000
70		0.0054	0.53	0.37	-0.03	0.00	0.002	0.000	0.000	0.000
71		0.0053	0.53	-6.67	-0.19	0.00	0.707	0.001	0.000	0.000
72		0.0053	0.66	-0.01	0.78	0.00	0.000	0.010	0.000	0.000
73		0.0051	0.26	0.94	2.49	0.00	0.014	0.098	0.000	0.000
74		0.0051	0.10	6.27	-0.00	0.00	0.623	0.000	0.000	0.000
75		0.0051	0.10	-0.00	0.00	0.00	0.000	0.000	0.000	0.000
76		0.0051	0.61	-0.64	1.42	0.00	0.007	0.032	0.000	0.000
77		0.0051	0.33	0.39	-4.40	0.00	0.002	0.308	0.000	0.000
78		0.0050	0.33	0.07	-0.31	0.00	0.000	0.002	0.000	0.000
79		0.0050	0.77	-0.63	1.31	0.00	0.006	0.027	0.000	0.000
80		0.0049	0.42	-0.13	-0.11	0.00	0.000	0.000	0.000	0.000
81		0.0049	0.42	0.28	-0.04	0.00	0.001	0.000	0.000	0.000
82		0.0048	0.70	0.42	0.00	0.00	0.003	0.000	0.000	0.000

83	0.0048	0.70	0.04	0.02	0.00	0.000	0.000	0.000	0.000
84	0.0047	0.29	0.17	0.00	0.00	0.000	0.000	0.000	0.000
85	0.0047	0.29	-0.40	0.48	0.00	0.003	0.004	0.000	0.000
86	0.0047	0.11	0.27	-0.30	0.00	0.001	0.001	0.000	0.000
87	0.0047	0.11	-0.09	0.03	0.00	0.000	0.000	0.000	0.000
88	0.0046	1.14	0.04	0.01	0.00	0.000	0.000	0.000	0.000
89	0.0045	1.14	-0.06	-0.72	0.00	0.000	0.008	0.000	0.000
90	0.0045	0.53	0.41	-0.35	0.00	0.003	0.002	0.000	0.000
91	0.0045	0.53	-0.09	0.33	0.00	0.000	0.002	0.000	0.000
92	0.0044	0.17	-0.30	-0.37	0.00	0.001	0.002	0.000	0.000
93	0.0044	0.13	-0.01	0.08	0.00	0.000	0.000	0.000	0.000
94	0.0044	0.13	0.06	0.10	0.00	0.000	0.000	0.000	0.000
95	0.0044	1.43	-0.01	0.13	0.00	0.000	0.000	0.000	0.000
96	0.0043	0.26	0.01	-0.30	0.00	0.000	0.001	0.000	0.000
97	0.0042	0.26	0.00	0.00	0.00	0.000	0.000	0.000	0.000
98	0.0042	0.44	0.22	-2.07	0.00	0.001	0.068	0.000	0.000
99	0.0042	0.62	0.52	1.12	0.00	0.004	0.020	0.000	0.000
100	0.0042	0.44	0.01	0.04	0.00	0.000	0.000	0.000	0.000
101	0.0042	0.44	0.00	0.23	0.00	0.000	0.001	0.000	0.000
102	0.0040	0.01	0.13	-0.00	0.00	0.000	0.000	0.000	0.000
103	0.0040	0.01	0.26	-0.00	0.00	0.001	0.000	0.000	0.000
104	0.0040	0.35	0.07	-0.01	0.00	0.000	0.000	0.000	0.000
105	0.0040	0.31	-0.32	-0.02	0.00	0.002	0.000	0.000	0.000
106	0.0040	0.31	0.05	-0.05	0.00	0.000	0.000	0.000	0.000
107	0.0039	0.21	0.19	0.23	0.00	0.001	0.001	0.000	0.000
108	0.0039	0.17	0.04	0.79	0.00	0.000	0.010	0.000	0.000
109	0.0039	0.17	0.04	0.28	0.00	0.000	0.001	0.000	0.000
110	0.0038	0.32	0.03	-0.05	0.00	0.000	0.000	0.000	0.000
111	0.0038	0.32	0.15	0.05	0.00	0.000	0.000	0.000	0.000
112	0.0038	0.42	-0.41	-0.09	0.00	0.003	0.000	0.000	0.000
113	0.0038	0.33	0.02	0.04	0.00	0.000	0.000	0.000	0.000
114	0.0038	0.33	-0.04	-0.72	0.00	0.000	0.008	0.000	0.000
115	0.0037	0.53	-0.00	-0.00	0.00	0.000	0.000	0.000	0.000
116	0.0037	0.99	-0.00	0.01	0.00	0.000	0.000	0.000	0.000
117	0.0036	0.99	-0.05	-4.57	0.00	0.000	0.331	0.000	0.000
118	0.0036	0.52	-6.50	0.08	0.00	0.669	0.000	0.000	0.000
119	0.0036	0.12	0.17	0.00	0.00	0.000	0.000	0.000	0.000
120	0.0036	0.12	-0.02	-0.09	0.00	0.000	0.000	0.000	0.000
Tot.cons.						86.08	89.76	0.00	0.00

ELENCO COEFFICIENTI DI RISPOSTA

Simbologia

Modo = Numero del modo di vibrare
Sx = Coefficiente di risposta (moltiplicato per 100) in dir. X
Sy = Coefficiente di risposta (moltiplicato per 100) in dir. Y

Stato limite di danno	Modo	Sx	Sy
	1	17.96	17.96
	2	18.52	18.52
	3	18.52	18.52
	4	18.07	18.07
	5	15.16	15.16
	6	13.69	13.69
	7	12.35	12.35
	8	10.95	10.95
	9	10.84	10.84
	10	10.44	10.44
	11	10.26	10.26
	12	10.23	10.23
	13	10.05	10.05
	14	9.62	9.62
	15	9.37	9.37
	16	9.04	9.04
	17	8.99	8.99
	18	8.91	8.91
	19	8.86	8.86
	20	8.85	8.85
	21	8.70	8.70

22	8.63	8.63
23	8.51	8.51
24	8.51	8.51
25	8.45	8.45
26	8.45	8.45
27	8.42	8.42
28	8.40	8.40
29	8.34	8.34
30	8.30	8.30
31	8.26	8.26
32	8.26	8.26
33	8.25	8.25
34	8.24	8.24
35	8.21	8.21
36	8.20	8.20
37	8.17	8.17
38	8.17	8.17
39	8.17	8.17
40	8.15	8.15
41	8.14	8.14
42	8.12	8.12
43	8.12	8.12
44	8.11	8.11
45	8.11	8.11
46	8.09	8.09
47	8.08	8.08
48	8.07	8.07
49	7.98	7.98
50	7.96	7.96
51	7.92	7.92
52	7.87	7.87
53	7.86	7.86
54	7.86	7.86
55	7.83	7.83
56	7.83	7.83
57	7.81	7.81
58	7.81	7.81
59	7.80	7.80
60	7.80	7.80
61	7.79	7.79
62	7.79	7.79
63	7.78	7.78
64	7.77	7.77
65	7.77	7.77
66	7.77	7.77
67	7.76	7.76
68	7.75	7.75
69	7.74	7.74
70	7.73	7.73
71	7.73	7.73
72	7.73	7.73
73	7.71	7.71
74	7.71	7.71
75	7.71	7.71
76	7.71	7.71
77	7.70	7.70
78	7.70	7.70
79	7.70	7.70
80	7.69	7.69
81	7.69	7.69
82	7.68	7.68
83	7.68	7.68
84	7.68	7.68
85	7.68	7.68
86	7.67	7.67
87	7.67	7.67
88	7.66	7.66
89	7.66	7.66
90	7.65	7.65
91	7.65	7.65
92	7.65	7.65
93	7.65	7.65
94	7.65	7.65

95	7.64	7.64
96	7.63	7.63
97	7.63	7.63
98	7.63	7.63
99	7.63	7.63
100	7.63	7.63
101	7.62	7.62
102	7.61	7.61
103	7.61	7.61
104	7.61	7.61
105	7.61	7.61
106	7.61	7.61
107	7.60	7.60
108	7.60	7.60
109	7.60	7.60
110	7.60	7.60
111	7.60	7.60
112	7.59	7.59
113	7.59	7.59
114	7.59	7.59
115	7.59	7.59
116	7.58	7.58
117	7.58	7.58
118	7.57	7.57
119	7.57	7.57
120	7.57	7.57

Stato limite di salvaguardia della vita

Modo	Sx	Sy
1	27.62	27.62
2	27.62	27.62
3	27.62	27.62
4	26.38	26.38
5	23.87	23.87
6	22.59	22.59
7	21.44	21.44
8	20.23	20.23
9	20.14	20.14
10	19.79	19.79
11	19.64	19.64
12	19.62	19.62
13	19.45	19.45
14	19.08	19.08
15	18.87	18.87
16	18.59	18.59
17	18.54	18.54
18	18.47	18.47
19	18.43	18.43
20	18.42	18.42
21	18.29	18.29
22	18.23	18.23
23	18.13	18.13
24	18.13	18.13
25	18.08	18.08
26	18.07	18.07
27	18.05	18.05
28	18.03	18.03
29	17.98	17.98
30	17.94	17.94
31	17.92	17.92
32	17.91	17.91
33	17.90	17.90
34	17.89	17.89
35	17.86	17.86
36	17.86	17.86
37	17.84	17.84
38	17.84	17.84
39	17.84	17.84
40	17.82	17.82
41	17.81	17.81
42	17.80	17.80
43	17.79	17.79

44	17.78	17.78
45	17.78	17.78
46	17.76	17.76
47	17.75	17.75
48	17.75	17.75
49	17.67	17.67
50	17.65	17.65
51	17.62	17.62
52	17.57	17.57
53	17.57	17.57
54	17.57	17.57
55	17.54	17.54
56	17.54	17.54
57	17.53	17.53
58	17.52	17.52
59	17.52	17.52
60	17.51	17.51
61	17.51	17.51
62	17.51	17.51
63	17.50	17.50
64	17.49	17.49
65	17.49	17.49
66	17.49	17.49
67	17.48	17.48
68	17.47	17.47
69	17.46	17.46
70	17.46	17.46
71	17.45	17.45
72	17.45	17.45
73	17.44	17.44
74	17.44	17.44
75	17.44	17.44
76	17.44	17.44
77	17.43	17.43
78	17.43	17.43
79	17.43	17.43
80	17.42	17.42
81	17.42	17.42
82	17.41	17.41
83	17.41	17.41
84	17.41	17.41
85	17.41	17.41
86	17.40	17.40
87	17.40	17.40
88	17.40	17.40
89	17.39	17.39
90	17.39	17.39
91	17.39	17.39
92	17.38	17.38
93	17.38	17.38
94	17.38	17.38
95	17.38	17.38
96	17.37	17.37
97	17.37	17.37
98	17.37	17.37
99	17.37	17.37
100	17.37	17.37
101	17.36	17.36
102	17.35	17.35
103	17.35	17.35
104	17.35	17.35
105	17.35	17.35
106	17.35	17.35
107	17.34	17.34
108	17.34	17.34
109	17.34	17.34
110	17.34	17.34
111	17.34	17.34
112	17.34	17.34
113	17.33	17.33
114	17.33	17.33
115	17.33	17.33
116	17.33	17.33

117 17.32 17.32
118 17.32 17.32
119 17.32 17.32
120 17.32 17.32

Verifica pushover
SPOSTAMENTI RELATIVI MASSIMI ALLO SLD:

Simbologia

N1 = Nodo1
N2 = Nodo2
h = Altezza teorica
δ = Spostamento relativo
δ/h = Rapporto (moltiplicato per 1000) tra lo spostamento relativo e l'altezza
CC = Numero della combinazione delle condizioni di carico elementari

N1	N2	h <m>	δ <cm>	δ/h	CC	N1	N2	h <m>	δ <cm>	δ/h	CC	N1	N2	h <m>	δ <cm>	δ/h	CC
1	-73	1.00	0.07181	0.718	20	-73	-112	1.00	0.07614	0.761	18	-112	-151	1.00	0.07665	0.766	20
-151	-190	1.00	0.07702	0.770	20	-190	-229	1.00	0.07795	0.779	18	2	-75	1.00	0.07170	0.717	18
-75	-114	1.00	0.07644	0.764	20	-114	-153	1.00	0.07656	0.766	20	-153	-192	1.00	0.07704	0.770	20
-192	-231	1.00	0.07781	0.778	20	3	-90	1.00	0.07181	0.718	18	-90	-129	1.00	0.07613	0.761	20
-129	-168	1.00	0.07652	0.765	18	-168	-207	1.00	0.07701	0.770	18	-207	-247	1.00	0.07751	0.775	20
4	-92	1.00	0.07169	0.717	20	-92	-131	1.00	0.07643	0.764	18	-131	-170	1.00	0.07653	0.765	18
-170	-209	1.00	0.07705	0.771	20	-209	-249	1.00	0.07834	0.783	18						

Min = 0.72
Max = 0.78

Elenco unità geotecniche

1 :
Classificazione: Non classificato

Pesi:
- Peso specifico del terreno naturale: γ = 1800.00 daN/mc
- Peso specifico del terreno saturo: γ_{sat} = 2000.00 daN/mc
Parametri plastici:
- Angolo di attrito efficace: ϕ' = 24.00 grad
- Coesione efficace: c' = 500.00 daN/mq
- Coesione non drenata: c_u = 8671.40 daN/mq
  correlata alla stratigrafia 1
  valutata come valore medio risultante dalle seguenti correlazioni:

Correlazione	c_u <daN/mq>
Hara et al. (1971)	8671.40

Caratteristiche litostatiche:
- Grado di sovraconsolidazione: OCR = 8.33
  correlata alla stratigrafia 1
  valutata come valore medio risultante dalle seguenti correlazioni:

Correlazione	OCR
SPT Mayne e Kemper (1988)	8.33

- Coeff. di spinta a riposo: κ_0 = 1.41
  calcolato utilizzando le seguenti opzioni:
  -Calcolo di k0 Jaky(1936)
  -Calcolo di α Kulhawy (1989)

Parametri elastici:
- Modulo elastico normale: E = 450000.00 daN/mq
- Modulo elastico tangenziale: G = 173077.00 daN/mq
- Esponente del parametro tensionale: k_j = 0.00
- Coeff. di Poisson: ν = 0.30

- Modulo edometrico: E_{ed} = 605769.00 daN/mq
- Modulo elastico non drenato: E_u = 519231.00 daN/mq
  correlati alla stratigrafia 1
  Tipo di prova SPT, Stroud 1989
  Fattore elastico riduzione modulo secante: 1.00

2 :
Classificazione: Incoerente

Pesi:
- Peso specifico del terreno naturale: γ = 1800.00 daN/mc
- Peso specifico del terreno saturo: γ_{sat} = 2000.00 daN/mc

Parametri plastici:
- Angolo di attrito efficace: ϕ' = 34.00 grad
- Coesione efficace: c' = 500.00 daN/mq

Caratteristiche litostatiche:
- Grado di sovraconsolidazione: OCR = 5.22
  correlata alla stratigrafia 1
  valutata come valore medio risultante dalle seguenti correlazioni:

Correlazione	OCR
SPT Mayne e Kemper (1988)	5.22

- Coeff. di spinta a riposo: κ_0 = 1.11
  calcolato utilizzando le seguenti opzioni:
  -Calcolo di k0 Jaky(1936)
  -Calcolo di α Kulhawy (1989)

Parametri elastici:
- Modulo elastico normale: E = 405000.00 daN/mq
- Modulo elastico tangenziale: G = 184091.00 daN/mq
- Esponente del parametro tensionale: k_j = 0.00
- Coeff. di Poisson: ν = 0.10
- Modulo edometrico: E_{ed} = 414204.00 daN/mq
- Modulo elastico non drenato: E_u = 0.00 daN/mq

Elenco colonne stratigrafiche

Prove in sito

Report grafico complessivo
Le verifiche degli elementi di fondazione sono state effettuate utilizzando l'approccio 2.

Coefficienti parziali per le azioni, per verifiche in condizioni statiche:
Permanenti strutturali, sicurezza a favore γ_A = 1.00;
Permanenti strutturali, sicurezza a sfavore γ_A = 1.30;
Permanenti non strutturali, sicurezza a favore γ_A = 0.00;
Permanenti non strutturali, sicurezza a sfavore γ_A = 1.50;
Variabili, sicurezza a favore γ_A = 0.00;
Variabili, sicurezza a sfavore γ_A = 1.50.

I coefficienti parziali per le azioni sono posti pari all'unità per le verifiche in condizioni sismiche.

Tali coefficienti sono comunque desumibili dalla tabella delle combinazioni delle CCE (Parametri di calcolo).

Coefficienti parziali per i parametri geotecnici:
Tangente dell'angolo di attrito γ_M = 1.00;
Coesione efficace γ_M = 1.00;
Coesione non drenata γ_M = 1.00;

Coefficienti parziali per la resistenza delle fondazioni superficiali:
Capacità portante γ_R = 2.30;
Scorrimento γ_R = 1.10;

Coefficienti parziali per la resistenza delle fondazioni profonde:
Per pali infissi:
Resistenza alla base γ_R,b = 1.15;

Resistenza laterale in compressione γ_R,s = 1.15;
Resistenza laterale in trazione γ_R,t = 1.25;
Per pali trivellati:
Resistenza alla base γ_R,b = 1.35;
Resistenza laterale in compressione γ_R,s = 1.15;
Resistenza laterale in trazione γ_R,t = 1.25;
Per pali ad elica continua:
Resistenza alla base γ_R,b = 1.30;
Resistenza laterale in compressione γ_R,s = 1.15;
Resistenza laterale in trazione γ_R,t = 1.25;

Fattore di correlazione per la determinazione della resistenza caratteristica desumibile dai criteri di progetto.
Fondazioni superficiali

Simbologia

B = Base della fondazione
L = Lunghezza della fondazione (L>B)
D = Profondità del piano di posa della fondazione
β = Inclinazione del piano di campagna
η = Inclinazione del piano di posa della fondazione
γ_r = Peso specifico rappresentativo del terreno di fondazione
$\sigma_{v0,f}$ = Pressione verticale alla profondità del piano di posa della fondazione
φ'_r = Angolo di attrito rappresentativo del terreno di fondazione
c'_r = Coesione efficace rappresentativa del terreno di fondazione
N_q = Coefficiente di capacità portante relativo al sovraccarico laterale
N_c = Coefficiente di capacità portante relativo alla coesione del terreno di fondazione
N_g = Coefficiente di capacità portante relativo al peso del terreno di fondazione
b_q = Fattore di inclinazione del piano di fondazione relativo a sovraccarico laterale
b_c = Fattore di inclinazione del piano di fondazione relativo a coesione
b_g = Fattore di inclinazione del piano di fondazione relativo a peso del terreno
CC = Numero della combinazione delle condizioni di carico elementari
N = Sforzo normale
Tx = Taglio in dir. X
Ty = Taglio in dir. Y
Mx = Momento intorno all'asse X
My = Momento intorno all'asse Y
B' = Base della fondazione reagente
L' = Lunghezza della fondazione reagente
s_q = Fattore di forma relativo al sovraccarico laterale
s_c = Fattore di forma relativo alla coesione
s_g = Fattore di forma relativo al peso del terreno
i_q = Fattore di inclinazione relativo al sovraccarico laterale
i_c = Fattore di inclinazione relativo alla coesione
i_g = Fattore di inclinazione relativo al peso del terreno
q_{lim} = Pressione limite
R_d = Resistenza di progetto (Carico limite)
Sic. = Sicurezza a rottura

Verifiche capacità portante
Verifiche di capacità portante per rottura generale in condizioni statiche
Metodo utilizzato: Indicazioni EC7

Plinto n. 2

B=3.80 <m> L=3.80 <m> D=1.70 <m> β=0.00 <grad> η=0.00 <grad> γ_r=1800.00 <daN/mc>
$\sigma_{v0,f}$=3060.00 <daN/mq>

Verifiche in condizioni drenate

φ'_r=34.00 <grad> c'_r=500.00 <daN/mq>
N_q=29.44 N_c=42.16 N_g=38.37 b_q=1.00 b_c=1.00 b_g=1.00

CC	N	Tx	Ty	Mx	My	B'	L'	s_q	s_c	s_g	i_q	i_c	i_g	q_{lim}	R_d	Sic.
	<daN>	<daN>	<daN>	<daNm>	<daNm>	<m>	<m>							<daN/mq>	<daN>	
1	60162.70	6054.91	-5159.56	19046.50	10449.80	3.17	3.45	1.51	1.53	0.72	1.00	1.00	1.00	247825.00		

1178130.00 19.58
 2 59579.60 5804.26 -4991.52 18766.00 9433.03 3.17 3.48 1.51 1.53 0.73 1.00 1.00 1.00 247693.00
1189180.00 19.96
 3 59592.20 5870.20 -4949.81 18496.70 9842.81 3.18 3.47 1.51 1.53 0.73 1.00 1.00 1.00 248108.00
1189930.00 19.97
 4 60150.20 5988.97 -5201.27 19315.80 10040.00 3.16 3.47 1.51 1.53 0.73 1.00 1.00 1.00 247412.00
1177390.00 19.57
33 68338.90 6039.85 -10655.80 17859.00 33802.40 2.81 3.28 1.48 1.50 0.74 1.00 1.00 1.00 236919.00
948887.00 13.88
34 67755.80 5789.20 -10487.80 17578.50 32785.60 2.83 3.28 1.48 1.50 0.74 1.00 1.00 1.00 237655.00
960223.00 14.17
35 67768.40 5855.14 -10446.10 17309.20 33195.40 2.82 3.29 1.48 1.50 0.74 1.00 1.00 1.00 237159.00
956528.00 14.11
36 68326.40 5973.92 -10697.50 18128.30 33392.60 2.82 3.27 1.48 1.50 0.74 1.00 1.00 1.00 237412.00
952534.00 13.94

Verifiche di capacità portante per rottura generale in condizioni statiche
Metodo utilizzato: Indicazioni EC7

Plinto n. 1

B=3.80 <m> L=3.80 <m> D=1.70 <m> β=0.00 <grad> η=0.00 <grad> γ_r=1800.00 <daN/mc>
$\sigma_{v0,f}$=3060.00 <daN/mq>

Verifiche in condizioni drenate

φ'_r=34.00 <grad> c'_r=500.00 <daN/mq>
N_q=29.44 N_c=42.16 N_g=38.37 b_q=1.00 b_c=1.00 b_g=1.00

CC	N	Tx	Ty	Mx	My	B'	L'	s_q	s_c	s_g	i_q	i_c	i_g	q_{lim}	R_d
Sic.	<daN>	<daN>	<daN>	<daNm>	<daNm>	<m>	<m>							<daN/mq>	<daN>
1	59433.80	5800.19	4950.88	-18700.00	9280.83	3.17	3.49	1.51	1.53	0.73	1.00	1.00	1.00	247682.00	1190870.00 20.04
2	60016.90	6050.87	5118.91	-18980.50	10297.70	3.17	3.46	1.51	1.53	0.73	1.00	1.00	1.00	247814.00	1179760.00 19.66
3	59446.50	5865.31	4909.95	-18432.10	9689.27	3.18	3.47	1.51	1.53	0.73	1.00	1.00	1.00	248095.00	1191610.00 20.05
4	60004.30	5985.75	5159.84	-19248.30	9889.23	3.16	3.47	1.51	1.53	0.73	1.00	1.00	1.00	247403.00	1179030.00 19.65
33	21161.60	-1595.83	-5552.88	9282.99	-26398.30	1.31	2.92	1.25	1.26	0.87	1.00	1.00	1.00	178138.00	295423.00 13.96
34	21744.70	-1345.15	-5384.86	9002.52	-25381.40	1.47	2.97	1.28	1.29	0.85	1.00	1.00	1.00	185143.00	350601.00 16.12
35	21174.30	-1530.71	-5593.81	9550.87	-25989.80	1.35	2.90	1.26	1.27	0.86	1.00	1.00	1.00	180195.00	305398.00 14.42
36	21732.10	-1410.27	-5343.93	8734.65	-25789.90	1.43	3.00	1.27	1.28	0.86	1.00	1.00	1.00	183185.00	340421.00 15.66

Verifiche di capacità portante per rottura generale in condizioni statiche
Metodo utilizzato: Indicazioni EC7

Plinto n. 4

B=3.80 <m> L=3.80 <m> D=1.70 <m> β=0.00 <grad> η=0.00 <grad> γ_r=1800.00 <daN/mc>
$\sigma_{v0,f}$=3060.00 <daN/mq>

Verifiche in condizioni drenate

φ'_r=34.00 <grad> c'_r=500.00 <daN/mq>
N_q=29.44 N_c=42.16 N_g=38.37 b_q=1.00 b_c=1.00 b_g=1.00

CC	N	Tx	Ty	Mx	My	B'	L'	s_q	s_c	s_g	i_q	i_c	i_g	q_{lim}	R_d
Sic.	<daN>	<daN>	<daN>	<daNm>	<daNm>	<m>	<m>							<daN/mq>	<daN>
1	30068.80	-1358.98	150.46	10125.50	-1879.68	3.13	3.67	1.48	1.49	0.74	1.00	1.00	1.00	244809.00	1222970.00 40.67
2	29485.70	-1609.66	-17.59	10406.00	-2896.52	3.09	3.60	1.48	1.50	0.74	1.00	1.00	1.00	244218.00	

1183920.00 40.15
 3 30056.30 -1424.93   192.28   9855.98 -2289.48 3.14 3.65 1.48 1.50 0.74 1.00 1.00 1.00 245600.00
1224670.00 40.75
 4 29498.30 -1543.70   -59.42 10675.50 -2486.72 3.08 3.63 1.47 1.49 0.75 1.00 1.00 1.00 243403.00
1182190.00 40.08
33 68334.60 6053.66 10671.90 -17884.60 33822.20 2.81 3.28 1.48 1.50 0.74 1.00 1.00 1.00 236903.00
948379.00 13.88
34 67751.50 5802.98 10503.90 -17604.10 32805.40 2.83 3.28 1.48 1.50 0.74 1.00 1.00 1.00 237639.00
959709.00 14.17
35 68322.10 5987.71 10713.70 -18154.10 33412.40 2.82 3.27 1.48 1.50 0.74 1.00 1.00 1.00 237396.00
952023.00 13.93
36 67764.10 5868.93 10462.00 -17334.60 33215.10 2.82 3.29 1.48 1.50 0.74 1.00 1.00 1.00 237143.00
956015.00 14.11

Verifiche di capacità portante per rottura generale in condizioni statiche
Metodo utilizzato: Indicazioni EC7

Plinto n. 3

B=3.80 <m> L=3.80 <m> D=1.70 <m> β=0.00 <grad> η=0.00 <grad> γ_r=1800.00 <daN/mc>
$\sigma_{v0,f}$=3060.00 <daN/mq>

Verifiche in condizioni drenate

φ'_r=34.00 <grad> c'_r=500.00 <daN/mq>
N_q=29.44 N_c=42.16 N_g=38.37 b_q=1.00 b_c=1.00 b_g=1.00

CC	N	Tx	Ty	Mx	My	B'	L'	s_q	s_c	s_g	i_q	i_c	i_g	q_{lim}	R_d Sic.
	<daN>	<daN>	<daN>	<daNm>	<daNm>	<m>	<m>							<daN/mq>	<daN>
1	29335.60	-1605.59	46.08	-10453.40	-3038.63	3.09	3.59	1.48	1.50	0.74	1.00	1.00	1.00	244063.00	1177050.00 40.12
2	29918.70	-1354.93	-121.95	-10172.90	-2021.82	3.12	3.66	1.48	1.49	0.74	1.00	1.00	1.00	244658.00	1216290.00 40.65
3	29906.10	-1420.04	-162.75	-9905.22	-2430.24	3.14	3.64	1.48	1.50	0.74	1.00	1.00	1.00	245449.00	1217950.00 40.73
4	29348.30	-1540.48	86.88	-10721.00	-2630.21	3.07	3.62	1.47	1.49	0.75	1.00	1.00	1.00	243247.00	1175360.00 40.05
33	21165.80	-1603.57	5568.96	-9308.38	-26407.90	1.30	2.92	1.25	1.26	0.87	1.00	1.00	1.00	178135.00	295100.00 13.94
34	21748.90	-1352.91	5400.93	-9027.90	-25391.10	1.47	2.97	1.28	1.29	0.85	1.00	1.00	1.00	185140.00	350235.00 16.10
35	21736.20	-1418.02	5360.12	-8760.25	-25799.50	1.43	2.99	1.27	1.28	0.86	1.00	1.00	1.00	183182.00	340064.00 15.64
36	21178.50	-1538.46	5609.76	-9576.03	-25999.40	1.34	2.90	1.26	1.27	0.86	1.00	1.00	1.00	180192.00	305066.00 14.40

Cedimenti
Metodo utilizzato: Terzaghi (1955)

Simbologia

B = Base della fondazione
L = Lunghezza della fondazione (L>B)
k_1 = Costante di sottofondo standardizzata
kw = Costante di sottofondo
CC = Numero della combinazione delle condizioni di carico elementari
N = Sforzo normale
q_{es} = Pressione di esercizio
Ced = Cedimento calcolato

Plinto n. 2
B=3.80 <m> L=3.80 <m> k_1=1500000.00 <daN/mc> kw=436548.00 <daN/mc>

CC	N	q_{es}	Ced
	<daN>	<daN/mq>	<cm>
1	60162.70	4166.39	0.95
2	59579.60	4126.01	0.95
3	59592.20	4126.88	0.95

4	60150.20	4165.52	0.95
5	50533.90	3499.58	0.80
6	49950.80	3459.20	0.79
7	49963.40	3460.07	0.79
8	50521.40	3498.71	0.80
9	41696.10	2887.54	0.66
10	41113.00	2847.16	0.65
11	41125.60	2848.03	0.65
12	41683.50	2886.67	0.66
13	39442.50	2731.47	0.63
14	38859.40	2691.09	0.62
15	38871.90	2691.96	0.62
16	39429.90	2730.60	0.63
17	48203.90	3338.22	0.76
18	45267.10	3134.84	0.72
19	52467.30	3633.47	0.83
20	47173.40	3266.86	0.75
21	33664.70	2331.35	0.53
22	38958.60	2697.96	0.62
23	37928.10	2626.60	0.60
24	40864.90	2829.98	0.65
25	38141.20	2641.36	0.61
26	40835.00	2827.91	0.65
27	33779.40	2339.29	0.54
28	38942.40	2696.85	0.62
29	52352.60	3625.53	0.83
30	47189.50	3267.97	0.75
31	47990.80	3323.46	0.76
32	45297.00	3136.91	0.72
33	68338.90	4732.61	1.08
34	67755.80	4692.23	1.07
35	67768.40	4693.10	1.08
36	68326.40	4731.74	1.08
37	55984.70	3877.06	0.89
38	55401.60	3836.68	0.88
39	55414.20	3837.55	0.88
40	55972.20	3876.19	0.89
41	42786.30	2963.04	0.68
42	42203.20	2922.66	0.67
43	42215.70	2923.53	0.67
44	42773.70	2962.17	0.68
45	39442.50	2731.47	0.63
46	38859.40	2691.09	0.62
47	38871.90	2691.96	0.62
48	39429.90	2730.60	0.63

Plinto n. 1
B=3.80 <m> L=3.80 <m> k_1=1500000.00 <daN/mc> kw=436548.00 <daN/mc>

CC	N <daN>	q_{es} <daN/mq>	Ced <cm>
1	59433.80	4115.92	0.94
2	60016.90	4156.30	0.95
3	59446.50	4116.79	0.94
4	60004.30	4155.42	0.95
5	49847.80	3452.06	0.79
6	50430.90	3492.44	0.80
7	49860.40	3452.94	0.79
8	50418.20	3491.57	0.80
9	41028.50	2841.31	0.65
10	41611.60	2881.69	0.66
11	41041.10	2842.18	0.65
12	41598.90	2880.81	0.66
13	38780.50	2685.63	0.62
14	39363.60	2726.01	0.62
15	38793.20	2686.51	0.62
16	39351.00	2725.14	0.62
17	33578.30	2325.37	0.53
18	38871.90	2691.96	0.62
19	37840.30	2620.52	0.60
20	40777.60	2823.94	0.65
21	48118.30	3332.29	0.76
22	45181.00	3128.88	0.72

23	52380.30	3627.44	0.83
24	47086.70	3260.85	0.75
25	33695.00	2333.45	0.53
26	38856.80	2690.91	0.62
27	38057.00	2635.53	0.60
28	40749.50	2821.99	0.65
29	47901.60	3317.28	0.76
30	45209.10	3130.82	0.72
31	52263.60	3619.36	0.83
32	47101.80	3261.90	0.75
33	21161.60	1465.49	0.34
34	21744.70	1505.87	0.34
35	21174.30	1466.36	0.34
36	21732.10	1504.99	0.34
37	24333.00	1685.11	0.39
38	24916.10	1725.49	0.40
39	24345.70	1685.99	0.39
40	24903.40	1724.61	0.40
41	35925.50	2487.92	0.57
42	36508.60	2528.30	0.58
43	35938.20	2488.79	0.57
44	36495.90	2527.42	0.58
45	38780.50	2685.63	0.62
46	39363.60	2726.01	0.62
47	38793.20	2686.51	0.62
48	39351.00	2725.14	0.62

Plinto n. 4
B=3.80 <m> L=3.80 <m> k_1=1500000.00 <daN/mc> kw=436548.00 <daN/mc>

CC	N <daN>	q_{es} <daN/mq>	Ced <cm>
1	30068.80	2082.33	0.48
2	29485.70	2041.95	0.47
3	30056.30	2081.46	0.48
4	29498.30	2042.82	0.47
5	30471.30	2110.20	0.48
6	29888.20	2069.82	0.47
7	30458.70	2109.33	0.48
8	29900.80	2070.69	0.47
9	37683.20	2609.64	0.60
10	37100.10	2569.26	0.59
11	37670.60	2608.77	0.60
12	37112.70	2570.13	0.59
13	39442.00	2731.44	0.63
14	38858.90	2691.06	0.62
15	39429.40	2730.57	0.63
16	38871.50	2691.93	0.62
17	52466.90	3633.44	0.83
18	47173.10	3266.83	0.75
19	48204.10	3338.23	0.76
20	45267.00	3134.83	0.72
21	37926.90	2626.52	0.60
22	40864.00	2829.92	0.65
23	33664.10	2331.31	0.53
24	38957.90	2697.92	0.62
25	52351.10	3625.42	0.83
26	47188.60	3267.91	0.75
27	47989.10	3323.35	0.76
28	45295.90	3136.84	0.72
29	38141.90	2641.40	0.61
30	40835.10	2827.91	0.65
31	33779.90	2339.33	0.54
32	38942.40	2696.84	0.62
33	68334.60	4732.32	1.08
34	67751.50	4691.94	1.07
35	68322.10	4731.45	1.08
36	67764.10	4692.81	1.07
37	55981.80	3876.86	0.89
38	55398.70	3836.48	0.88
39	55969.30	3875.99	0.89
40	55411.30	3837.35	0.88
41	42785.30	2962.97	0.68

42 42202.20 2922.59 0.67
43 42772.70 2962.10 0.68
44 42214.80 2923.46 0.67
45 39442.00 2731.44 0.63
46 38858.90 2691.06 0.62
47 39429.40 2730.57 0.63
48 38871.50 2691.93 0.62

Plinto n. 3
B=3.80 <m> L=3.80 <m> k_1=1500000.00 <daN/mc> kw=436548.00 <daN/mc>

CC	N <daN>	q_{es} <daN/mq>	Ced <cm>
1	29335.60	2031.55	0.47
2	29918.70	2071.94	0.47
3	29906.10	2071.06	0.47
4	29348.30	2032.43	0.47
5	29782.40	2062.49	0.47
6	30365.50	2102.87	0.48
7	30352.80	2101.99	0.48
8	29795.00	2063.37	0.47
9	37015.80	2563.42	0.59
10	37598.90	2603.80	0.60
11	37586.20	2602.92	0.60
12	37028.40	2564.30	0.59
13	38781.00	2685.67	0.62
14	39364.10	2726.05	0.62
15	39351.40	2725.17	0.62
16	38793.70	2686.54	0.62
17	37841.50	2620.60	0.60
18	40778.60	2824.00	0.65
19	33578.90	2325.41	0.53
20	38872.60	2692.01	0.62
21	52380.70	3627.47	0.83
22	47087.10	3260.88	0.75
23	48118.10	3332.28	0.76
24	45181.10	3128.88	0.72
25	47903.30	3317.40	0.76
26	45210.20	3130.90	0.72
27	52265.10	3619.46	0.83
28	47102.80	3261.96	0.75
29	33694.60	2333.42	0.53
30	38856.90	2690.92	0.62
31	38056.40	2635.48	0.60
32	40749.40	2821.98	0.65
33	21165.80	1465.78	0.34
34	21748.90	1506.16	0.35
35	21736.20	1505.28	0.34
36	21178.50	1466.65	0.34
37	24335.80	1685.31	0.39
38	24918.90	1725.69	0.40
39	24906.20	1724.81	0.40
40	24348.50	1686.18	0.39
41	35926.40	2487.98	0.57
42	36509.60	2528.36	0.58
43	36496.90	2527.49	0.58
44	35939.10	2488.86	0.57
45	38781.00	2685.67	0.62
46	39364.10	2726.05	0.62
47	39351.40	2725.17	0.62
48	38793.70	2686.54	0.62

Criteri di analisi geotecnica e progetto delle fondazioni

Fondazioni superficiali

Generali

Generali
Condizioni di calcolo per terreni coesivi Sia drenate che non drenate
Calcolo di a' dal rapporto con c'

1
Calcolo di a_u dal rapporto con c_u
1
Calcolo di σ'dal rapporto con ϕ'
1
Considera l'angolo di attrito in deformazione piana per fondazioni nastriformi
No
Calcolo dei parametri rappresentativi per terreni stratificati
Media pesata
-Calcola i valori medi dell'angolo di attrito secondo la sua tangente
No
Capacità portante in condizioni statiche
Calcolo della capacità portante per rottura generale Indicazioni EC7 (Allegato D)
-Combinazione dei fattori di forma e di inclinazione del carico Considera solo i fattori di forma
-Considera il fattore di riduzione per platee
No
-Considera gli effetti dell'eccentricità del carico con un unico fattore riduttivo
No
Considera eccentricità e inclinazione dei carichi attraverso domini di interazione
No
-Parametro correttivo del momento
0
-Parametro correttivo del carico orizzontale
0
Calcolo della capacità portante per rottura locale
No

Vesic (1975)
Calcolo della capacità portante per rottura per punzonamento
No
Calcolo della capacità portante per scorrimento
No
-Percentuale di carico orizzontale assorbito dai cordoli <%>
0
-Percentuale di spinta passiva mobilitata <%>
0
Calcolo della capacità portante per sollevamento
No
Capacità portante in condizioni sismiche
Calcolo della capacità portante per rottura generale
No
Riduzione dell'angolo d'attrito per terreni incoerenti ben addensati
No
Calcolo della capacità portante per scorrimento
No
-Percentuale di carico orizzontale assorbito dai cordoli <%>
0
-Percentuale di spinta passiva mobilitata <%>
0
Cedimenti
Cedimenti
Terzaghi (1955)
-Costante di sottofondo standardizzata k_1
****
Considera pressioni di esercizio al netto delle tensioni litostatiche
No
Calcola costante di sottofondo per pressioni di esercizio
No
Limita costante di sottofondo ad un valore
No

Fondazioni profonde

Generali

Generali
Calcolo capacità portante per carichi verticali Secondo formule statiche
Considera capacità portante
Entrambe

Condizioni di calcolo per terreni coesivi Sia drenate che non drenate
Calcolo della profondità critica
No
Effettua calcolo elasto-plastico per cedimenti
Si
Effettua calcolo elasto-plastico per spostamenti orizzontali
Si
Rapporto di elasticità trazione/compressione pari a
1
Fattori di correlazione
1.7
Considera fattori di correlazione anche per carichi orizzontali
No
Considera peso del palo
No
Attrito laterale limite da prove in sito
Correlato con prove CPT
No
Correlato con prove SPT
No
Fattore di riduzione attrito laterale per pali trivellati
No
Pressione limite alla base da prove in sito
Correlata con prove CPT
No
Correlata con prove SPT
No
Fattore di riduzione pressione limite alla base per pali trivellati
No
Spostamenti orizzontali
Spostamenti orizzontali Risposta elastica in funzione della stratigrafia
Specifici
1 2 3 4 5 6 7 8 9 10

Attrito laterale limite
Calcolo dell'attrito laterale limite
Si Si Si Si Si Si Si Si Si Si
-Condizioni non drenate
-Calcolo di α
-Pari a
-A.G.I. (1984)
x x x x x x x x x x
-A.P.I. (1984)
-Viggiani (1999)
-Olson e Dennis (1982)
-Stas e Kulhavy (1984)
-Skempton (1986)
-Reese e O'Neill (1989)
-Metodo di Bustamente e Doix (1985) per micropali
No No No No No No No No No No
-Iniezioni ripetute
x x x x x x x x x x
-Unica iniezione
-Condizioni drenate
-Calcolo di β
-Pari a
0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3
-Reese e O'Neill (1989)
-Calcolato
-Calcolo di k
-Pari a
-Dal rapporto con k_0 pari a
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
-Fleming (1985)
-Calcolo di δ
-Pari a <grad>
-Dal rapporto con ϕ' pari a
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
-Calcolo di a' dal rapporto con c'

1 1 1 1 1 1 1 1 1 1
Calcolo dell'attrito laterale limite per trazione
-Considera i risultati del calcolo per l'attrito laterale limite percompressione con un fattore di riduzione pari a 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7
-Sowa (1970)
No No No No No No No No No No
-Bowles (1991)
No No No No No No No No No No
Considera l'effetto dell'attrito negativo
No No No No No No No No No No
-Coefficiente di Lambe
Pressione limite alla base
Calcolo della pressione limite alla base del palo
Si Si Si Si Si Si Si Si Si Si
-Terzaghi (1943)
x x x x x x x x x x
-Meyerhof (1963)
-Hansen (1970)
-Vesic (1975)
-Berezantzev (1961)
-Berezantzev (1965)
-Stagg e Zienkiewicz (1968)
-Relazione generale, coefficienti di capacità portante
-In condizioni drenate
-N_q
-N_c
-In condizioni non drenate
-N_c
-Fattore di riduzione per terreni coesivi sovraconsolidati
No No No No No No No No No No
Cedimenti
Risposta elastica laterale
-Calcolata dalla rigidezza dello strato
x x x x x x x x x x
-Coefficiente di influenza
4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0
-Pari a <daN/mq>
Risposta elastica alla base
-Calcolata dalla rigidezza dello strato
x x x x x x x x x x
-Pari a <daN/mq>
Spostamenti orizzontali
Risposta elastica
-Vesic (1961)
-Broms (1964)
-Glick (1948)
-Chen (1978)
-Pari a <daN/mq>
-Dal modulo elastico
x x x x x x x x x x
-Coefficiente effetto tridimensionale
2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0
Resistenza limite
-Calcolata dai parametri plastici
x x x x x x x x x x
-Coefficiente effetto tridimensionale resistenza per attrito
3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0
-Coefficiente effetto tridimensionale resistenza per coesione
4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0
-Pari a <daN/mq>

Caratterizzazione

Specifici	1	2	3	4	5	6	7	8	9	10
Informazioni preliminari										
Coefficiente di uniformità	No	No	No	No	No	No	No	No	No	No
-Pari a	0	0	0	0	0	0	0	0		

0 0
Definizione della composizione granulometrica, per terreni incoerenti No No No No No No No No
No No
-Sabbia fine uniforme x x x x x x x x
x x
-Sabbia fine ben gradata - sabbia media uniforme
-Sabbia media ben gradata - sabbia grossa uniforme
-Sabbia e ghiaia - ghiaia media
Definizione indici compressibilità edometrica, per terreni coesivi No No No No No No No No
No No
-Indice di compressione (Cc) 0 0 0 0 0 0 0 0
0 0
-Indice di ricompressione (Cr) 0 0 0 0 0 0 0 0
0 0
-Considera incremento preconsolidazione costante No No No No No No No No
No No
-Pari a 0 0 0 0 0 0 0 0
0 0
Correggi NSPT se la misura è sottofalda No No No No No No No No
No No
Densità relativa
Correlata con prove SPT
-Terzaghi e Peck (1948) Si Si Si Si Si Si Si Si
Si Si
-Gibbs e Holtz (1957) No No No No No No No No
No No
-Meyerhof (1957) No No No No No No No No
No No
-Schultze e Menzenbach (1961) No No No No No No No No
No No
-Bazaara (1967) No No No No No No No No
No No
-Marcuson e Bieganousky (1977) No No No No No No No No
No No
-Skempton (1986) No No No No No No No No
No No
Correlata con prove CPT
-Schmertmann (1976) Si Si Si Si Si Si Si Si
Si Si
-Jamiolkowski et al. (1985) No No No No No No No No
No No
-Baldi et al. (1986) No No No No No No No No
No No
Elaborazione dei risultati
-Valore medio x x x x x x x x
x x
-Valore minore
Angolo d'attrito
Correlato con prove SPT
-Terzaghi e Peck (1948) Si Si Si Si Si Si Si Si
Si Si
-Schmertmann (1975) No No No No No No No No
No No
-Wolff (1989) No No No No No No No No
No No
-Hatanaka e Uchida (1996) No No No No No No No No
No No
-Road Bridge Specification No No No No No No No No
No No
-Owasaki e Iwasaki No No No No No No No No
No No
-Japanese National Railway No No No No No No No No
No No
-Peck-Hanson e Thornburn No No No No No No No No
No No
-De Mello No No No No No No No No
No No
Correlato con prove CPT
-Robertson e Campanella (1983) Si Si Si Si Si Si Si Si
Si Si
-Durgunoglu e Mitchell No No No No No No No No
No No
-Caquot No No No No No No No No

No No										
Correlata con proprietà indice										
-In funzione della densità relativa, per terreni incoerenti	No	No	No	No	No	No	No	No	No	No
-In funzione dell'indice di plasticità, per terreni coesivi	No	No	No	No	No	No	No	No	No	No
Elaborazione dei risultati										
-Valore medio	x	x	x	x	x	x	x	x	x	x
-Valore minore										
Coesione non drenata										
Correlata con prove SPT										
-Hara et al. (1971)	Si	Si	Si	Si	Si	Si	Si	Si	Si	Si
-Stroud (1974)	No	No	No	No	No	No	No	No	No	No
Correlata con prove CPT										
-Mayne e Kemper (1988)	Si	Si	Si	Si	Si	Si	Si	Si	Si	Si
-Lunne e Eide	No	No	No	No	No	No	No	No	No	No
Correlata con proprietà indice										
-Bjerrum e Simons (1960)	No	No	No	No	No	No	No	No	No	No
-Skempton (1953)	No	No	No	No	No	No	No	No	No	No
-Calcolata da $\sigma'v_0$ con moltiplicatore pari a	No	No	No	No	No	No	No	No	No	No
Pari a	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Elaborazione dei risultati										
-Valore medio	x	x	x	x	x	x	x	x	x	x
-Valore minore										
Caratteristiche litostatiche										
Grado di sovraconsolidazione										
-Correlato con prove SPT										
-Mayne e Kemper (1988)	Si	No	No	No	No	No	No	No	No	No
-Correlato con prove CPT										
-Mayne e Kemper (1988)	No	No	No	No	No	No	No	No	No	No
-Elaborazione dei risultati										
-Valore medio	x	x	x	x	x	x	x	x	x	x
-Valore minore										
Coefficiente di spinta a riposo										
-Calcolo di k_0 (NC)										
-Jaky (1936)	x	x	x	x	x	x	x	x	x	x
-Brooker e Ireland (1965)										
-Alpan (1967)										
-Massarsch (1979)										
-Correlato con Dr										
-Calcolato dal coefficiente di Poisson										
-Calcolo di α										
-Pari a										
-Kulhawy (1989)	x	x	x	x	x	x	x	x	x	x
-Alpan (1967) per terreni coesivi										
-Alpan (1967) per terreni incoerenti										
-Correlato con Dr										
Parametri elastici										
Correlati con prove GFS										
Correlati con prove SPT										
-Stroud e Butler (1975)										
-Stroud (1989)	x	x	x	x	x	x	x	x	x	x
-Schmertmann (1978)										
-Farrent										
-Menzenbach e Malcev										
-D'Appolonia										
-Schulze e Menzenbach										

-Crespellani e Vannucchi
-Ohsaki e Iwasaki, per sabbie
-Ohsaki e Iwasaki, per sabbie con fini
Correlati con prove CPT
-Schmertmann (1977)
-Robertson e Campanella (1983)
-Kulhawy e Mayne (1990)
-Rix e Stokoe (1992)
-Mayne e Rix (1993)
Fattore correttivo 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0